

Fatigue resistance of Al-Cu-Li alloys – effect of environment

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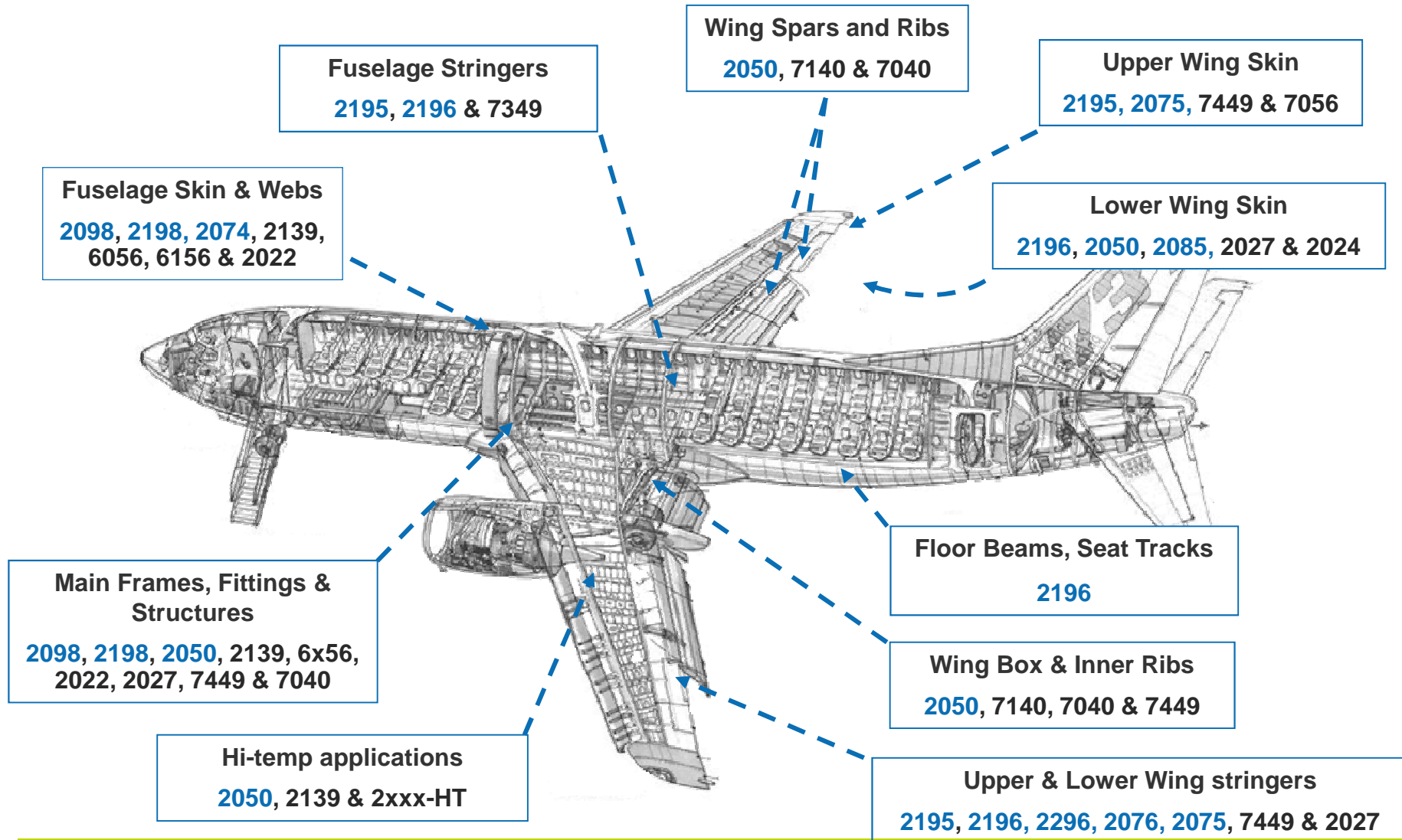


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- General introduction on Al-Cu-Li alloys → AIRWARE®
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 - ▶ Overall behaviour very attractive
 - ▶ Al-Cu-Li alloy fit in the framework of « Poitiers », J. Petit et al.
- Fatigue performance of Al-Cu-Li alloys
 - ▶ Conventional samples
 - ▶ Technological specimens
- Specific study: effect of environment on endurance fatigue
 - ▶ With or without notch
 - ▶ Air or vacuum
- Conclusion

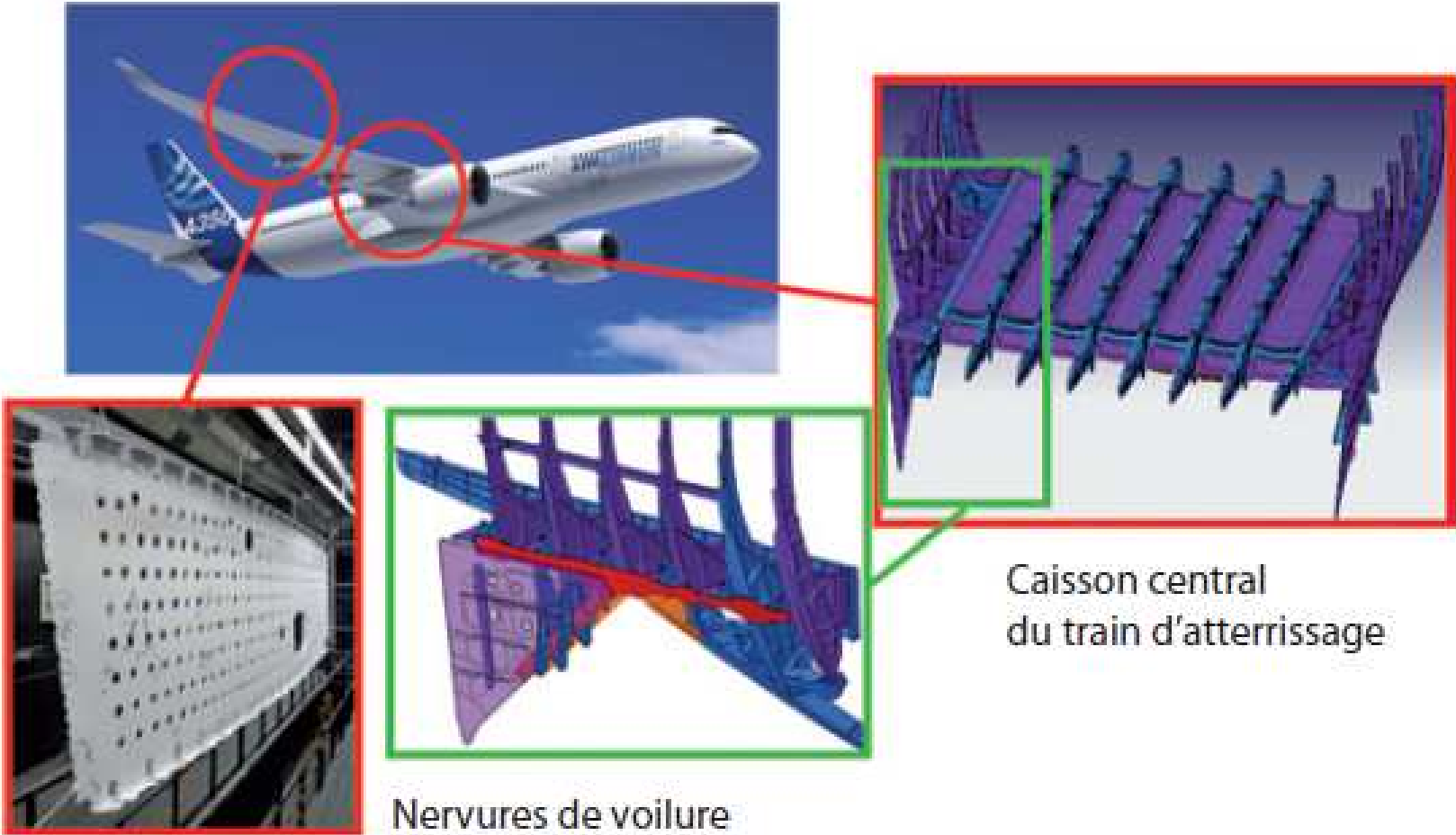
Airware® alloys can be used in the whole aircraft structure

Alloys in Blue designate AIRWARE® = trade mark for Constellium's Al-Cu-Li alloys



2050 industrially applied for thick structures

A350 ribs is a key market

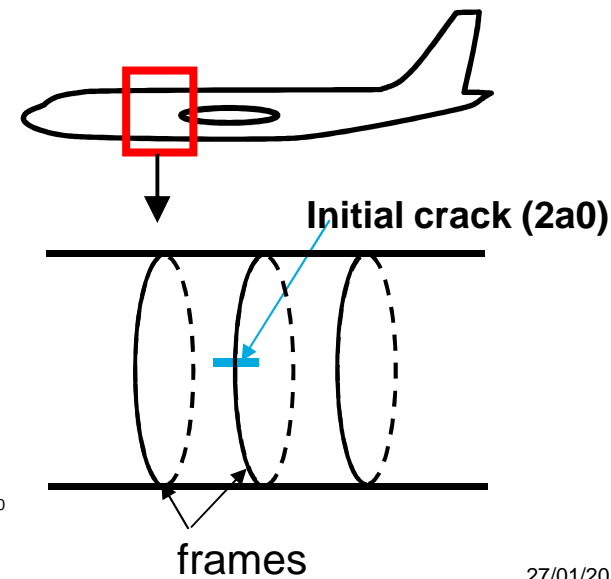
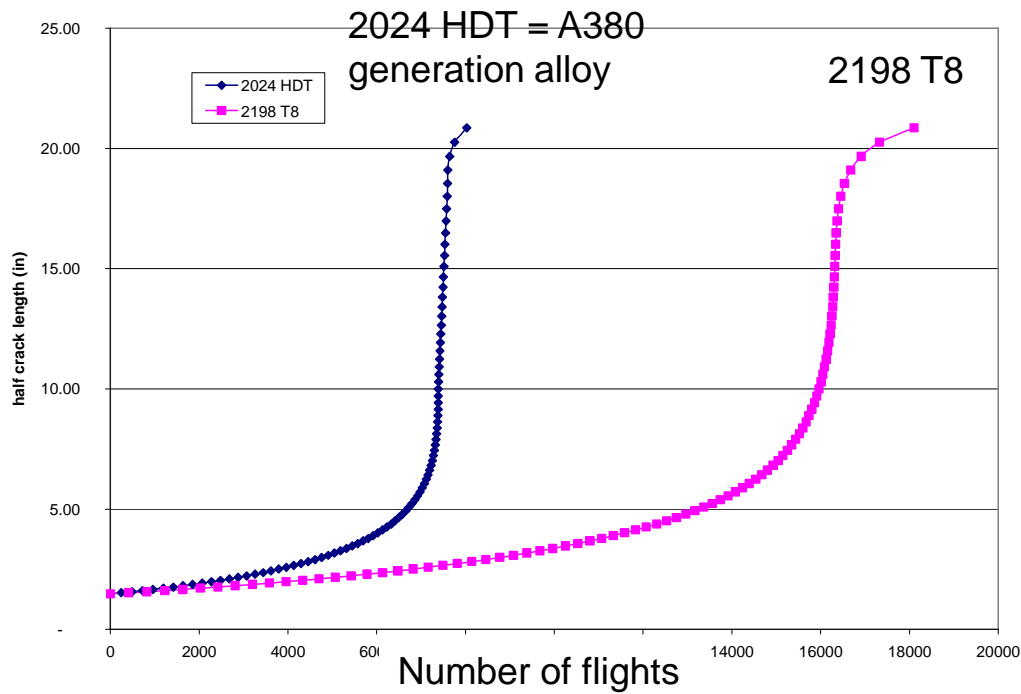


2198 damage tolerance → high performance fuselage

2198 T8 = alloy of C-series fuselage



Longitudinal crack length (in)



27/01/2017

5

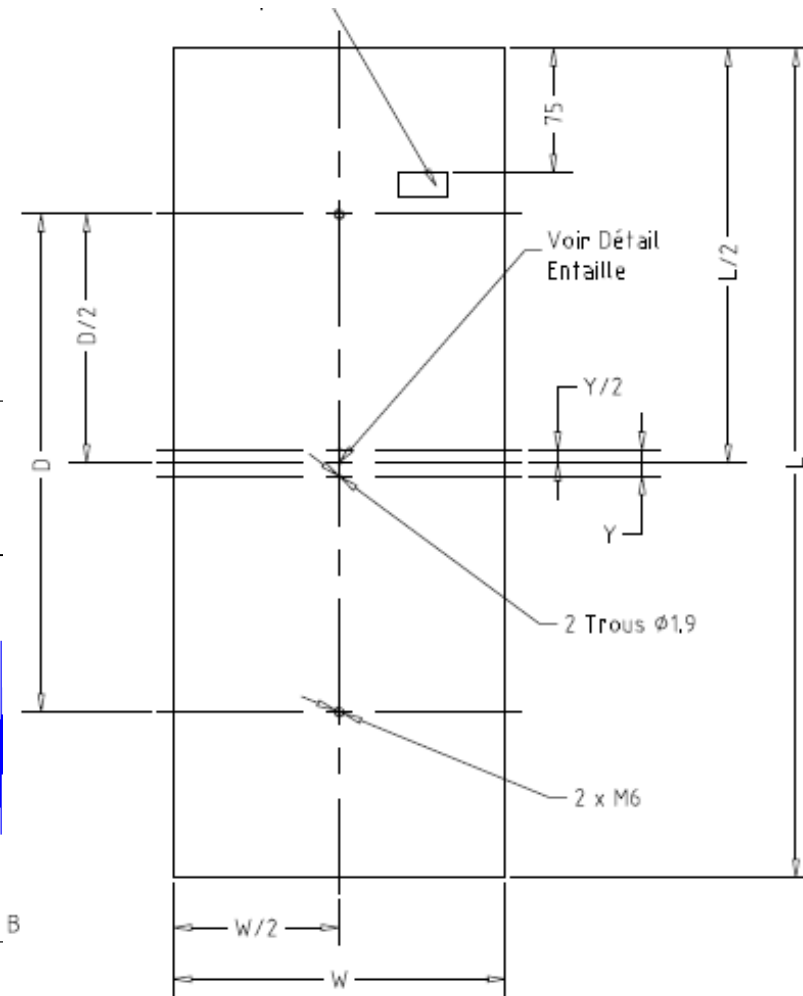
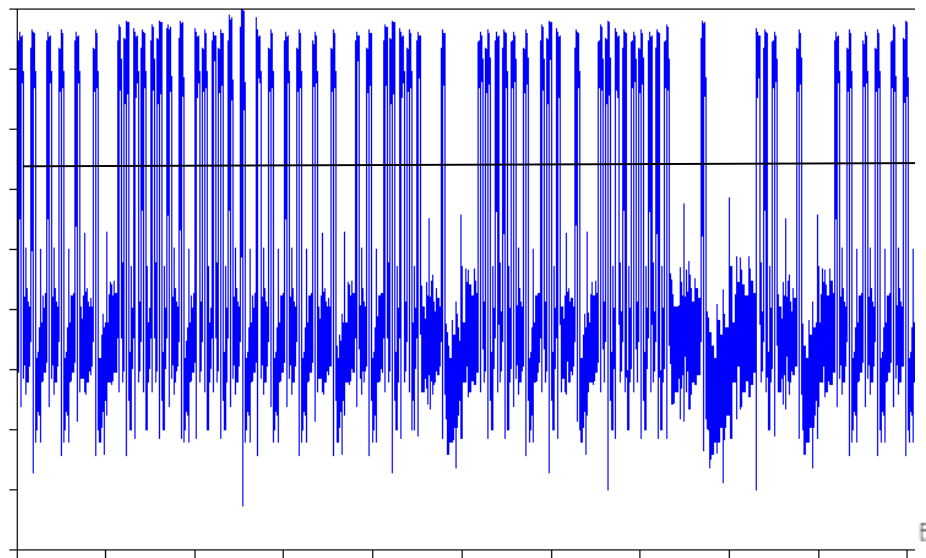


