

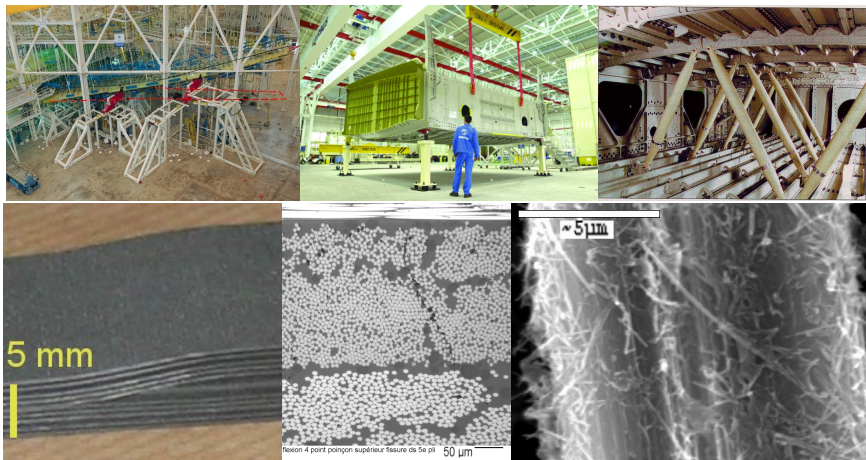
Aussois 2019  
21-25 janv. 2019

# Suivi de l'endommagement dans les composites par stéréo-corrélation d'images

J.-N. Périé, J.-C. Passieux

Institut Clément Ader (ICA), Université de Toulouse, CNRS/INSA/Mines Albi/UT3/ISAE, Toulouse, France

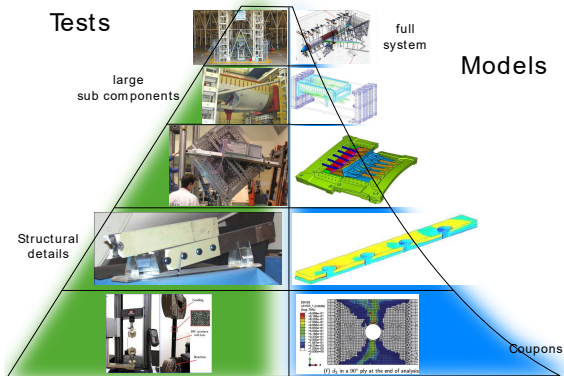


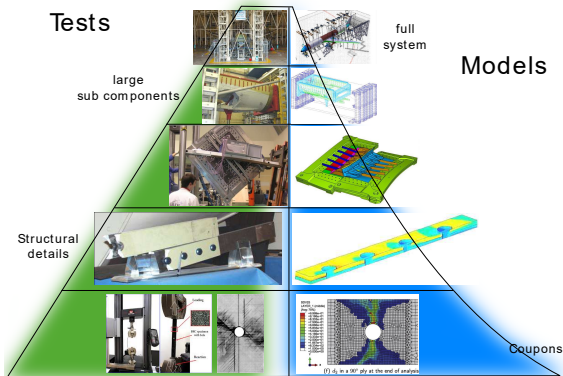


[Riccardis2006]

- Complex architecture, variabilities, defects, effect of manufacturing, etc.  
→ **the assessment and prediction of their behaviour is still a real challenge**







→ **More predictive models**

→ Images can be used to build more realistic models

→ X-ray  $\mu$  Computed Tomography can now provide a valuable insight at various scales

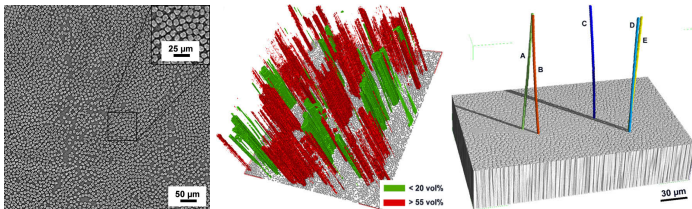


Figure: Fiber volume content and fiber orientation [Requena2009]

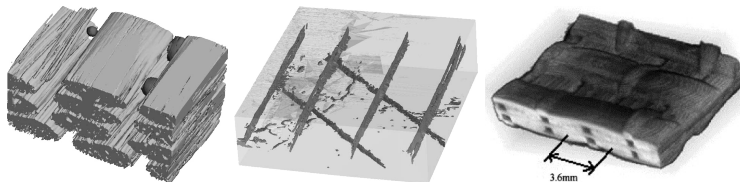
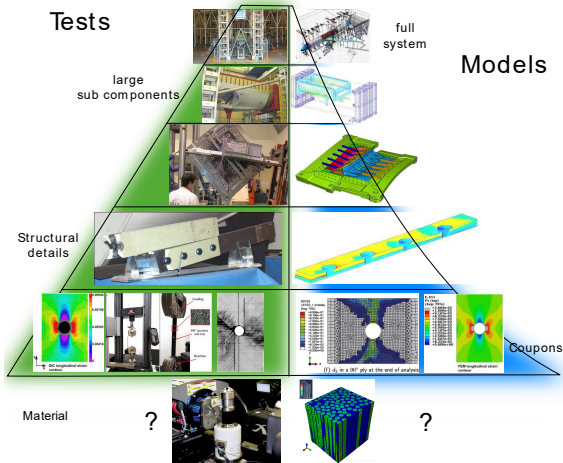
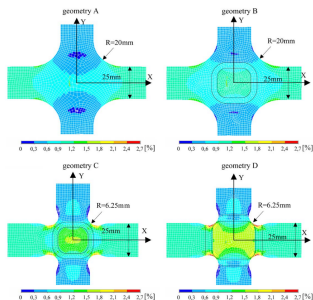


Figure: Defects and damages [Schilling2005] Geometry [Desplentere2005]

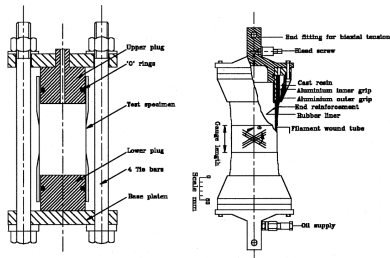


- More predictive models
  - Images can be used to propose more realistic models
- **More complex and well instrumented** experiments
  - DIC, stereo DIC and DVC can be used to measure kinematical fields

## More representative structure subjected to a multiaxial (and non-proportional) loading



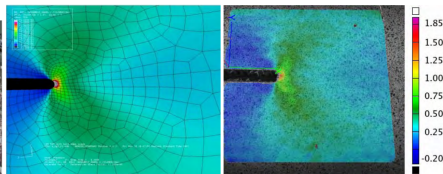
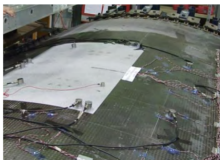
[Smits et al. 08]



[Soden et al. 02]

- Many specimens can be (easily?) manufactured and tested
- Loading is partly known (some components of the reactions) and may be used in a simulation/experiment dialog
- The specimen and the loading may not be representative of actual applications