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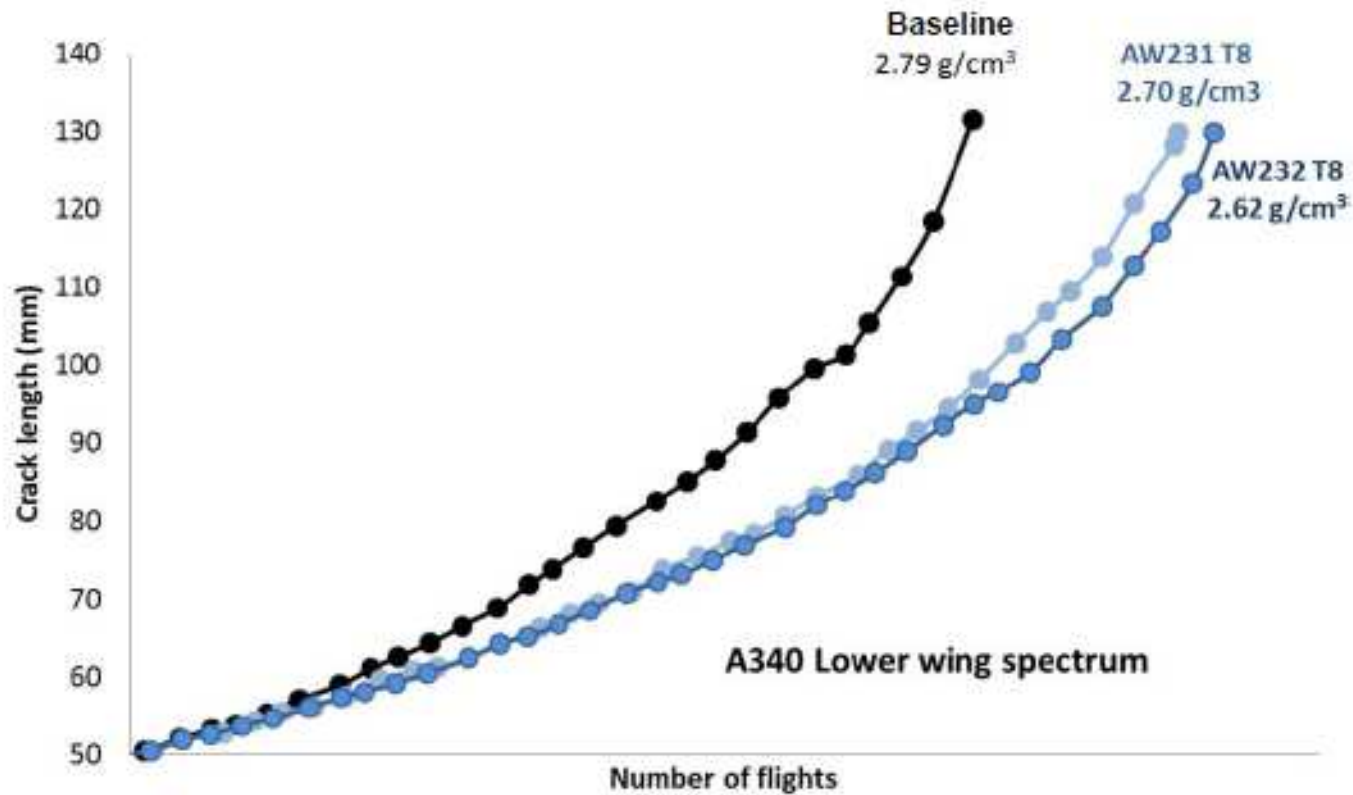
Method: fatigue crack propagation in wing panels

Long range spectrum



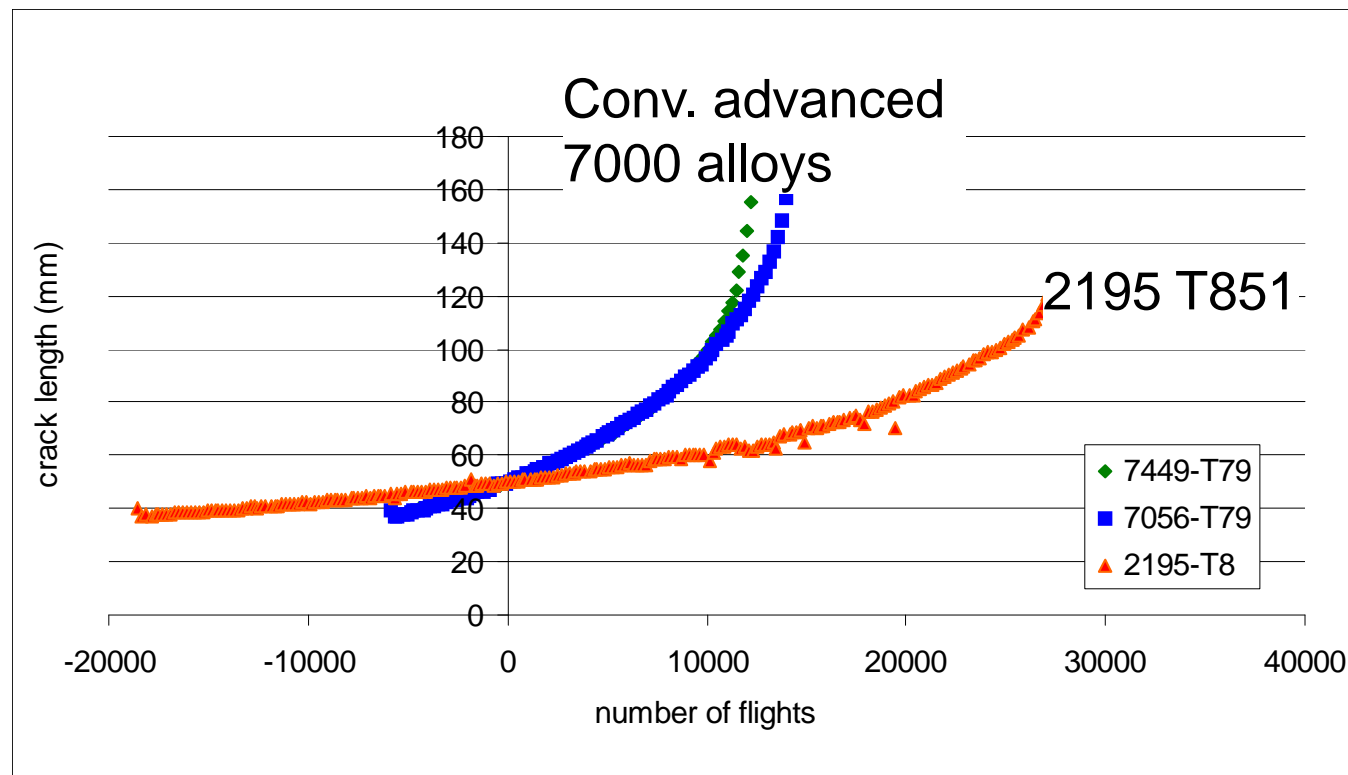
Lower wing Al-Cu-Li alloys performing better than A380 generation alloys (2027, 2024HDT > 2024)

Gain de densité de 5 – 6%



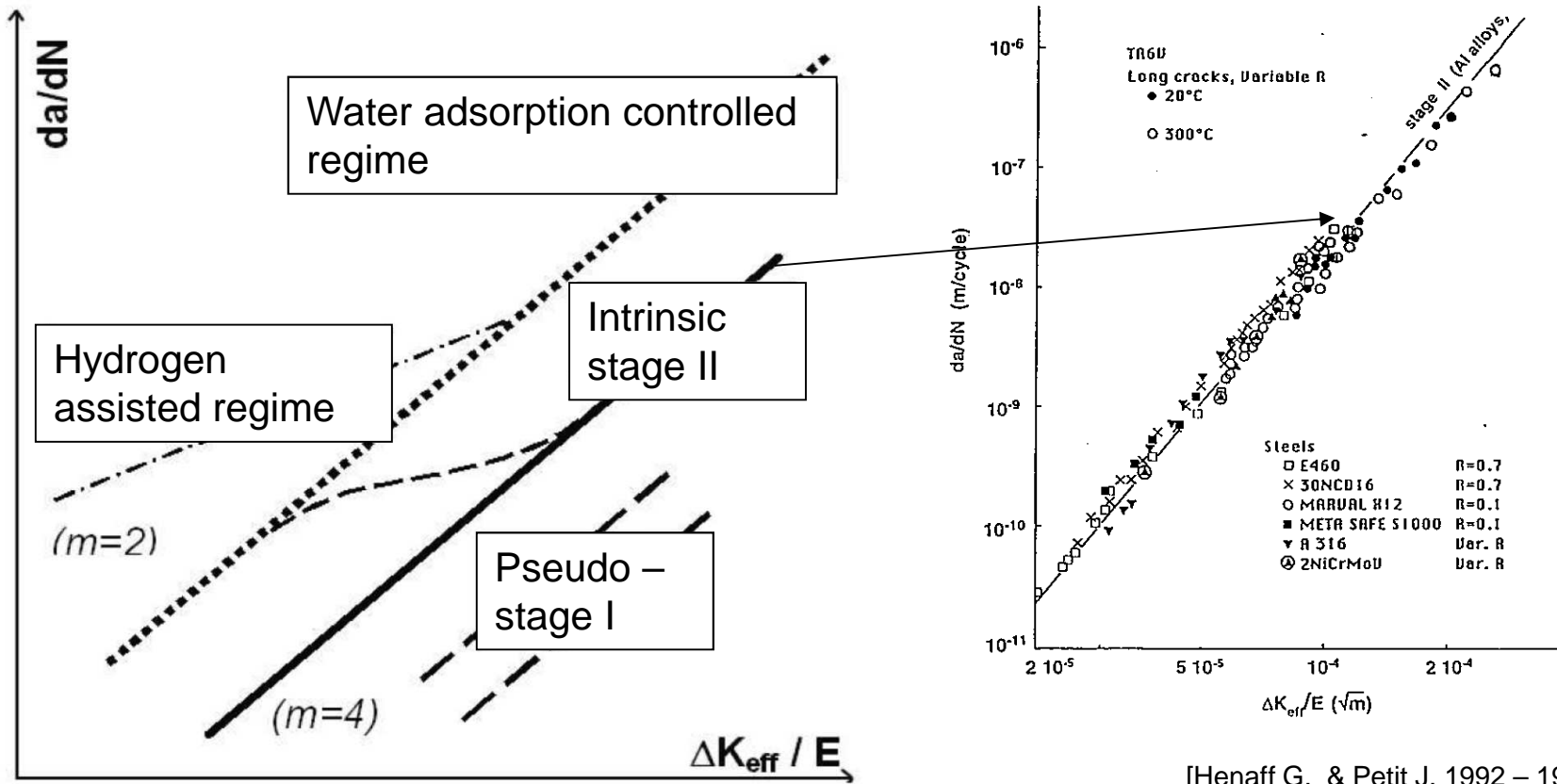
For high strength top wing alloys, FCG under spectrum is improved by a factor 2