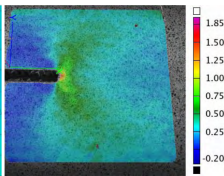
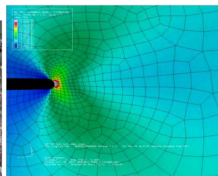
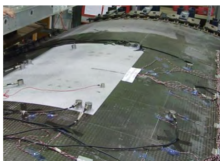
## Representative structure subjected to realistic loadings



[Leone et al. 08]

- Full scale specimens  
→ **Actual geometry**, material defects, residual stresses, etc.?
- Test bench is very specific  
→ **Actual boundary conditions and loading?**

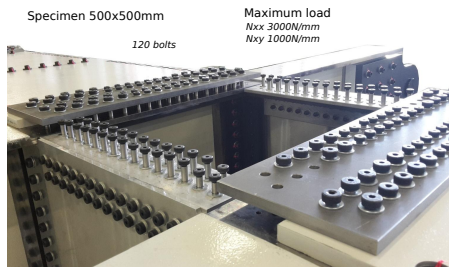
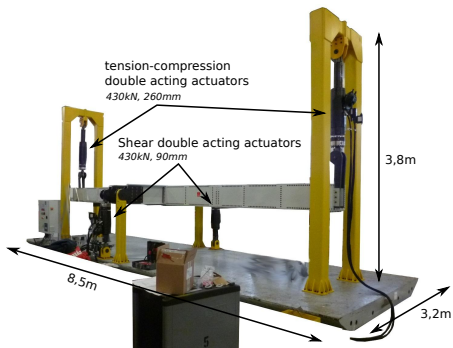
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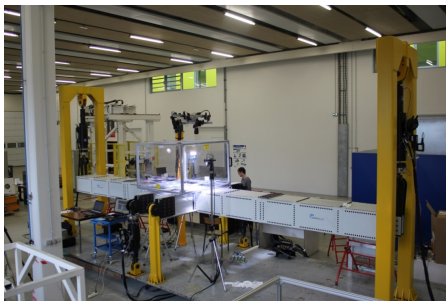
- Full scale specimens  
→ **Actual geometry**, material defects, residual stresses, etc.?
- Test bench is very specific  
→ **Actual boundary conditions and loading?**
- Digital Image Correlation is now widely used in such contexts to provide 3D information  
→ **Quantitative comparison of measured and simulated data?**  
→ **Small strains in comparison with "standard" DIC measurement uncertainties!**

- **VERTEX Project** (Funding: ANR-12-RMNP-0001 - More information: [web site](#))  
“Modelling and experimental validation of composite structures under complex loadings”
  - Partners: Airbus Group, Holo3, LMS Samtech Samcef  
ICA [Bouvet et al. 09] , LMT [Ladeveze et al. 05] , ONERA [Huchette et al. 06]
  - Our work package: **Stereo DIC instrumentation and control**

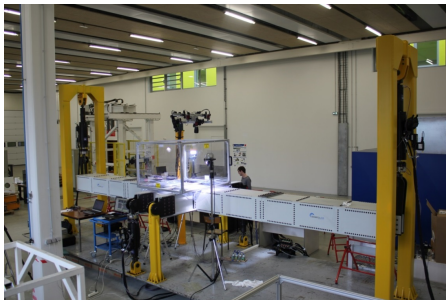




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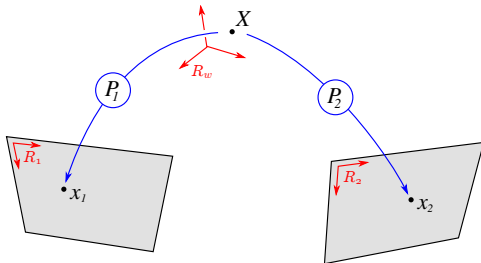


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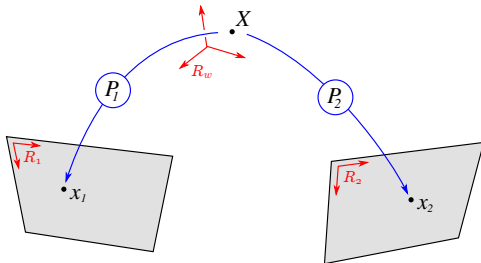


- **Non-conventional testing machine**
  - nonlinear transfer function (some parts of the machine may undergo plastification)
  - **Experiment:** how to control of the device to follow the **complex loading**?
  - **Validation:** Unknown (hyperstatic) loading conditions at the **FE model's** boundary

- Key features of the classical approach [Hartley 04, Sutton et al. 09]
  - nonlinear camera models  $x_c = P_c(X, p_c)$

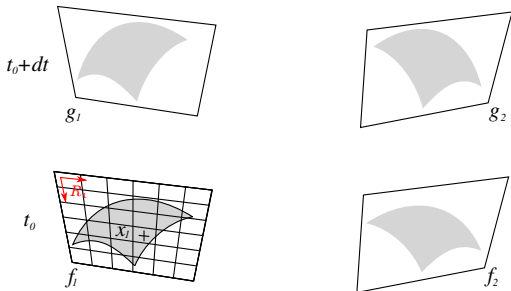


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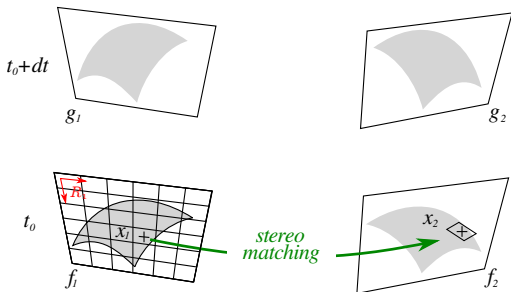


- **Calibration of the camera parameters  $p_c$**  [Lorusso et al. 97, Garcia and Orteu 01]
  - ⊗ **intrinsic** (focal length, image center, distortions) (considered offline)
  - ⊗ **extrinsic** (translations, rotations) (considered unknown)

- Displacement measurement with the classical approach

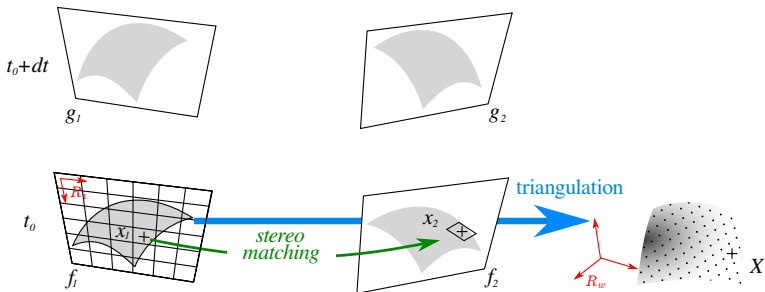


- Displacement measurement with the classical approach



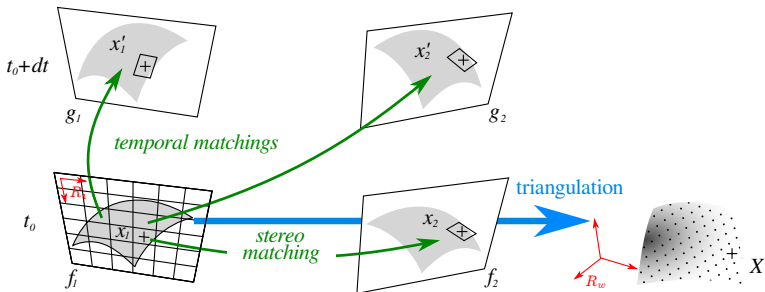
- **stereo matching** between reference images

- Displacement measurement with the classical approach



- o **stereo matching** between reference images
- o **triangulation**: reference shape  $X$

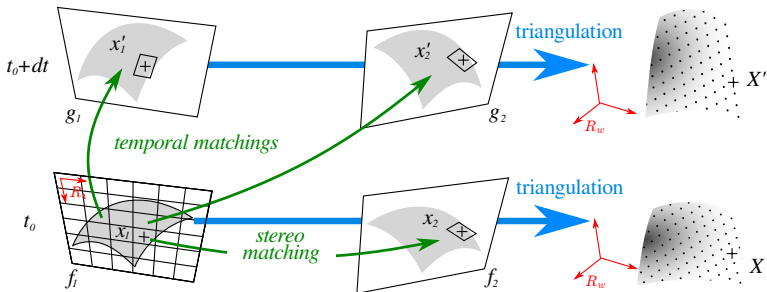
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- o **temporal matchings**: stereo matching points at  $t_0 + dt$

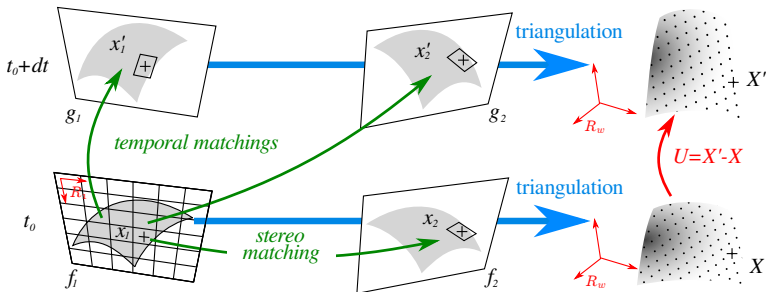


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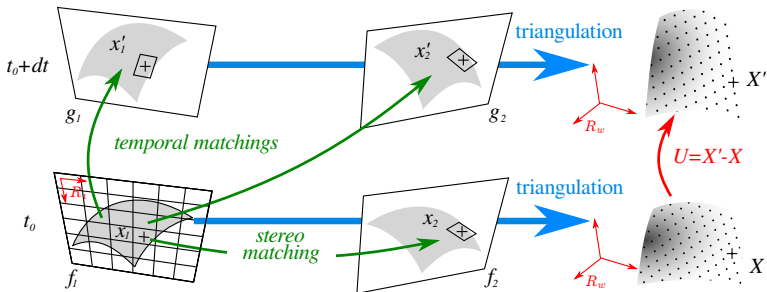
- o **stereo matching** between reference images
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- o **triangulation**: new shape  $X'$

- Displacement measurement with the classical approach



- o **temporal matchings** between reference images
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- o **displacement estimation**

## • Displacement measurement with the classical approach

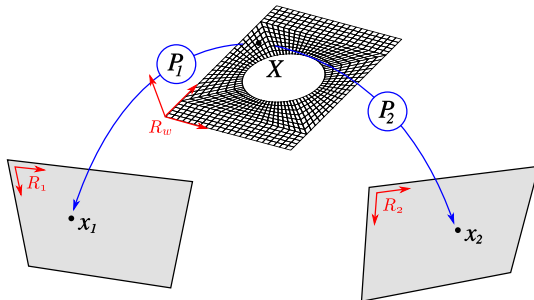


- **stereo matching** between reference images
- **triangulation**: reference shape  $X$
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- **triangulation**: new shape  $X'$
- **displacement estimation**

## • Limitations:

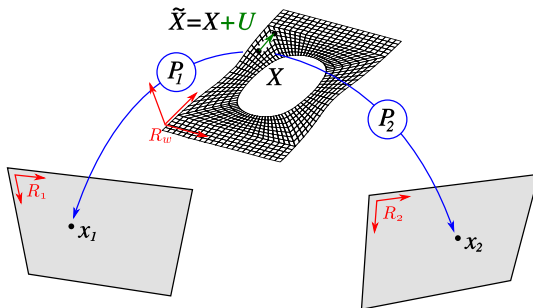
- Dissymmetric **master-slave** formulation
- Works in the **image coordinate system**, unit: pixel
- Displacement  $U$  **not** the solution of a **unique optimization process**

- Displacement measurement [Pierré et al. 17]



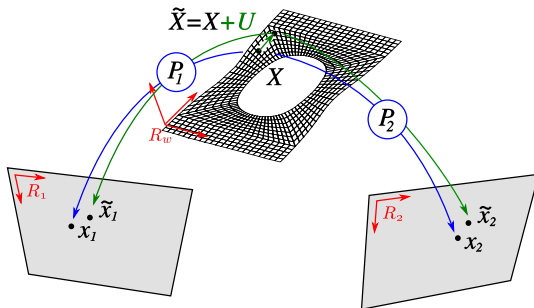
[Pierré et al. 17] Pierré, Passieux and Périé (2017). Finite Element Stereo Digital Image Correlation: framework and mechanical regularization. *Experimental Mechanics*. 53(7)443-456.

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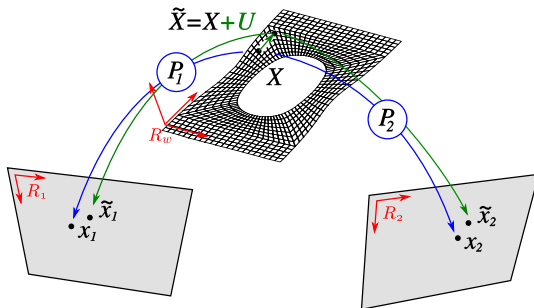
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Matching + Triangulation on the 3D displacement  $\mathbf{U}$ :

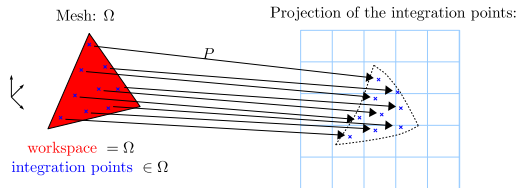
$$\mathbf{U}^* = \arg \min_{\mathbf{U}} \sum_c \int_{\Omega} \left[ f_c(\underbrace{\mathbf{P}_c(\mathbf{X})}_{\mathbf{x}_c}) - g_c(\underbrace{\mathbf{P}_c(\mathbf{X} + \mathbf{U}(\mathbf{X}))}_{\tilde{\mathbf{x}}_c}) \right]^2 d\mathbf{X}$$

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## Quadrature [Pierré et al. 16]

- Need to define a quadrature rule in the world coordinate system.