- All alloys have similar yield stress



FCG in metals can be described with 4 basic regimes

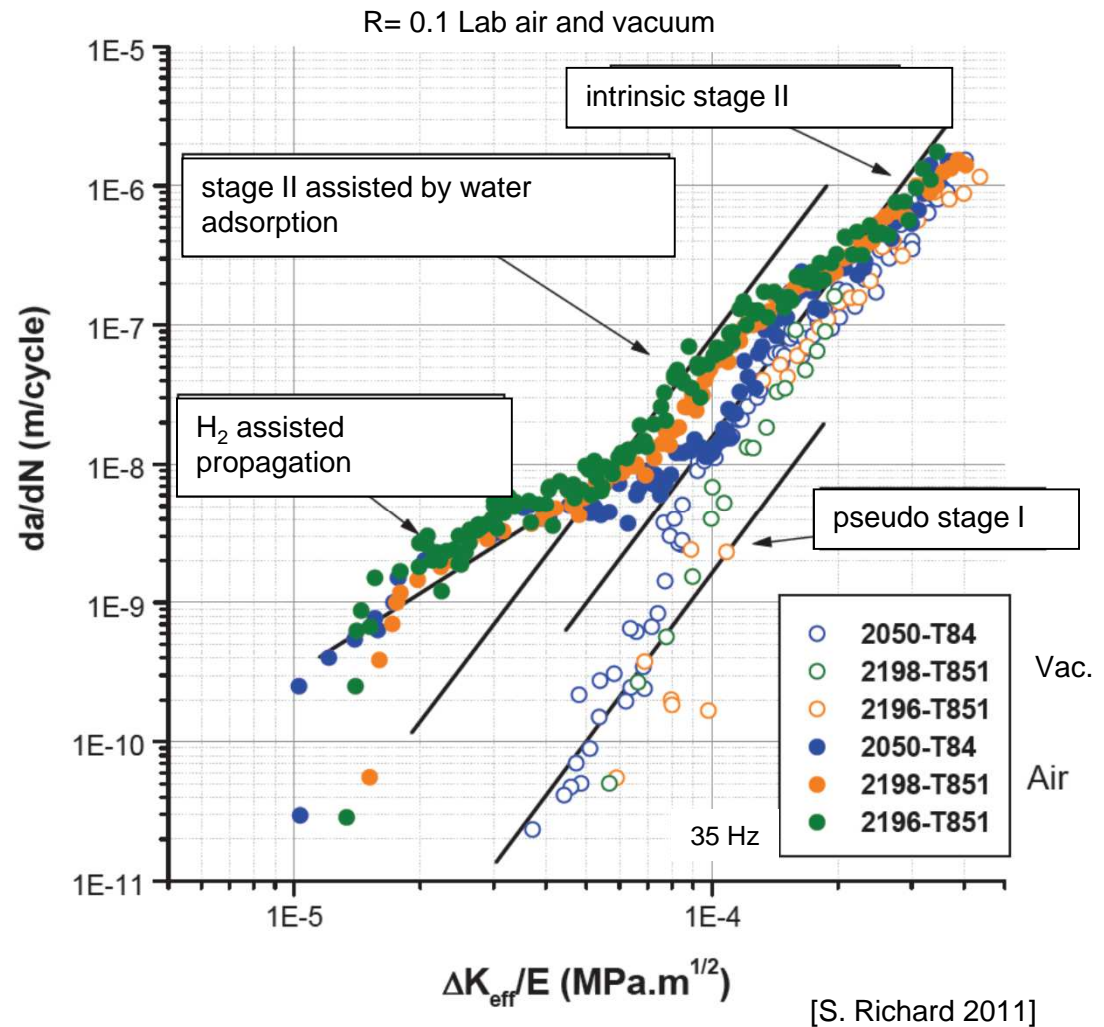
- FCG curves for different Al alloys and other metals (steel, Ti) can be reduced to master curves (e.g.. stage II)
- Effective stress intensity factor (divided by E) is the main parameter



[Henaff G. & Petit J. 1992 – 1995]

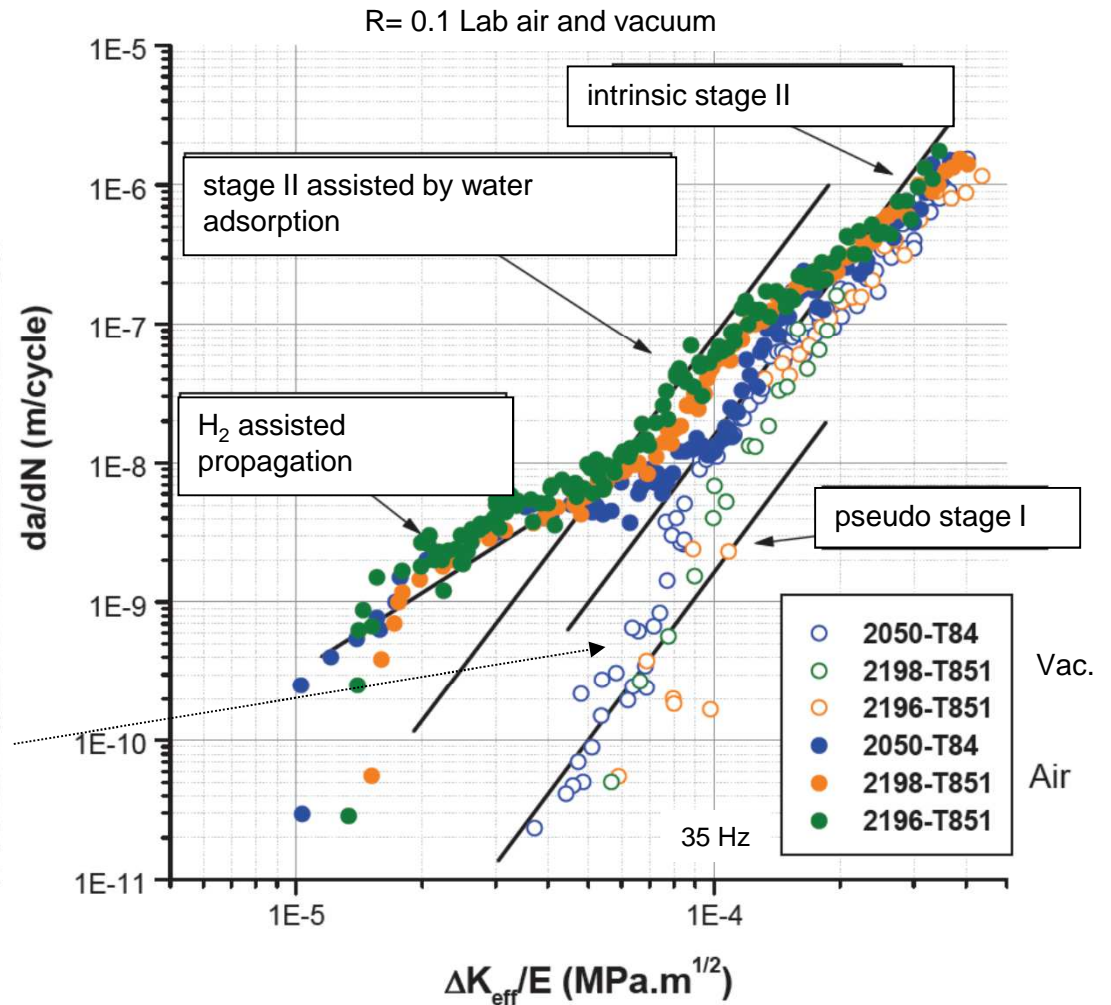
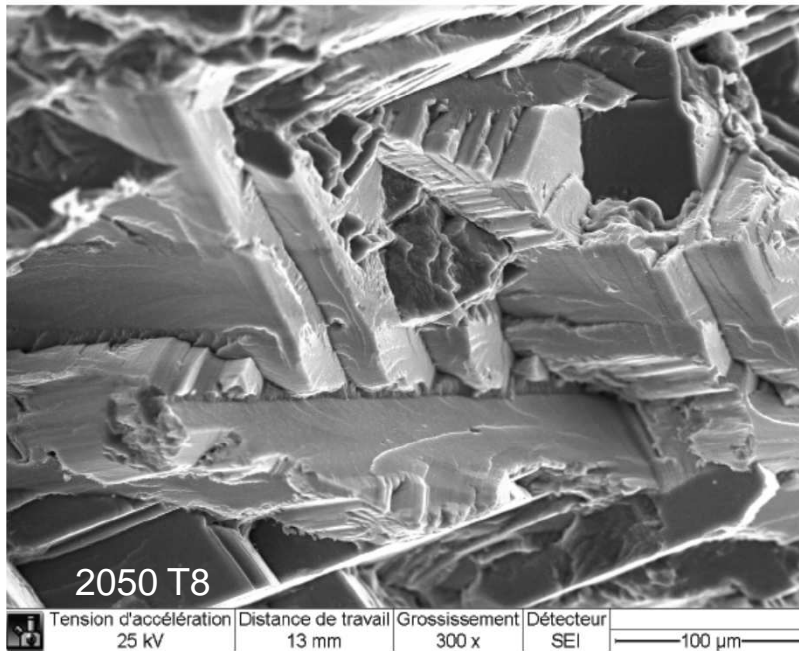
The 4 regimes positioning apply to AIRWARE®

- In ΔK_{eff} plots, all 3 alloys (sheet, plate, low and higher Li contents) behave similarly
- Environment effect amounts to x100 at $\Delta K_{\text{eff}} = 3 \text{ MPa}\cdot\text{m}^{1/2}$
- No environment effect at $\Delta K_{\text{eff}} > 15 \text{ MPa}\cdot\text{m}^{1/2}$



Pseudo-stage I observed under vacuum

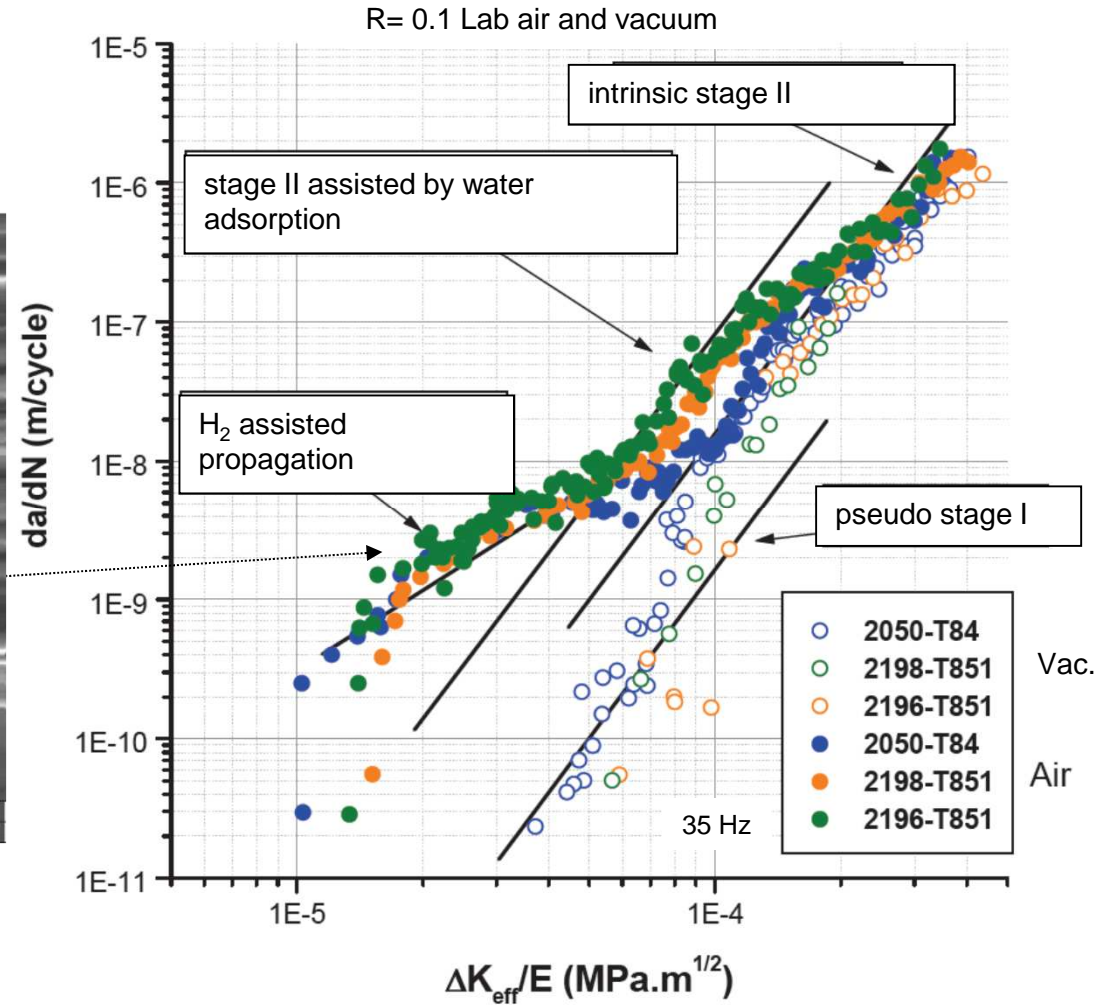
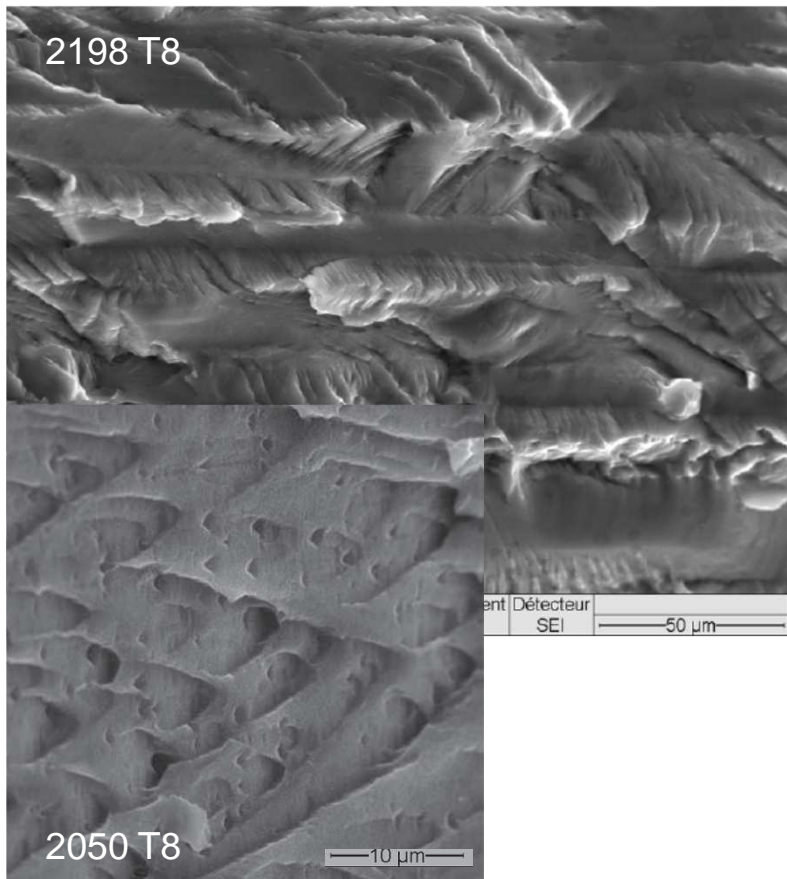
- Crystallographic fracture surface at $\Delta K_{eff} < 7 \text{ MPa}\cdot\text{m}^{1/2}$



[S. Richard 2011]