### Mesh Based Quadrature

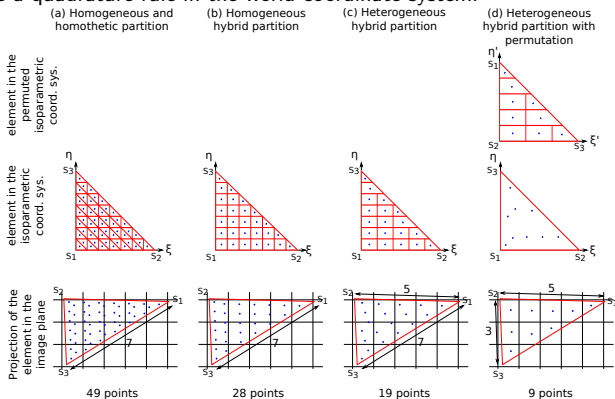


[Pierré et al. 16] Pierré, Passieux, Périé, Bugarin and Robert (2016) Unstructured Finite Element-based Digital Image Correlation with enhanced management of quadrature and lens distortions *Optics and Lasers in Engineering* 77, 44-53.



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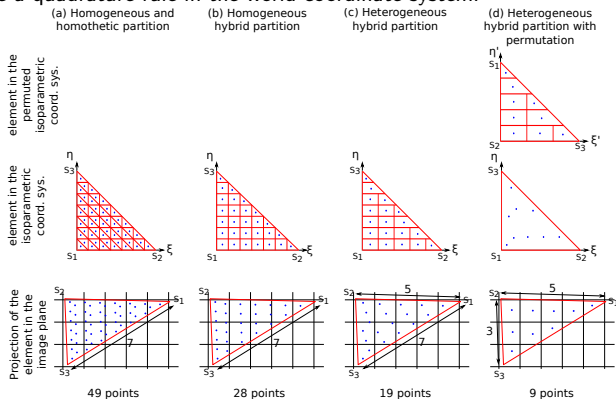
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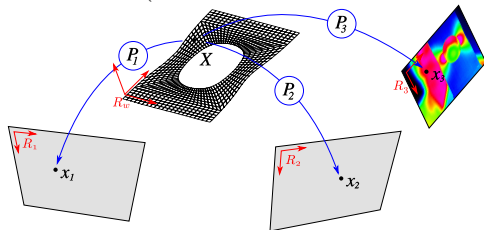
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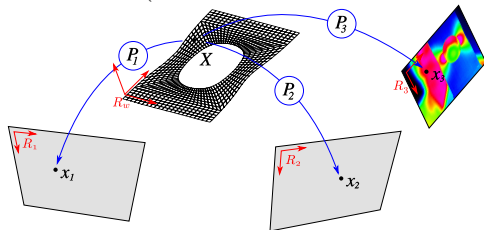
→ Proved to be optimal and also relevant for 2D-DIC...

[Pierré et al. 16] Pierré, Passieux, Périé, Bugarin and Robert (2016) Unstructured Finite Element-based Digital Image Correlation with enhanced management of quadrature and lens distortions *Optics and Lasers in Engineering* 77, 44-53.

- Advantages of using finite elements in SDIC:
  - No master-slave structure: no constraints on the number of camera
  - Works in the **CAD coordinate system**, units: m
  - Convenient for the user (link with analysis, validation, identification...)
  - 3D surface displacement reduced to a **unique optimisation problem**
  - Space-time regularization [Passieux et al. 18]
  - **General framework for data fusion** (IR camera [Charbal et al. 16] , acoustic emissions...)



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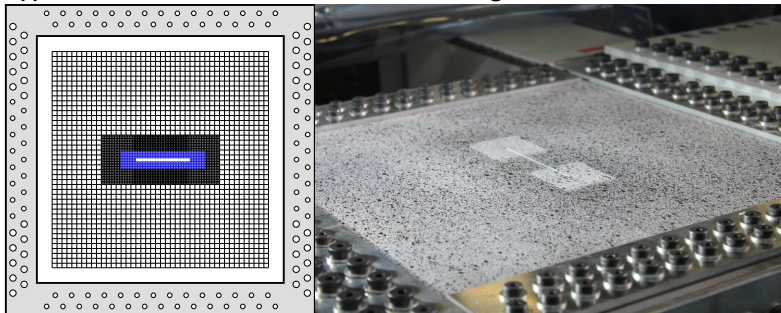


- **Today's presentation.**

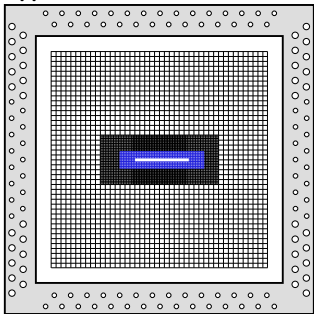
1. Applied to multiscale/multiview measurements [Serra et al. 2017]
2. Mechanical regularization [Pierré et al. 17, Serra et al. part I 2017]
3. Identification of kinematic boundary conditions [Serra et al. part I 2017]
4. Towards validation of composite structures [Serra et al. part II 2017]

## 1. Multiscale/multiview measurements (Application to Vertex)

## Application within the context of structural testing

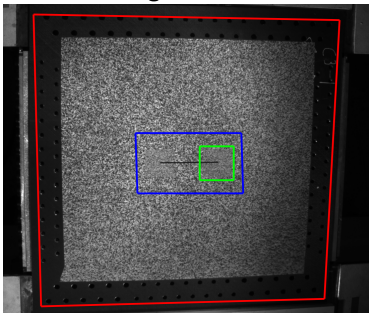
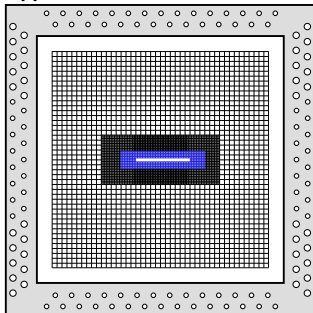


## Application within the context of structural testing



- The proposed framework can handle as many cameras as needed

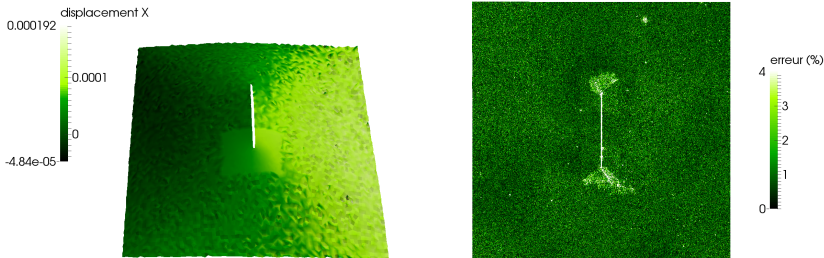
## Application within the context of structural testing



- The proposed framework can handle as many cameras as needed
  - **Allows using actual simulation meshes for Stereo FE DIC measurements**
  - **A suitable speckle is synthetised and printed onto the surface**

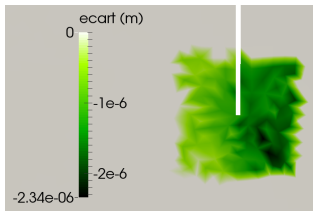
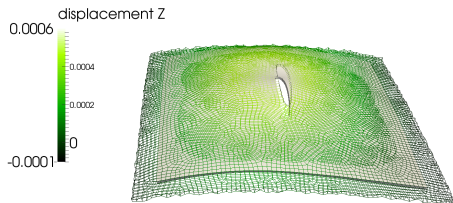


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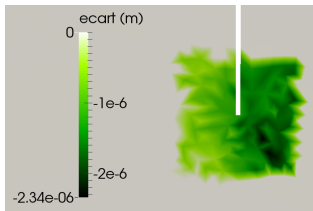
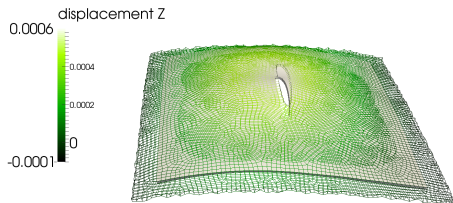
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- Gray level residual map reveals cracks

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- Stereo FE-DIC makes simulation/experiment dialog much easier

## Application within the context of structural testing

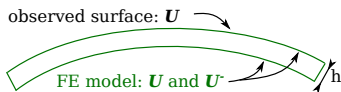


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- BCs? ← **mechanical regularisation of FE stereo measurements**

## 2. Mechanical Regularization

## Displacement measurement with mechanical regularisation

- Solid Shell model :



$$\begin{bmatrix} U_x \\ U_y \\ U_z \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} U_x \\ U_y \\ U_z \\ U_x^- \\ U_y^- \\ U_z^- \end{bmatrix}$$

## Displacement measurement with mechanical regularisation

- Solid Shell model :

observed surface:  $U$

FE model:  $U$  and  $\bar{U}$

$$\begin{bmatrix} U_x \\ U_y \\ U_z \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} U_x \\ U_y \\ U_z \\ U_x^- \\ U_y^- \\ U_z^- \end{bmatrix}$$

- Plate/Shell model :

observed surface

FE model:  $V$  and  $\theta$

$$\begin{bmatrix} U_x \\ U_y \\ U_z \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & \frac{h}{2} & 0 \\ 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} V_x \\ V_y \\ V_z \\ \theta_x \\ \theta_y \end{bmatrix}$$

## Displacement measurement with mechanical regularisation

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observed surface:  $U$

FE model:  $U$  and  $\bar{U}$

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- Plate/Shell model :

observed surface

FE model:  $V$  and  $\theta$

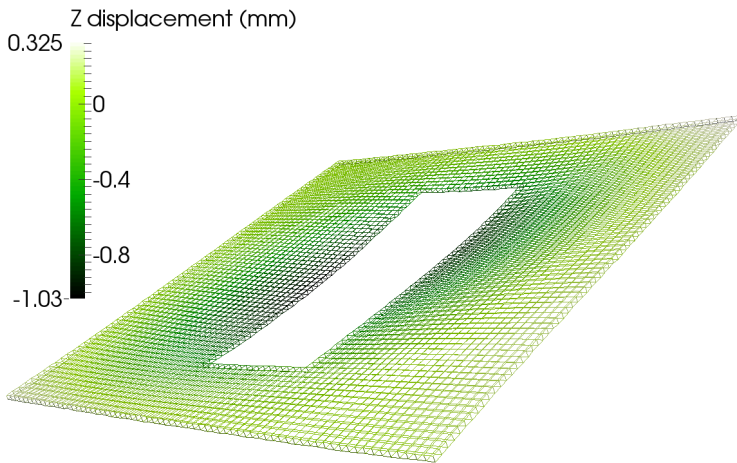
$$\begin{bmatrix} U_x \\ U_y \\ U_z \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & \frac{h}{2} & 0 \\ 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & \frac{h}{2} \end{bmatrix} \begin{bmatrix} V_x \\ V_y \\ V_z \\ \theta_x \\ \theta_y \end{bmatrix}$$

- Regularised DIC formulation [Rethore, Roux, Hild 08] [Leclerc et al. 10]

$$\mathbf{V}^* = \arg \min_{\mathbf{V}} \sum_c \int_{\Omega} \left[ f_c(\mathbf{P}_c(\mathbf{X})) - g_c(\mathbf{P}_c(\mathbf{X} + \Pi \mathbf{V}(\mathbf{X}))) \right]^2 d\mathbf{X} + \lambda_k \|\bar{\mathbf{K}}\mathbf{V}\|_2^2 + \lambda_T \|\mathbf{T}\mathbf{V}\|_2^2$$

# Example

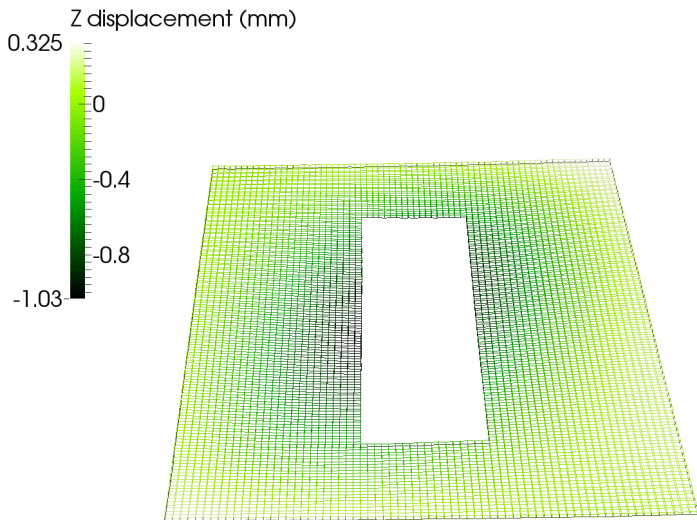
Measurement of mechanically consistent BC during a shear test





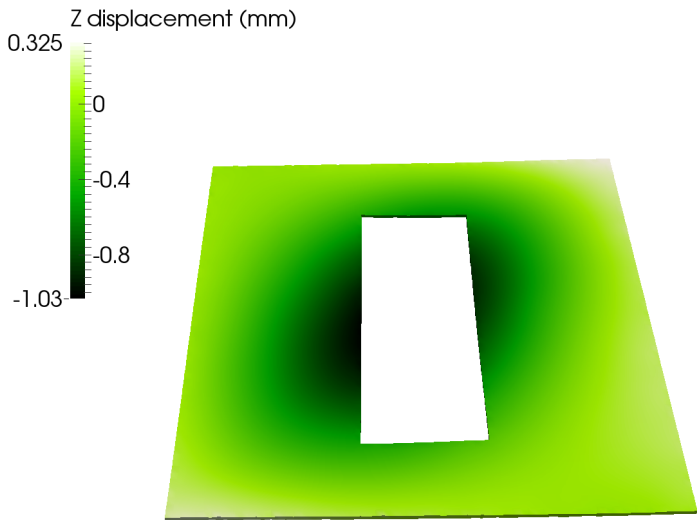
# Example

Measurement of mechanically consistent BC during a shear test



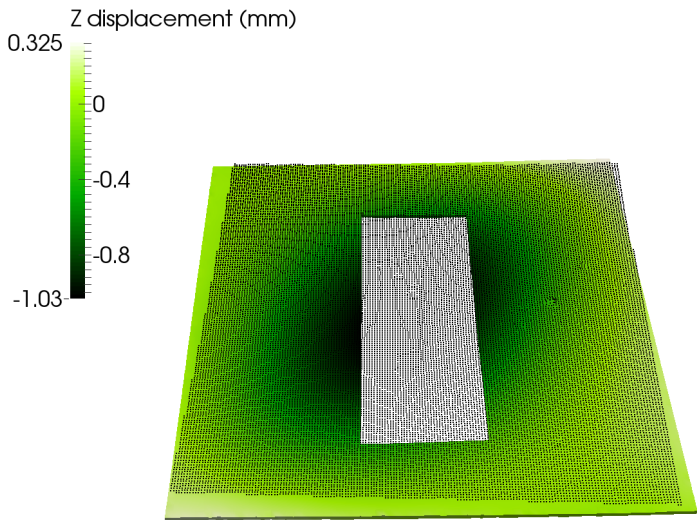
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Measurement of mechanically consistent BC during a shear test