H₂ assisted fracture → chevrons + smooth zones

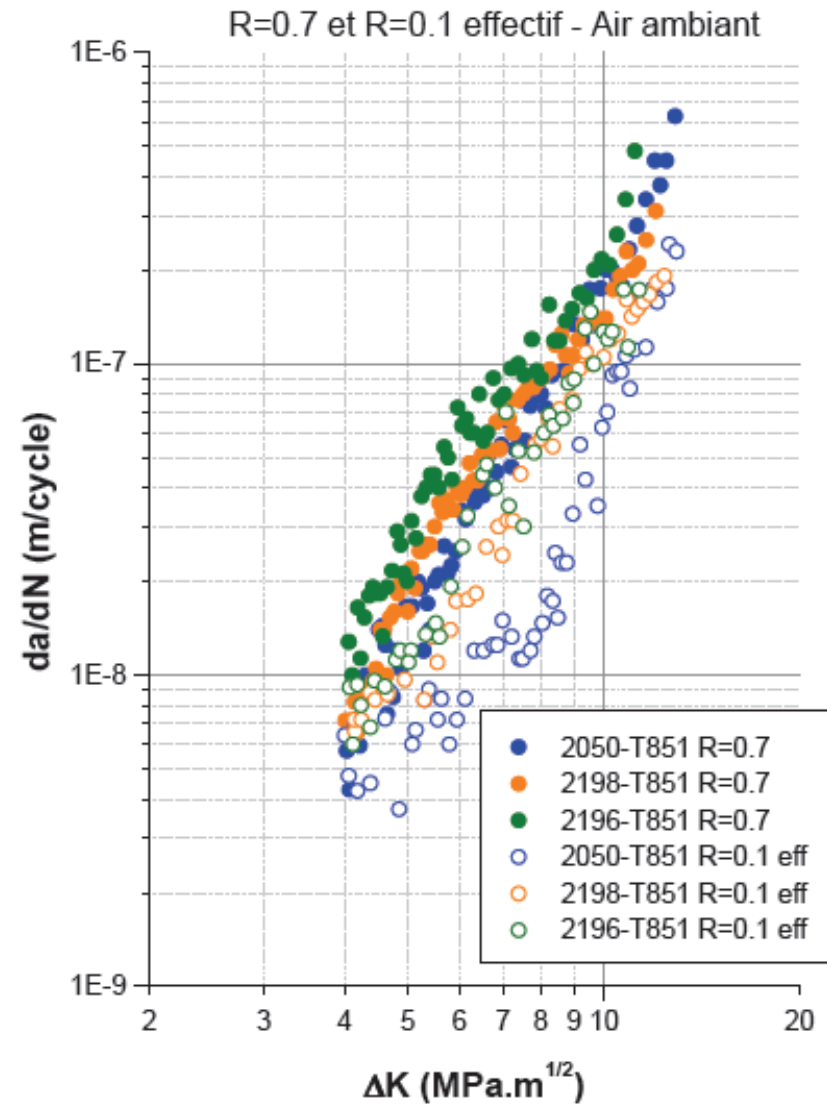
- Chevrons associated to cracking of {111} planes



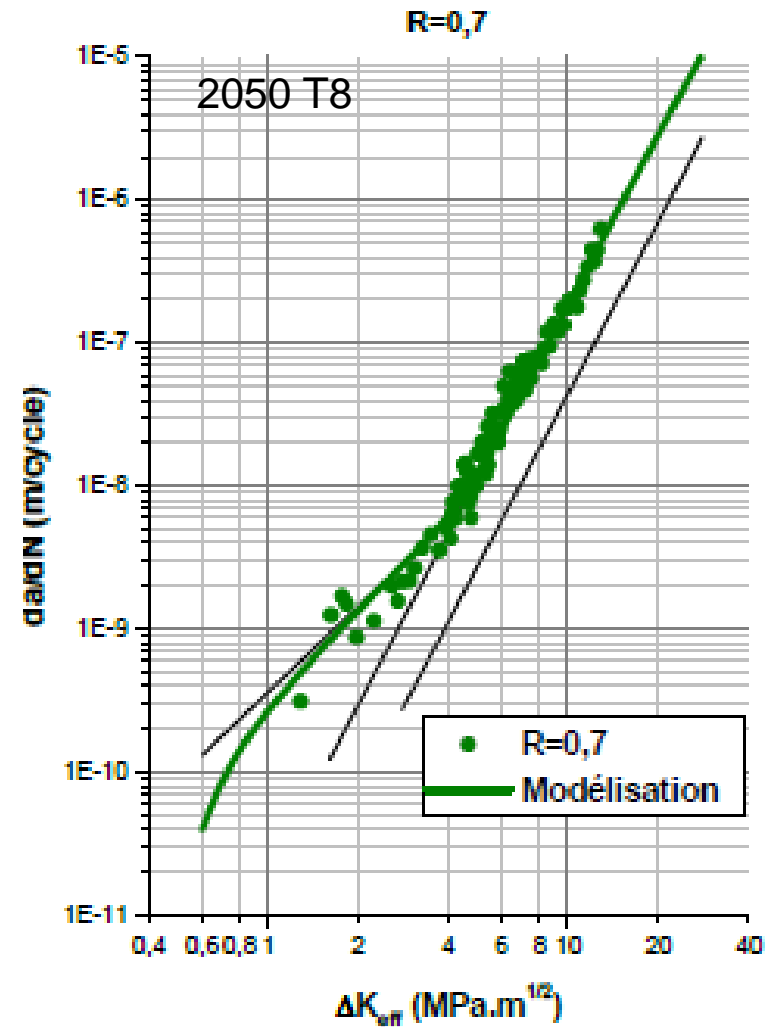
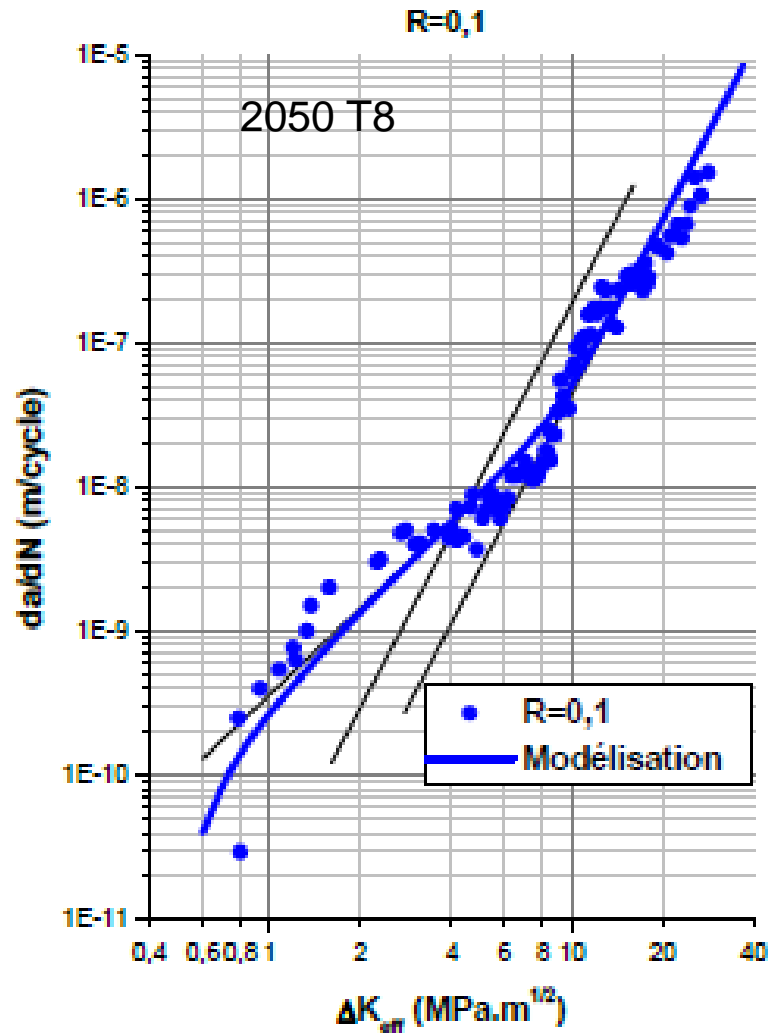
[S. Richard 2011]