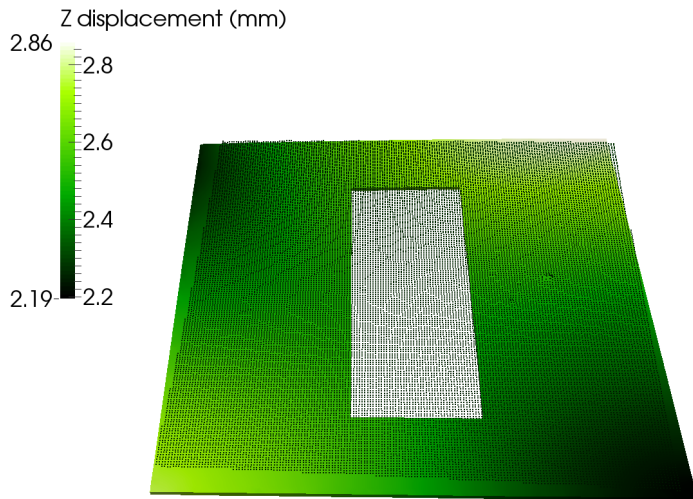
# Example

Measurement of mechanically consistent BC during a shear test



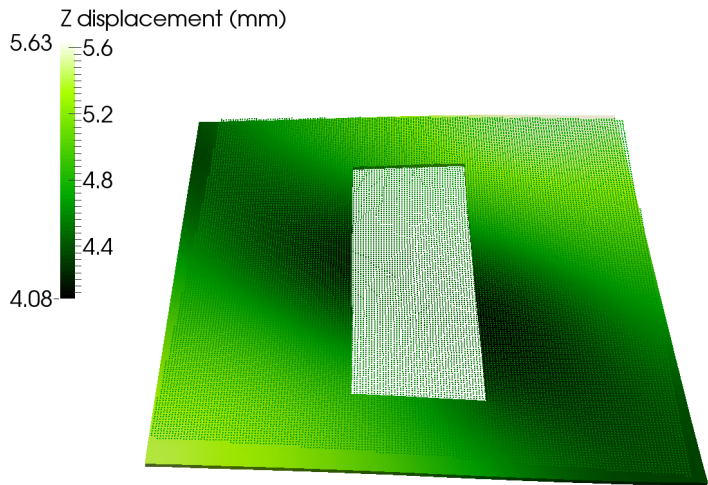
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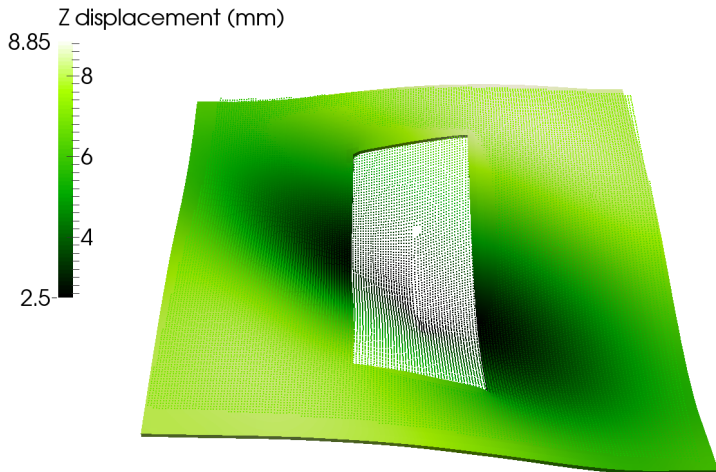
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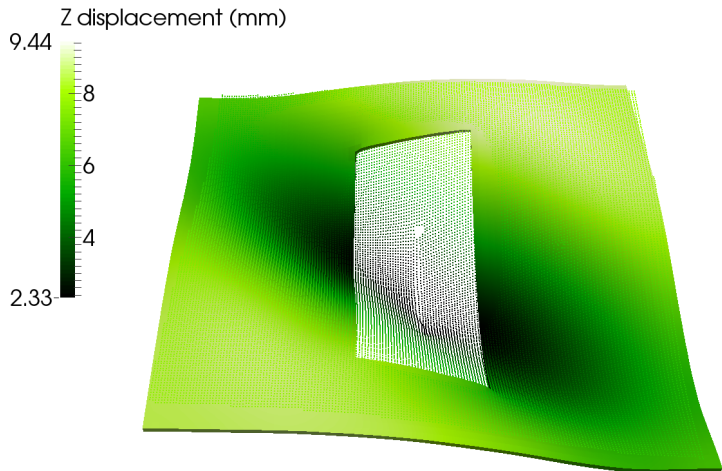
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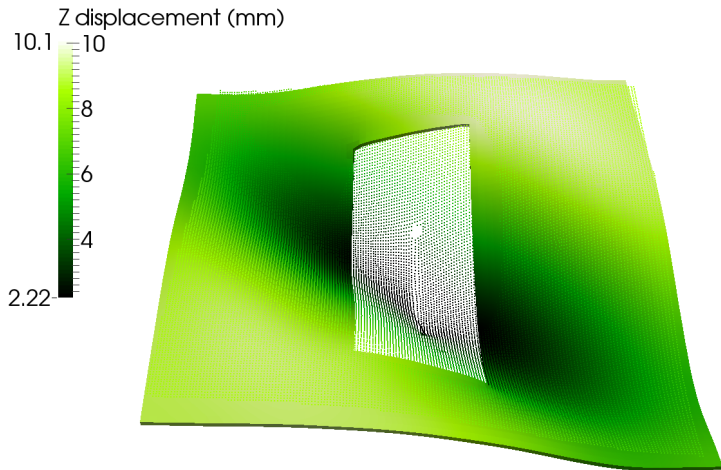
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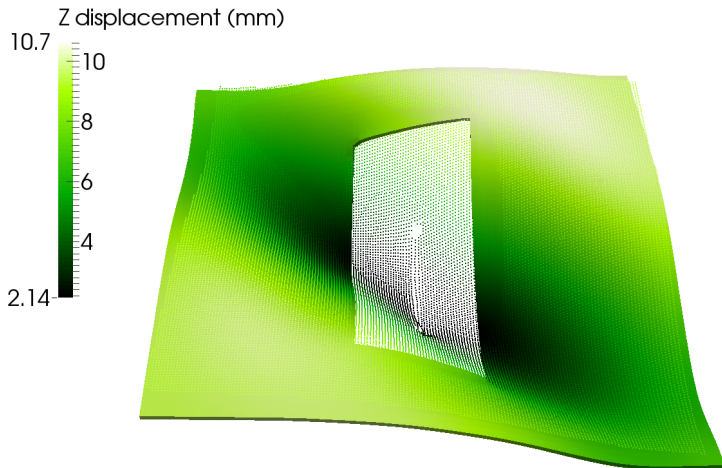
Measurement of mechanically consistent BC during a shear test