Closure does not fully explain R effect

R=0.7 → H₂O can access crack tip

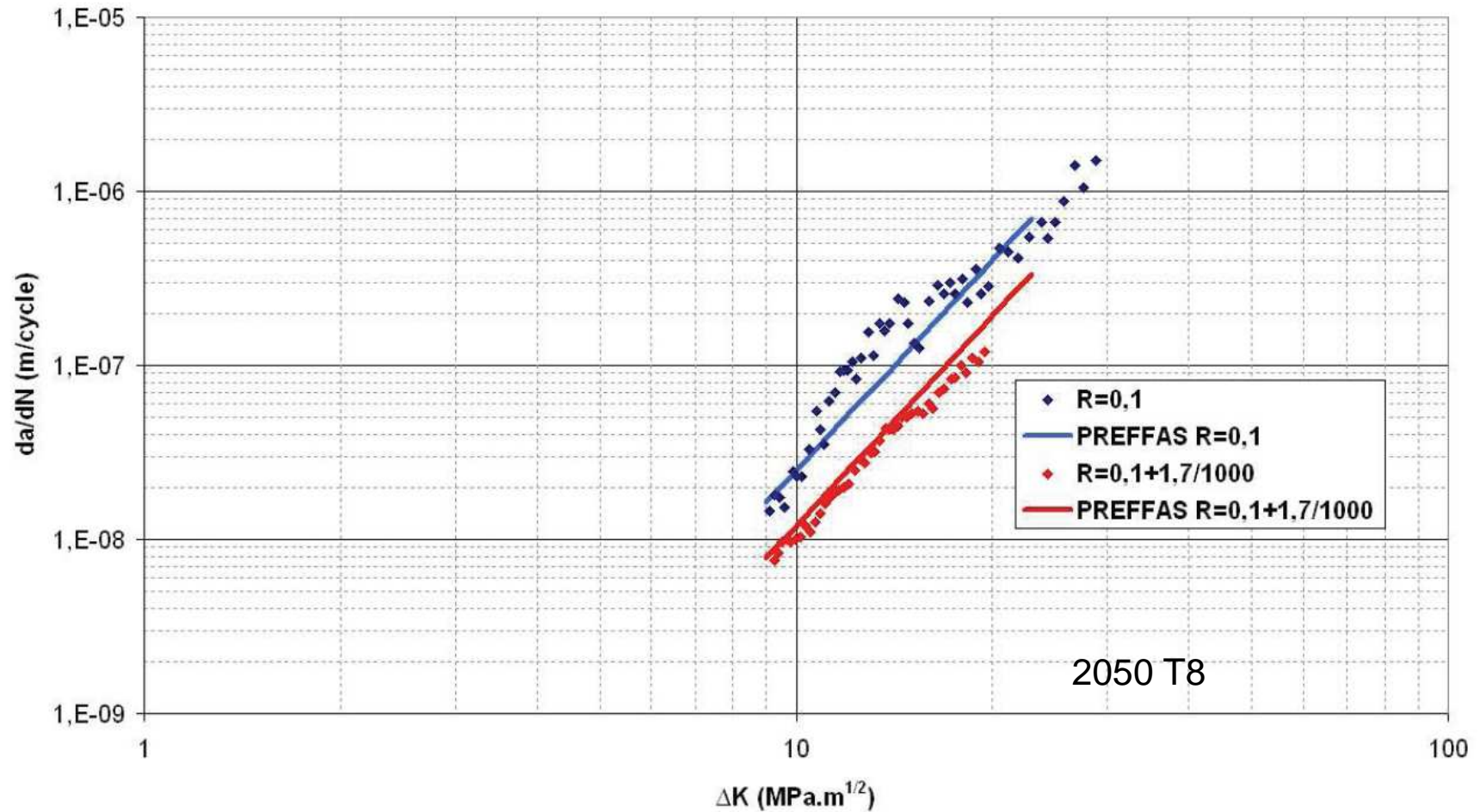


An exposure based model fits with the data



The exposure based model introduced in PREFFAS allows predicting overload effect

Comparaison courbes PREFFAS et expérimentales





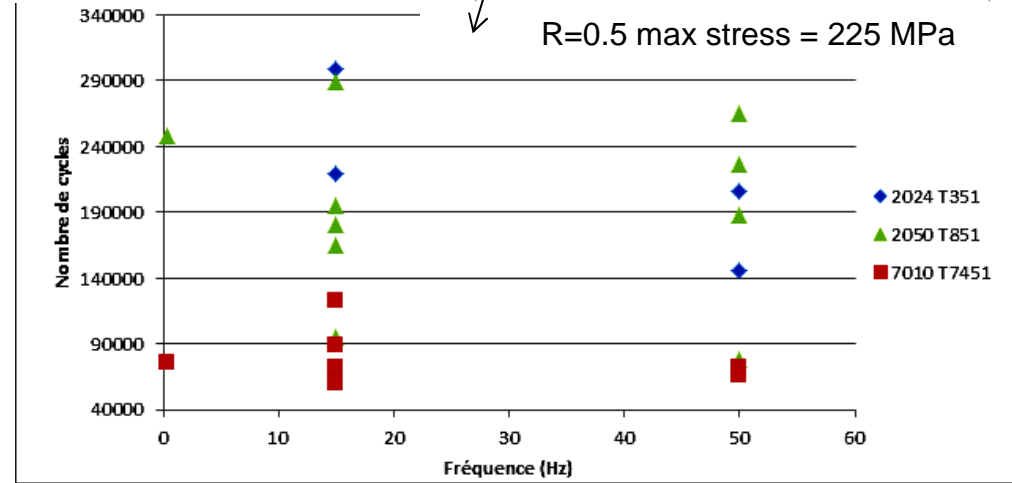
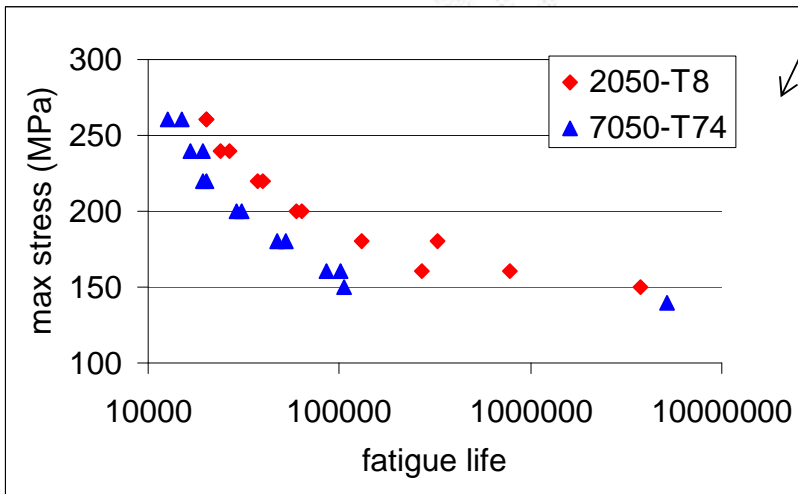
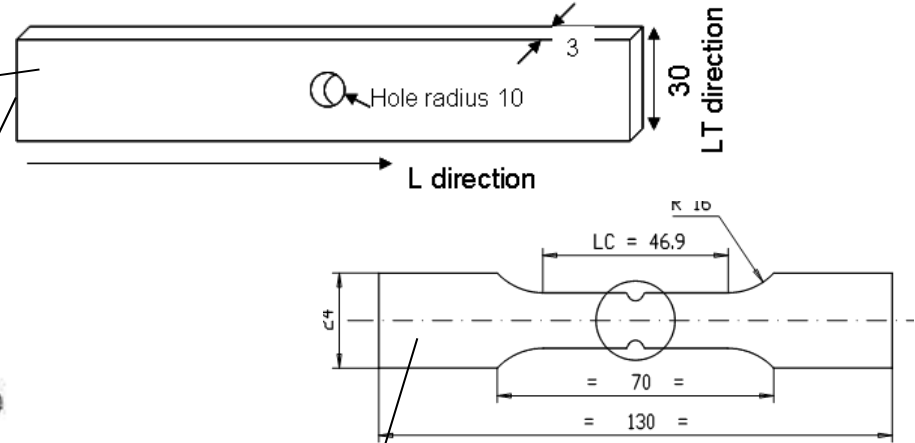
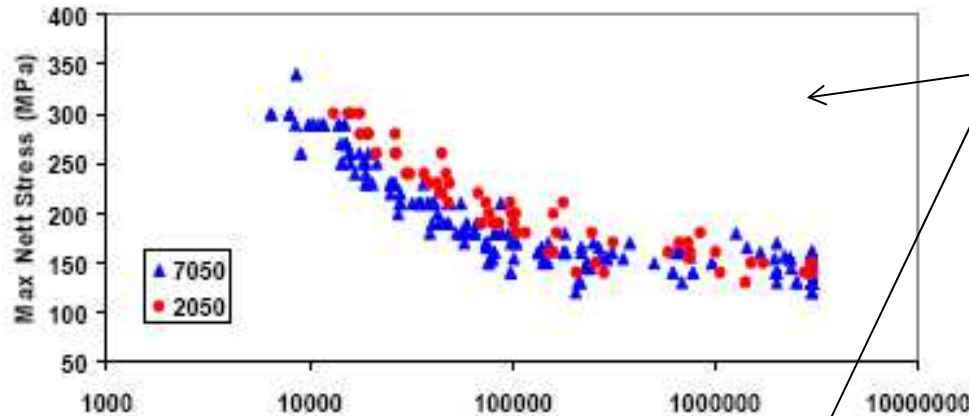
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Open hole fatigue: 2050 > 7050 or 7010

In many studies, 2050 shown to have better resistance than 7000 alloys

OH Fatigue - 2050 vs 7050 - Kt2,3, T-L, R0,1, t/2 - Th=75-125mm

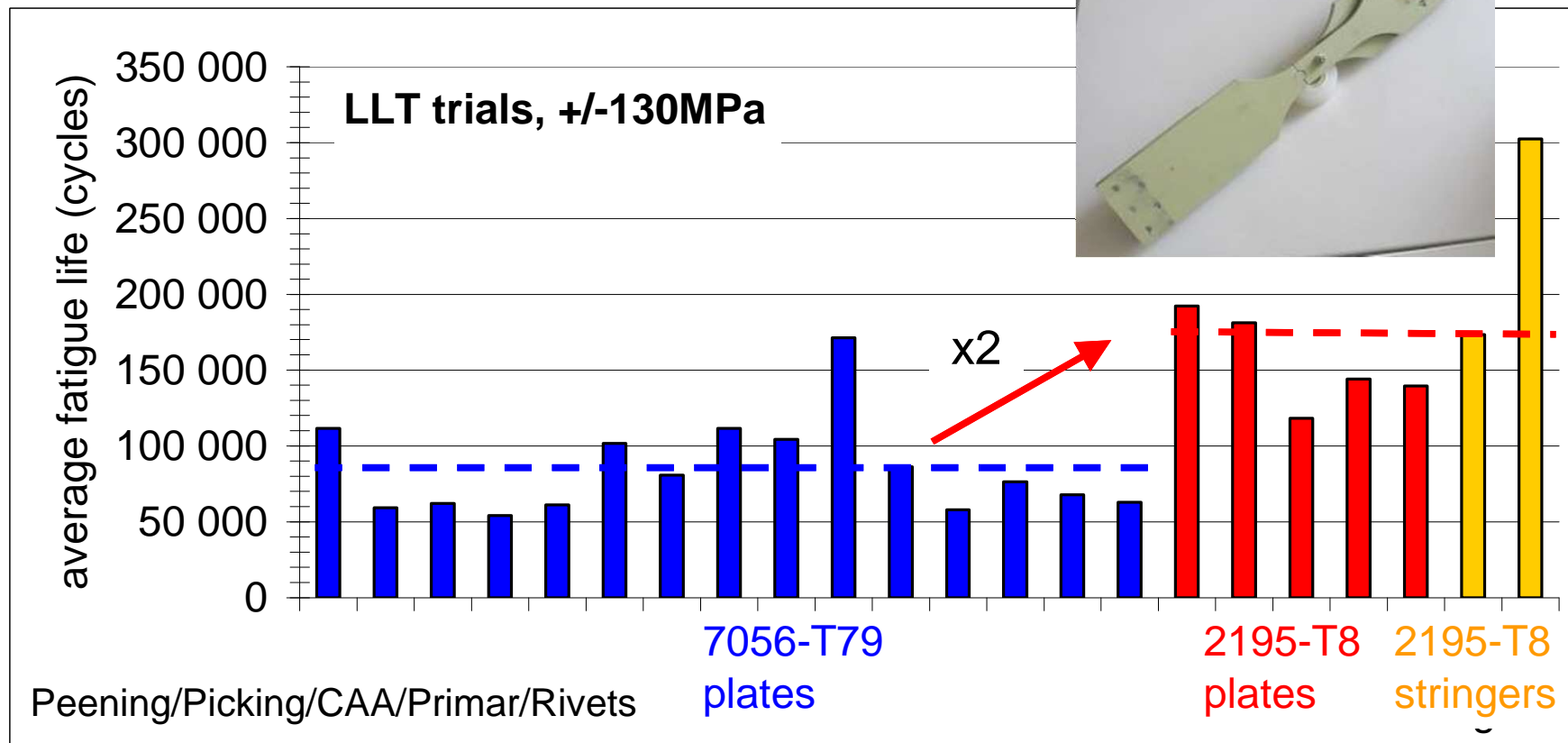


Low Load Transfer fatigue testing: Constant Amplitude

AIRWARE® products have increased lifetime compared to 7xxx alloys

AIRWARE® alloys have 2 times longer fatigue life compared to 7xxx alloys in a low load transfer assembly fatigue configuration

- Full surface preparation included before riveted assembly

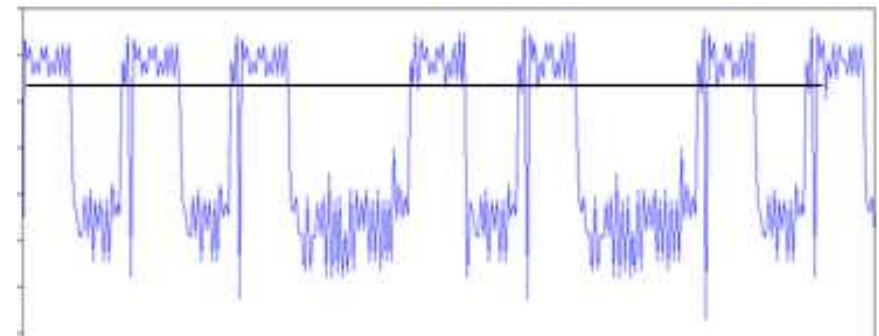
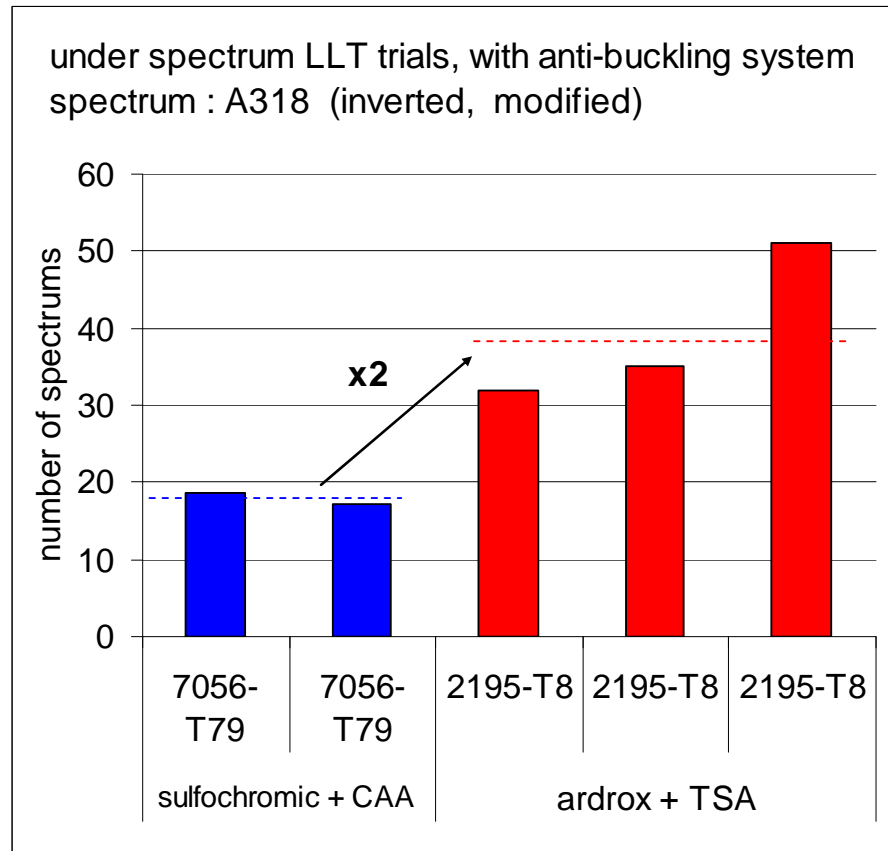


Low Load Transfer fatigue testing: Variable Amplitude

AIRWARE® products have increased lifetime compared to 7xxx alloys

AIRWARE® alloys have 2 times longer fatigue life compared to 7xxx alloys: This gain is confirmed for Chromium free surface treatment

■ Specimen preparation: Ardrex + TSA

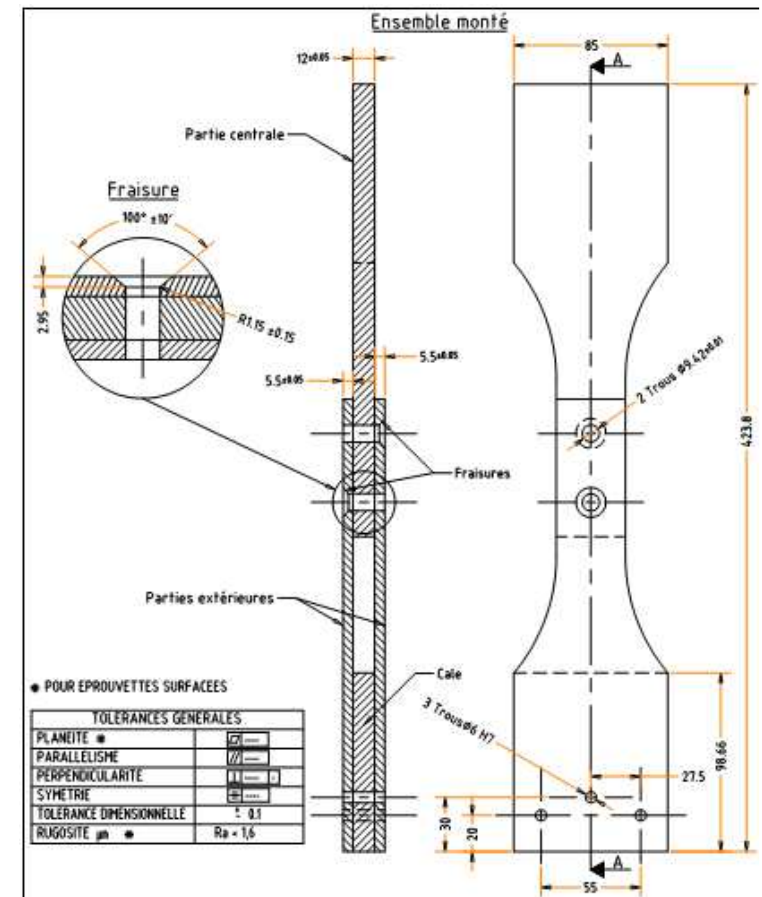
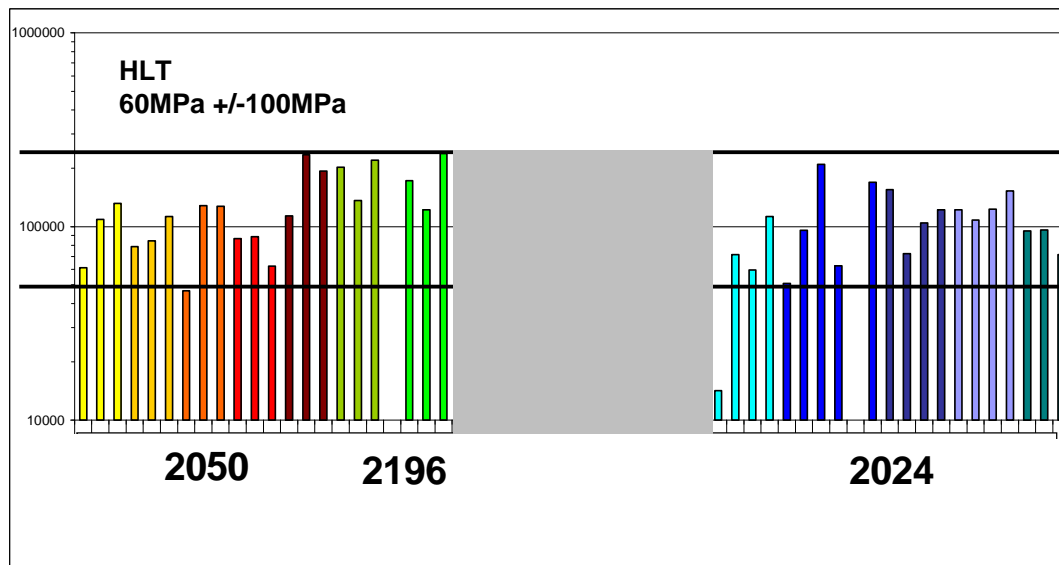


High Load Transfer fatigue testing

AIRWARE® 2050 has typical 2xxx alloys type behaviour

AIRWARE® 2050 has a high fatigue performance in an assembled test configuration including the full surface preparation process route.

- Specimens preparation:
 - ▶ Shot peening
 - ▶ Pickling + Chromic Acid Anodizing
 - ▶ Coating with primer
 - ▶ Titanium rivet



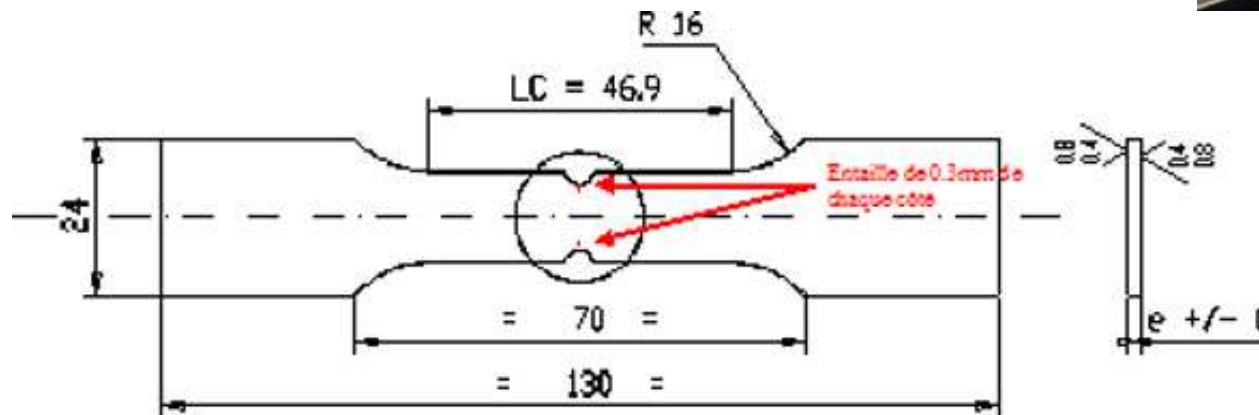


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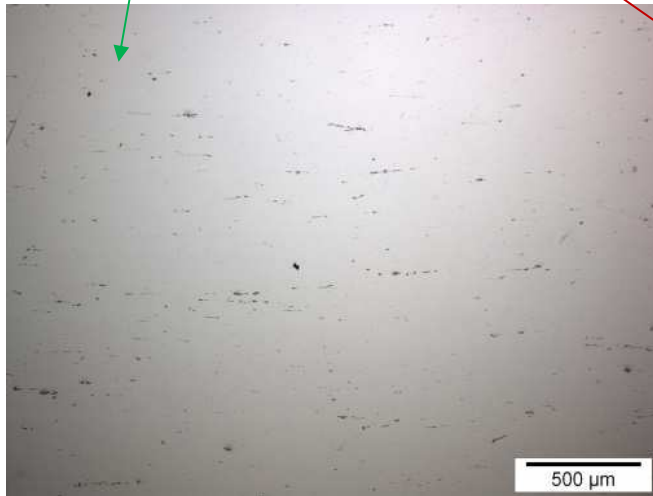
Tests selected to identify intrinsic behaviour

- Sample with and without a small slot at notch root
 - ▶ $K_t=2.15$
- $R=0.5 \rightarrow$ no closure
- Vacuum ($<2 \cdot 10^{-5}$ mBar), air at $f=0.3$ Hz, 15 Hz and 50 Hz



Materials investigated

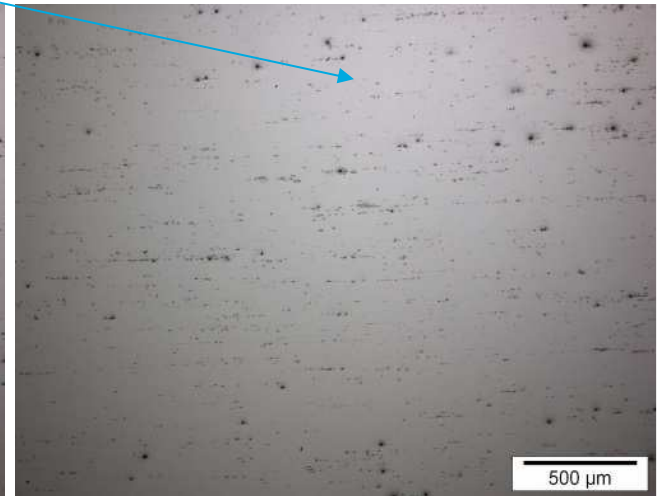
	Si	Fe	Cu	Mn	Mg	Zn	Ti	Zr	Ag	Li
2050	0.08 <i>max</i>	0.10 <i>max</i>	3.2- 3.9	0.20- 0.50	0.20- 0.6	-	0.10 <i>max</i>	0.06- 0.14	0.20- 0.7	0.7- 1.3
7010	0.12 <i>max</i>	0.15 <i>max</i>	1.5- 2.0	-	2.1- 2.6	5.6- 6.7	0.06 <i>max</i>	0.10- 0.16	-	-
2024	0.50 <i>max</i>	0.50 <i>max</i>	3.8- 4.9	0.30- 0.9	1.2- 1.8	-	0.15 <i>max</i>	-	-	-