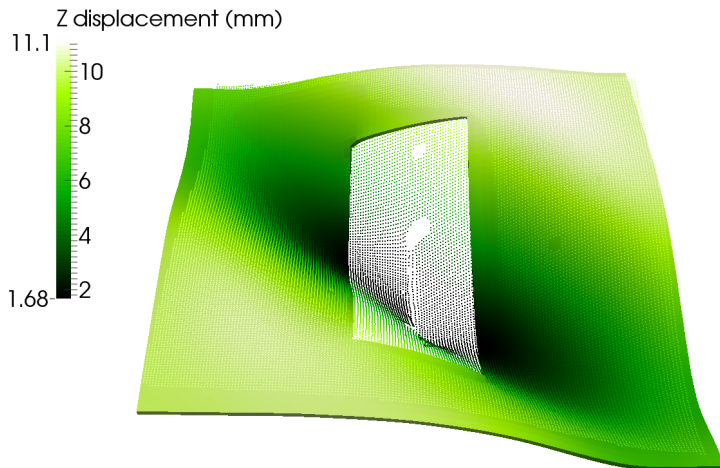
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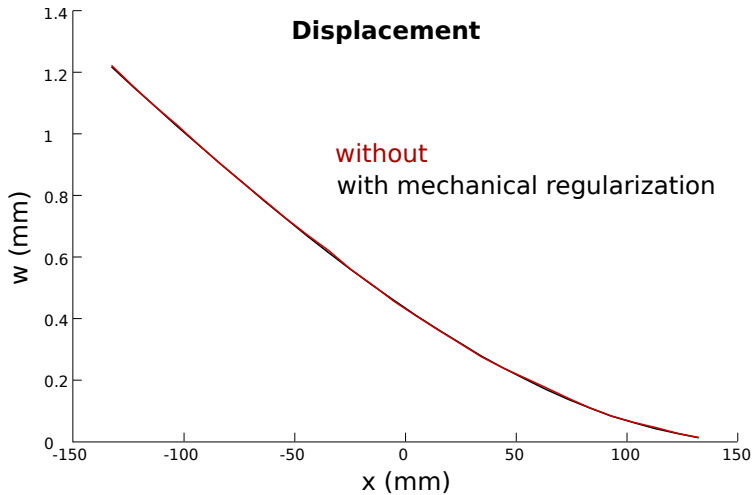


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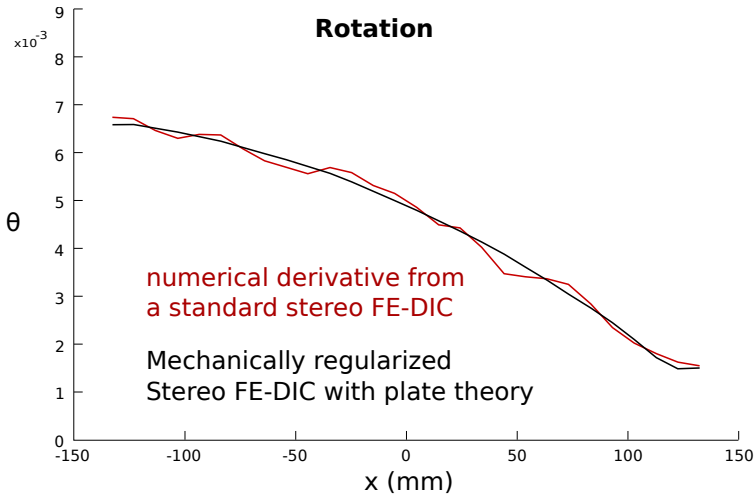
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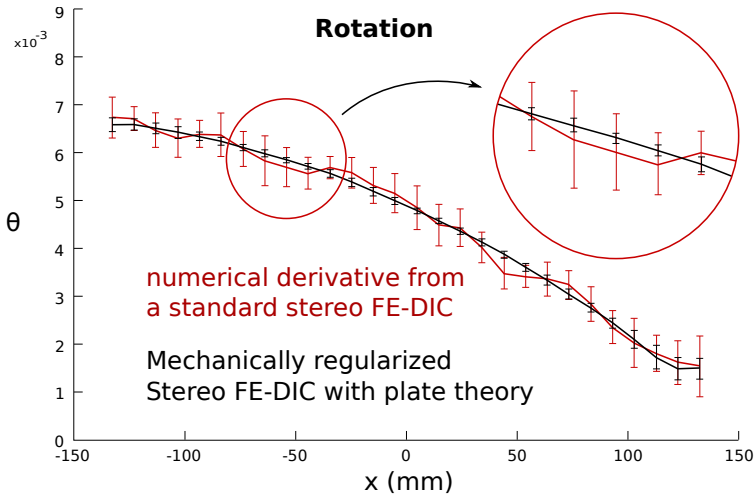
- Illustration on a simple test case of a plate in bending



- Illustration on a simple test case of a plate in bending



- Illustration on a simple test case of a plate in bending



### 3. Identification of Boundary Conditions in Stereo DIC (Application to Vertex)

- Assume that we have a reliable constitutive model far from the central notch.

$$Kq = f$$

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$$\mathbf{K}\mathbf{q} = \mathbf{f}$$

- renumber the dofs:

$$\begin{pmatrix} \mathbf{K}_{ii} & \mathbf{K}_{ib} \\ \mathbf{K}_{bi} & \mathbf{K}_{bb} \end{pmatrix} \begin{pmatrix} \mathbf{q}_i \\ \mathbf{q}_b \end{pmatrix} = \begin{pmatrix} 0 \\ \mathbf{f}_b \end{pmatrix} \Rightarrow \mathbf{q}_i = -\mathbf{K}_{ii}^{-1}\mathbf{K}_{ib}\mathbf{q}_b$$



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- building an operator:

$$\mathbf{q} = \mathbf{L}\mathbf{q}_b \quad \text{with} \quad \mathbf{L} = \begin{pmatrix} -\mathbf{K}_{ii}^{-1}\mathbf{K}_{ib} \\ \mathbf{I} \end{pmatrix}$$

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- Resolution of the DIC problem in projection on this basis

$$\mathbf{v}_b^* = \arg \min_{\mathbf{v}_b} \sum_c \int_{\Omega} \left[ f_c(\mathbf{P}_c(\mathbf{X})) - g_c(\mathbf{P}_c(\mathbf{X} + \Pi \mathbf{L} \mathbf{v}_b)) \right]^2 d\mathbf{X}$$