2050 T8 90 mm



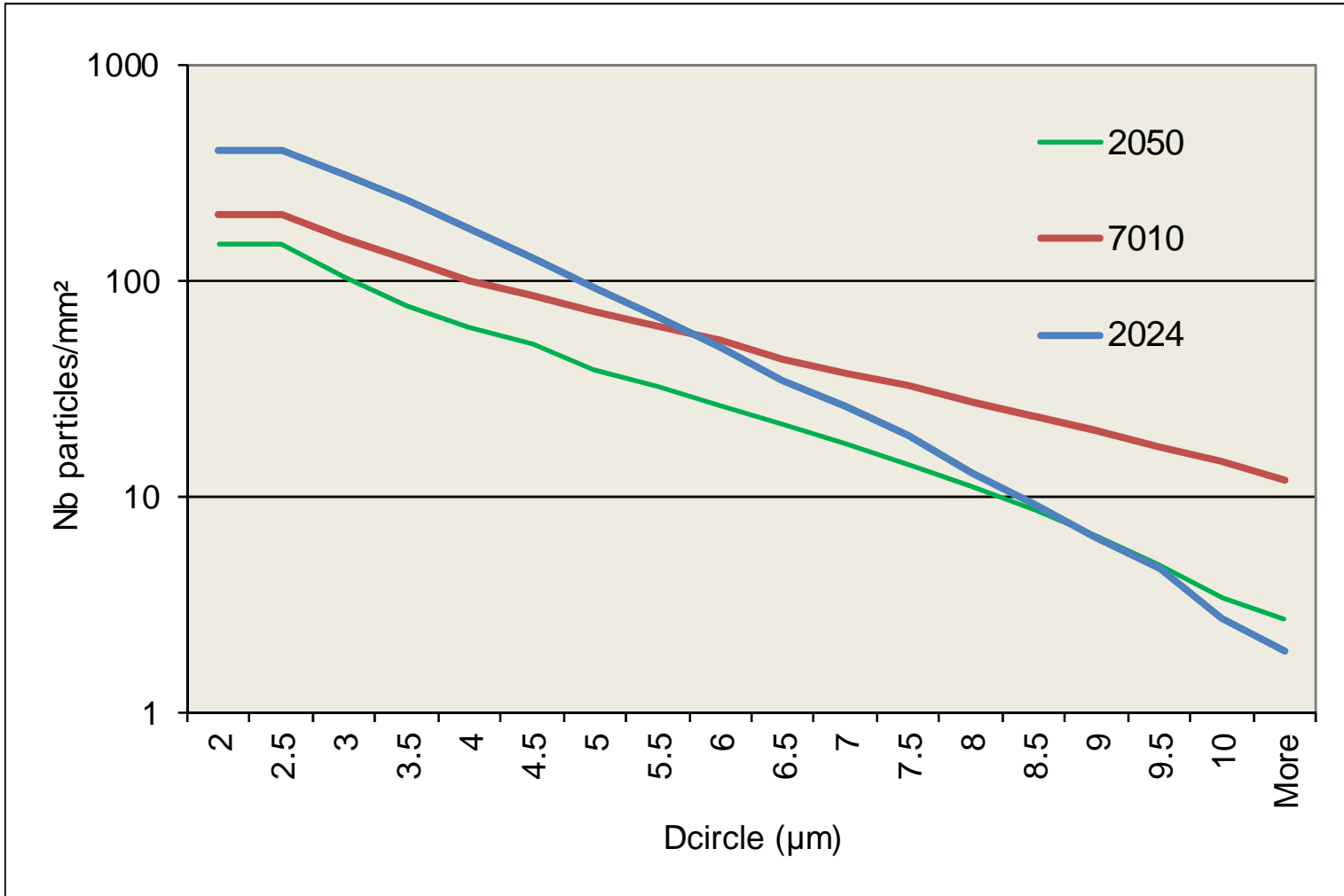
7010 T74 110 mm



2024 T3 30 mm

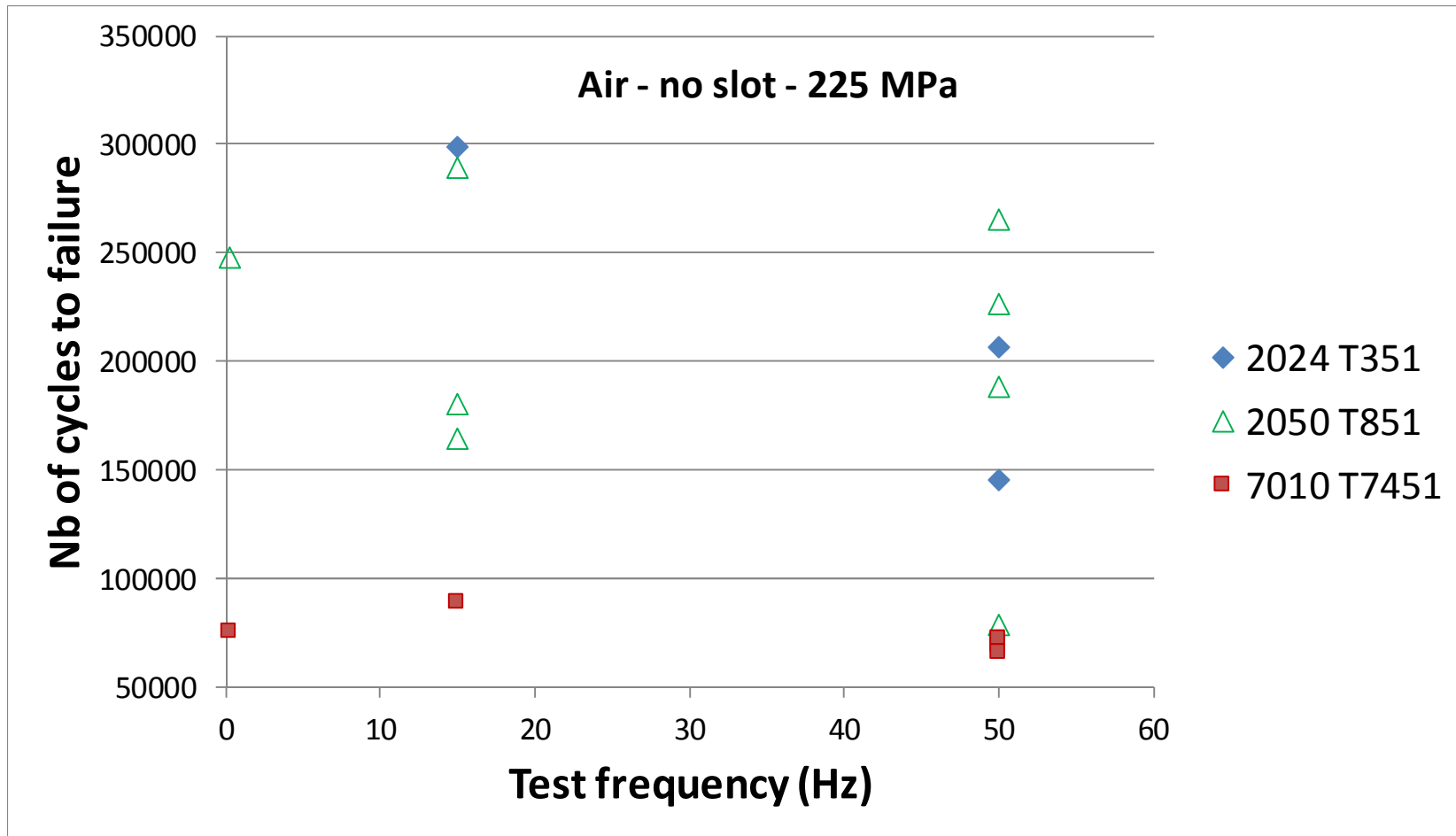


2050: less constituents > 7 microns than 7010

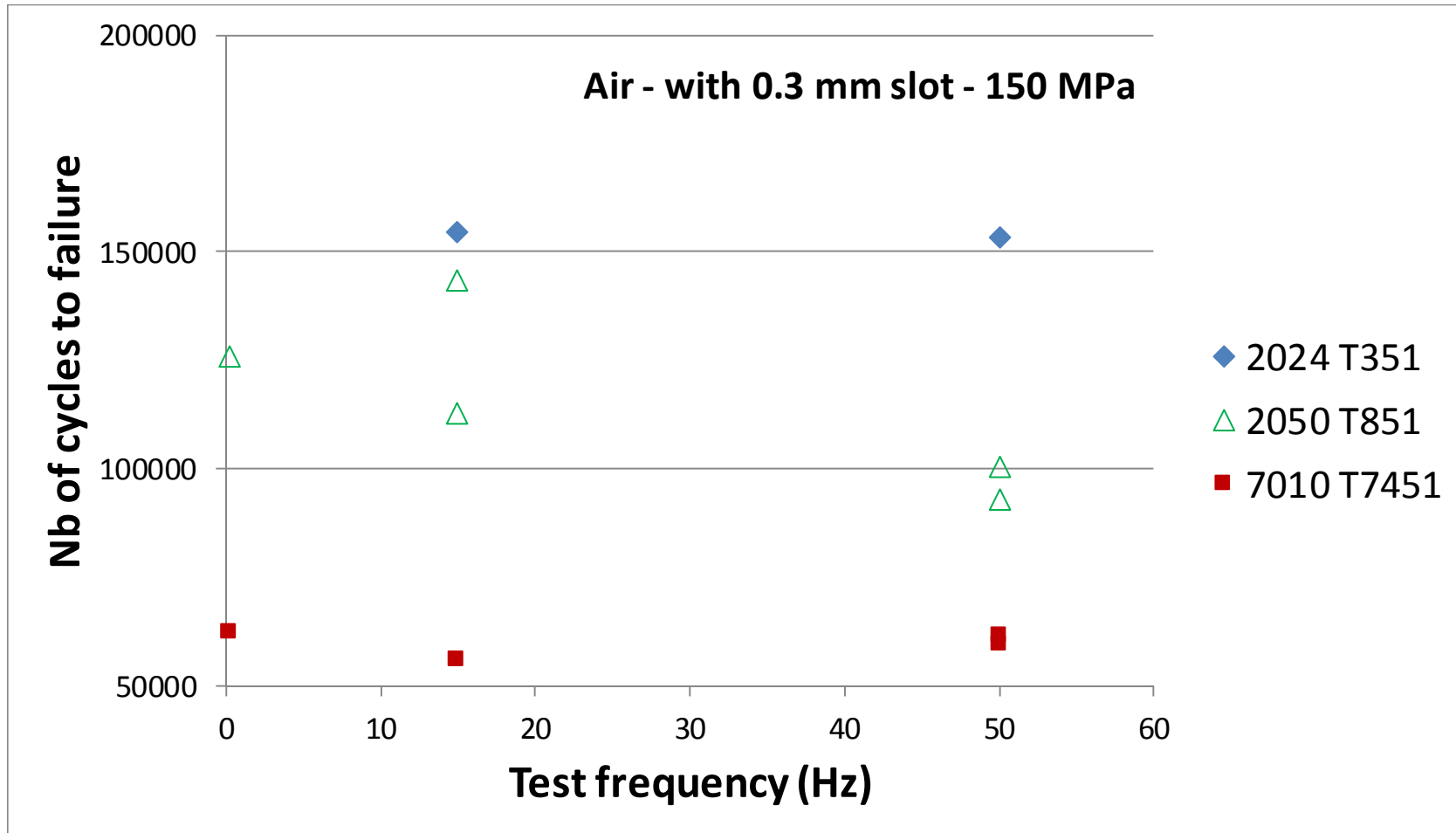


Air, no slot: 2050 ~ 2024 > 7010

■ No frequency effect



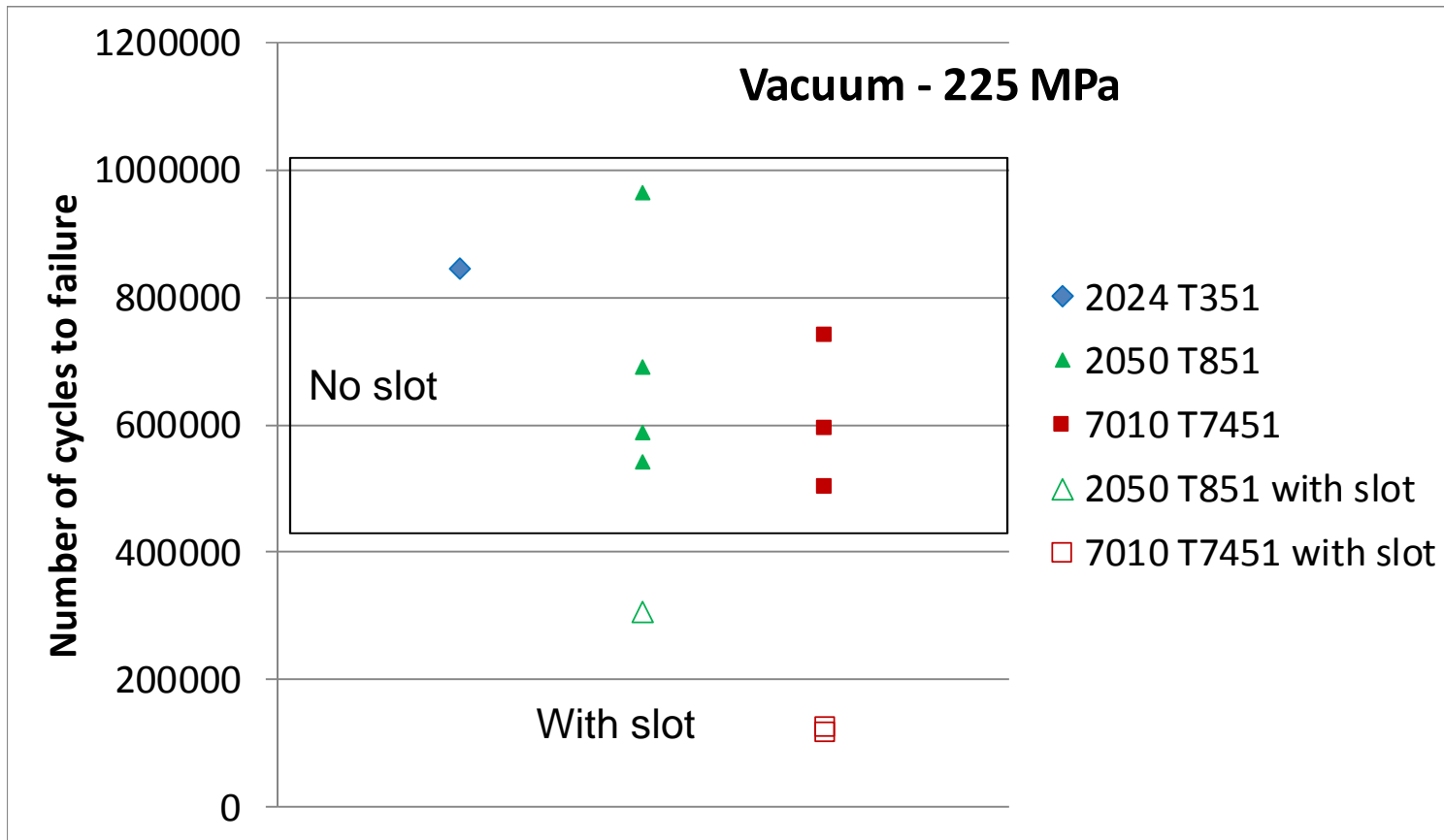
Air, with the slot: 2024 > 2050 > 7010



■ No frequency effect

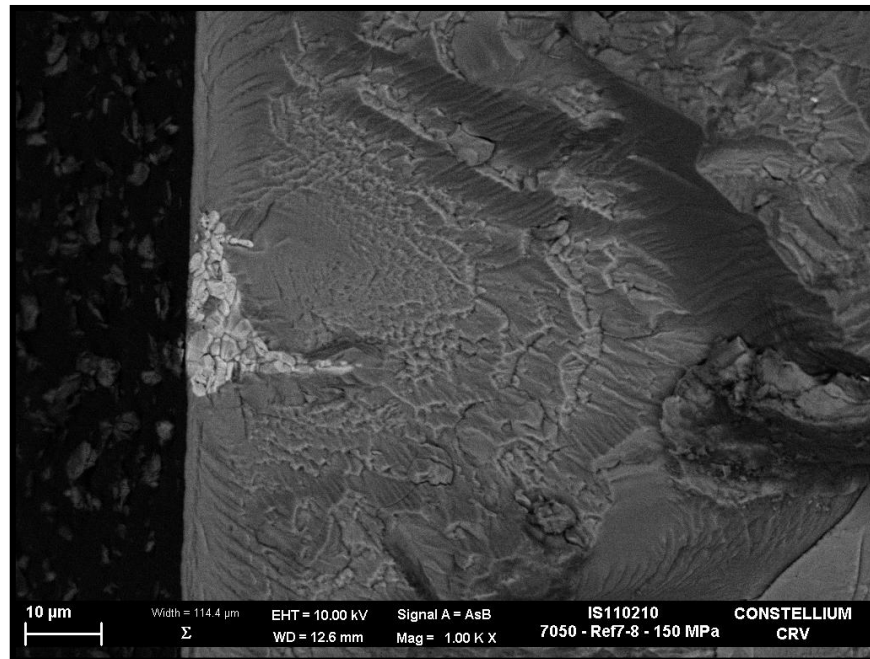
Vacuum, no slot: smaller difference between alloys

- No frequency effect

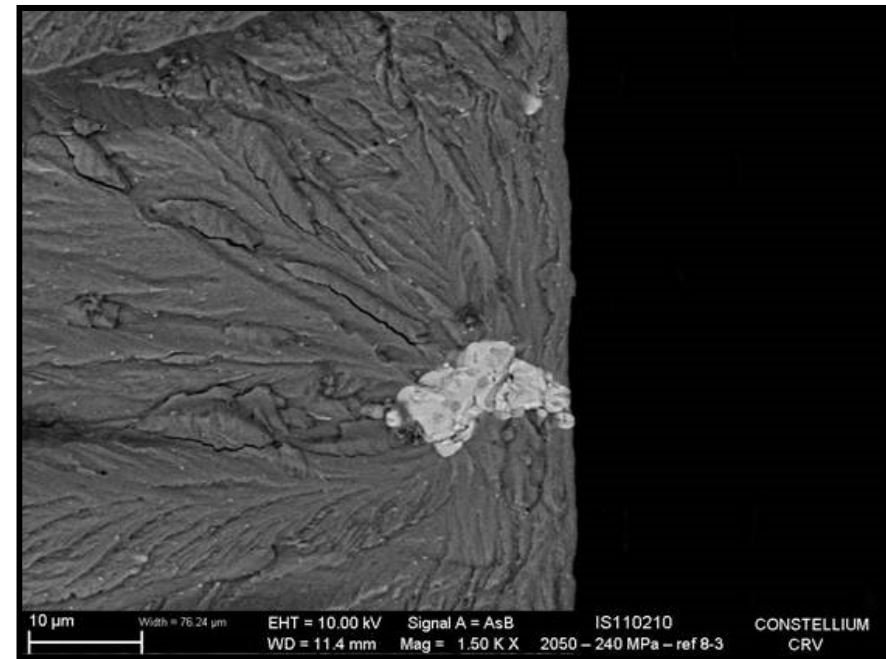


Most initiation occurs on constituent particles for 7050 (similar to 7010) and 2050

- Analysis of crack initiation by FEG-SEM (after failure)
- → Detection of the origin of fatigue failure
- → in most cases : presence of insoluble constituent particle



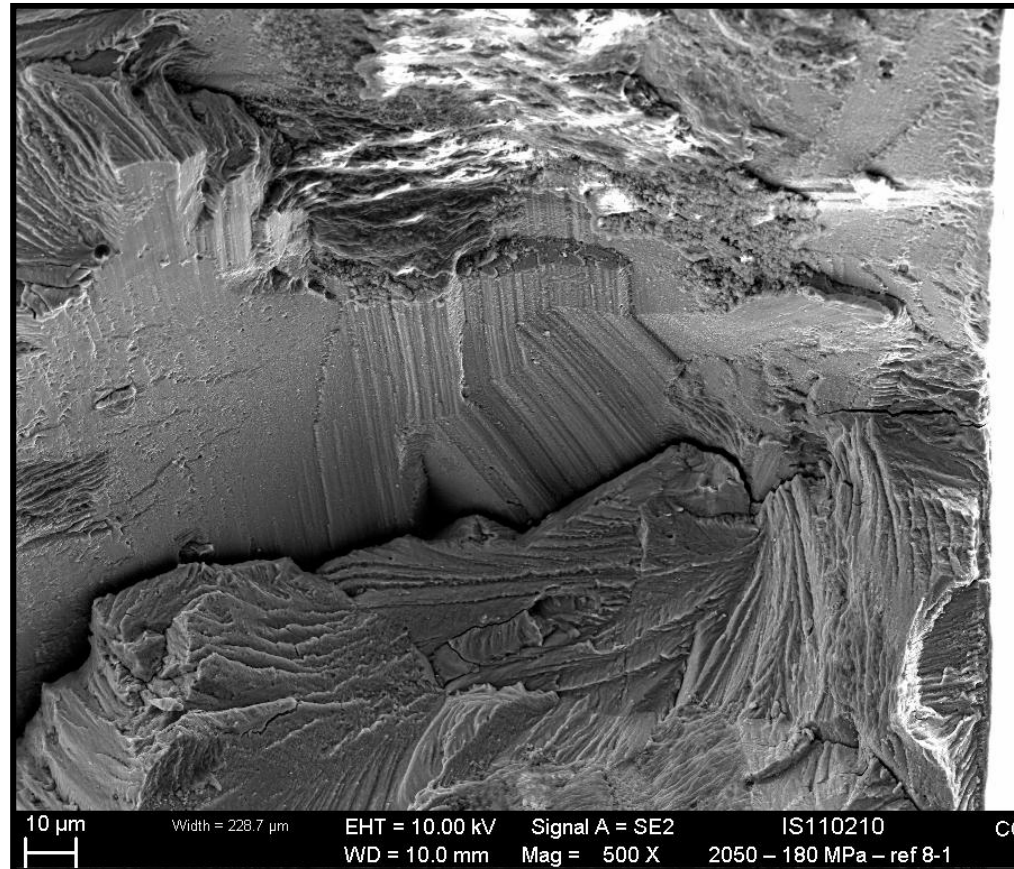
alloy 7050, 150MPa, 105986 cycles
 $\text{Al}_7\text{Cu}_2\text{Fe}$



alloy 2050, 220MPa, 32000 cycles
(Al, Cu, Fe, Mn) particle

Some initiation occurs on slip bands, for 2050-T8 only

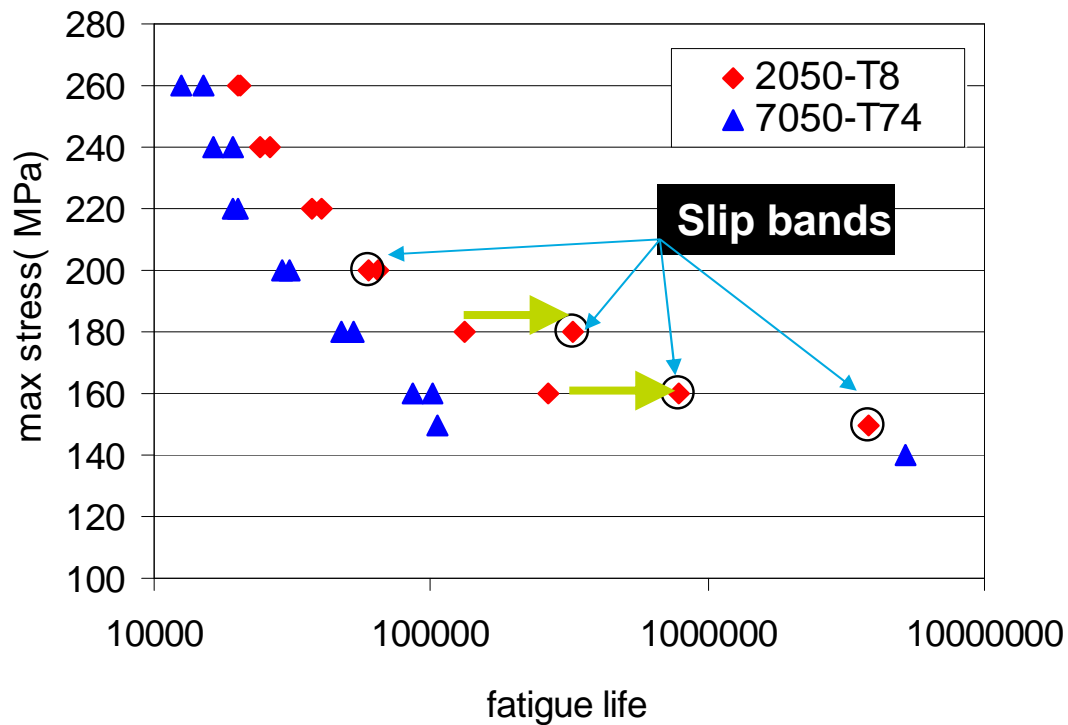
- Analysis of crack initiation by FEG-SEM (after failure)
 - ▶ At low stress level:
 - No constituent particle
 - Slip bands are present



Alloy 2050, 180MPa, 327960 cycles

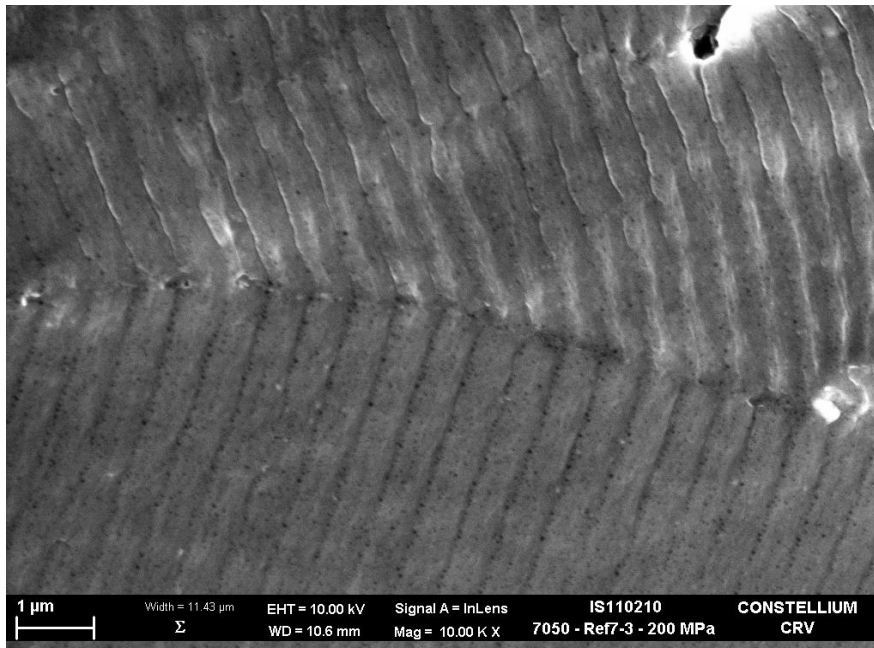
Initiation on slip bands corresponds to low stress level and high fatigue life

- FEG-SEM of fatigue initiation
 - ▶ Initiation on slip bands obtained only for 2050, for stress levels ≤ 200 MPa
 - ▶ The fatigue life is higher when initiation occurs on slip bands compared to initiation on constituent particles

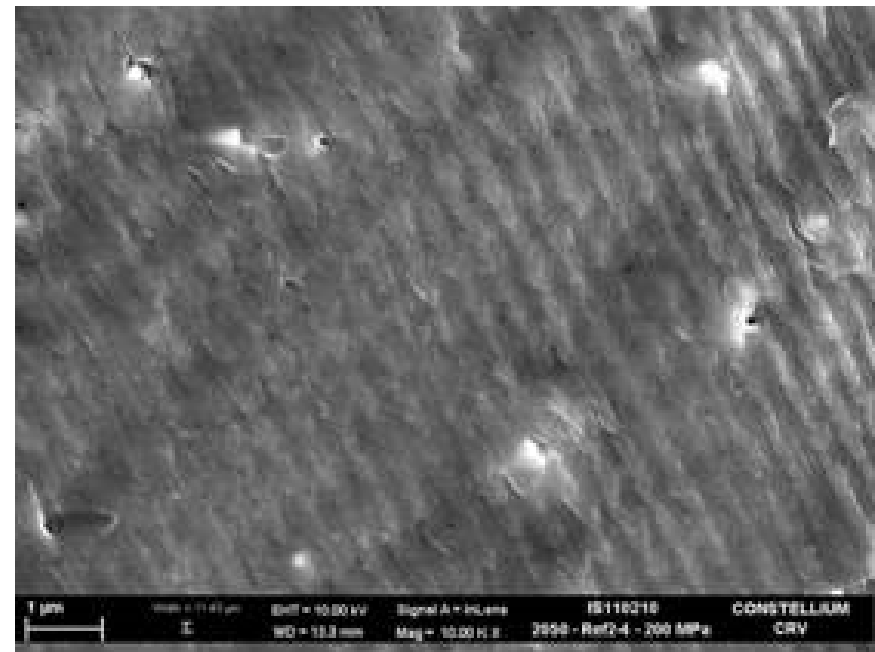


Inter-striation distance is higher for 7050 than for 2050

- Measure of inter-striation by FEG-SEM on failed samples at 1mm from the hole
- 1 striation = 1 cycle



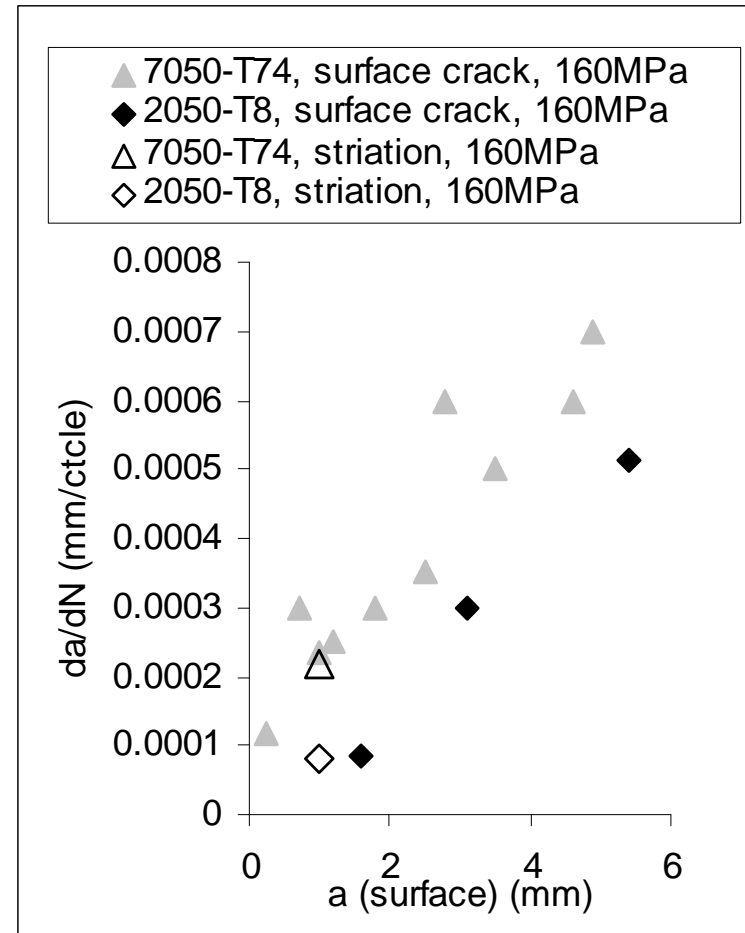
7050, 200MPa



2050, 200MPa

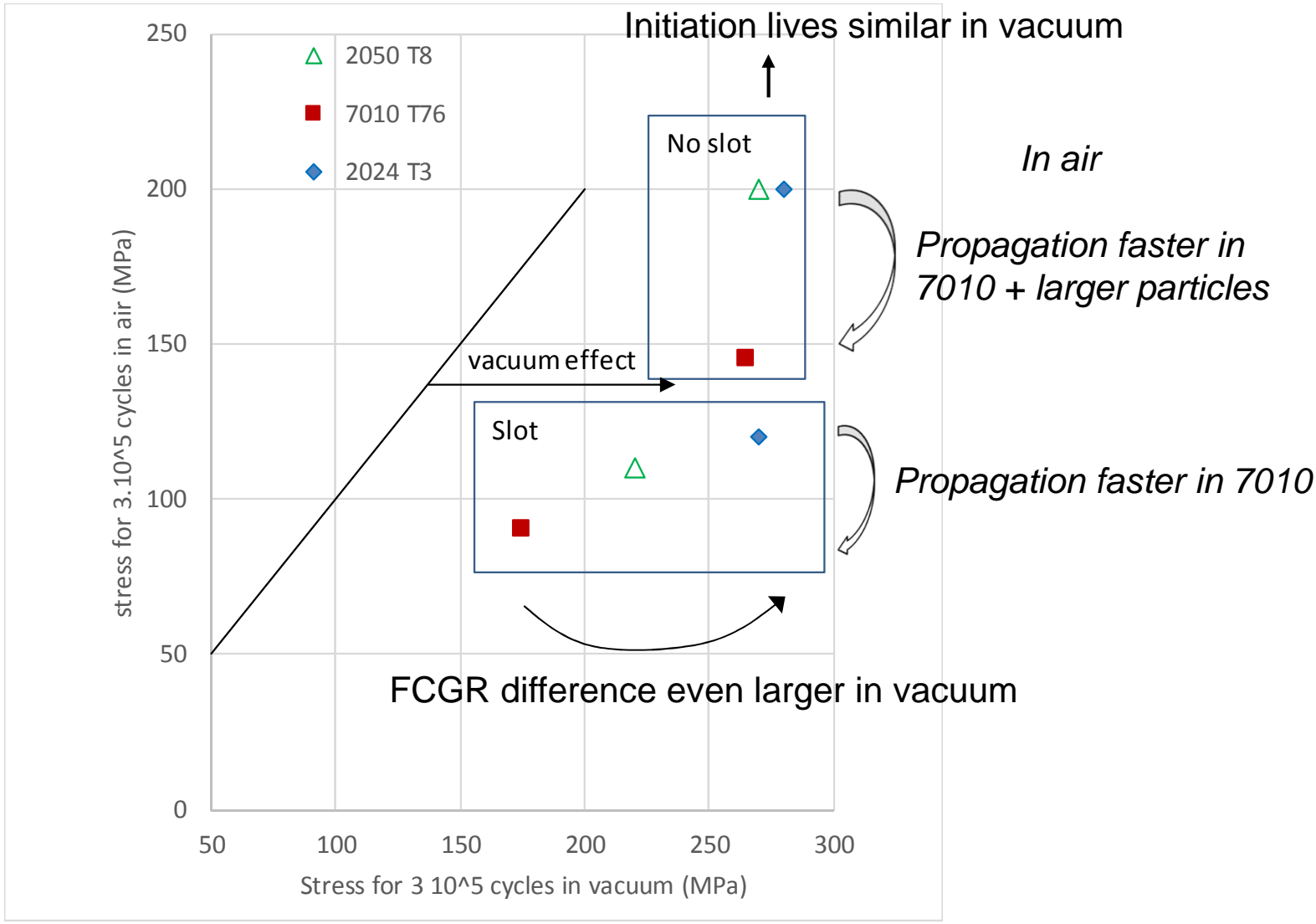
Striation distance is consistent with surface crack growth rate (\rightarrow slower rate for 2050)

- da/dN obtained by:
 - ▶ Measurement of small cracks by microscopy on the surface
 - ▶ Inter-striation distance on fractographs in the bulk
- For both methods:
 - ▶ da/dN (2050) < da/dN (7050)



Note: presentation as a function of a rather than ΔK avoids theoretical issues with K definition of small cracks in open hole specimens

2050 performance: slower FCGR, (smaller constituents)





Conclusion

- Al-Cu-Li alloys offer can fulfill the requirements on the whole aircraft
- Very high strength, higher than 7000 can be combined with 2000 type fatigue and damage tolerance properties
- Some very high damage tolerance versions show better DT than best conventional
- The effect of environment is significant and needed to understand the propagation behaviour
- Better fatigue properties than 7000 are mainly due to FCG improvement