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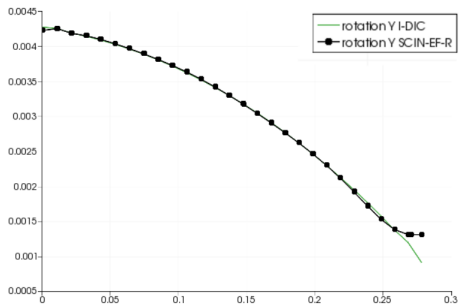
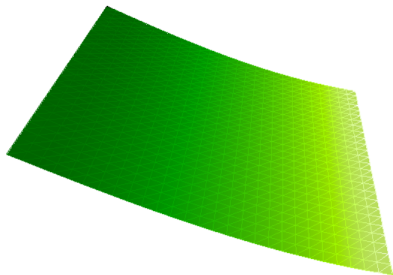
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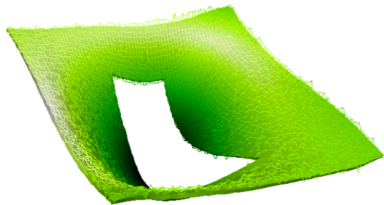
- Resolution of the DIC problem in projection on this basis

$$\left(\mathbf{L}^T \mathbf{M}_{sdic} \mathbf{L}\right) \mathbf{q}_b = \mathbf{L}^T \mathbf{b}$$

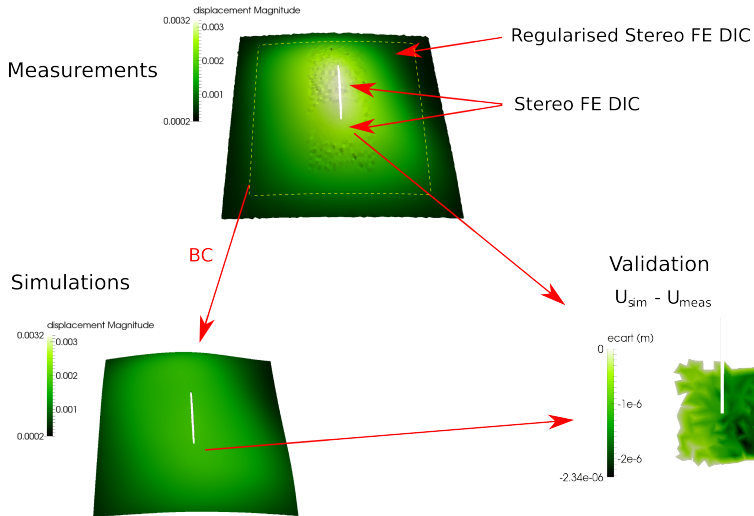
# Identification of boundary conditions



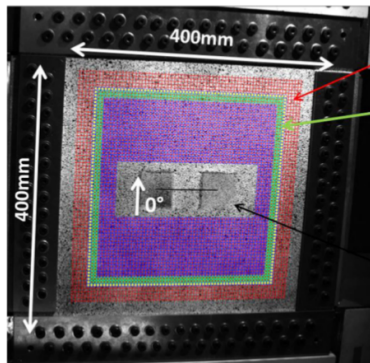
# Identification of boundary conditions



#### 4. Toward validation of non-linear models at the structural scale



- ICA's Discrete Ply Model [Bouvet et al, 09, Serra et al. 17]



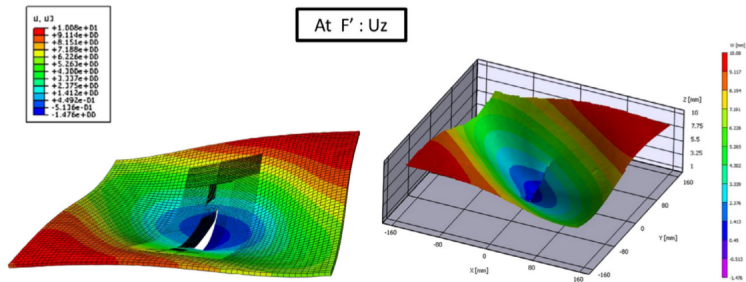
Zone ( $350 \times 350 \text{mm}^2$ ) far from bolted area where DIC is applied

Zone ( $300 \times 300 \text{mm}^2$ ) modeled by Abaqus with boundary conditions provided by FE-DIC  
In-plane and out-of-plane displacement imposed on a band of three elements

Zone not modeled by FE-SDIC (only DPM)



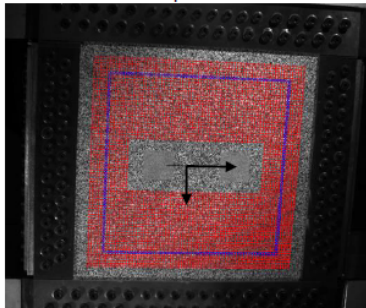
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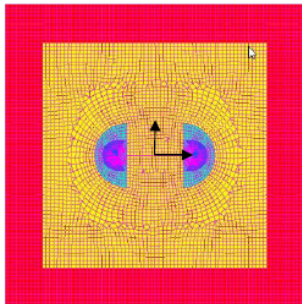
# Example of Damage Mesomodel

- Samtech implementation of LMT's Damage mesomodel [Lubineau and Ladevèze 08]  
[Courtesy of SIEMENS]

Plaque en essais

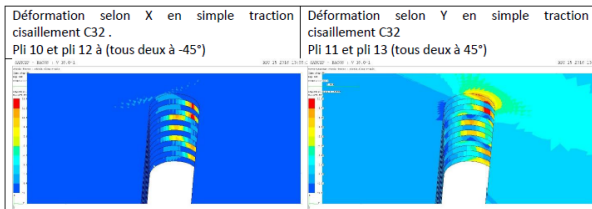
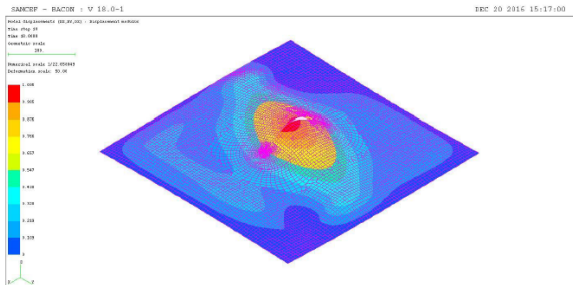


Modèle SAMCEF



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## Advantages of a formulation in the world coordinate system (FE-SDIC)

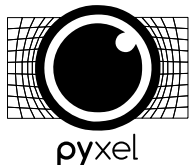
- A **convenient framework** for dialog with FE simulation (validation, identification)
- No master-slave structure: No restriction on the **number and the type of cameras**
- Possibility to incorporate the **knowledge of a model** (regularization, BC identification...)
- Open the way for **space-time formulations**
- A good formalism to incorporate **heterogeneous sensors**

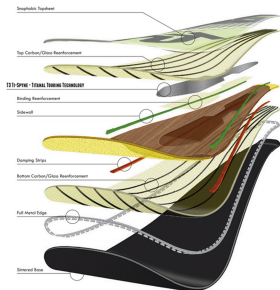
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- Open the way for **space-time formulations**
- A good formalism to incorporate **heterogeneous sensors**

## Perspectives

- Identification of elastic parameters of the models (loading assessment)
- Better consideration of **test history**
- **Validation** of non-linear FE models
- Possible **update** of constitutive parameters
- A **free FE-DIC Python library** available





Thank You

