

# Homogénéisation : les **microstructures** ont-elles leur mot à dire ?

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Colloque MECAMAT “Homogénéisation du comportement mécanique des matériaux hétérogènes”, Aussois, 27-31 janvier 2025

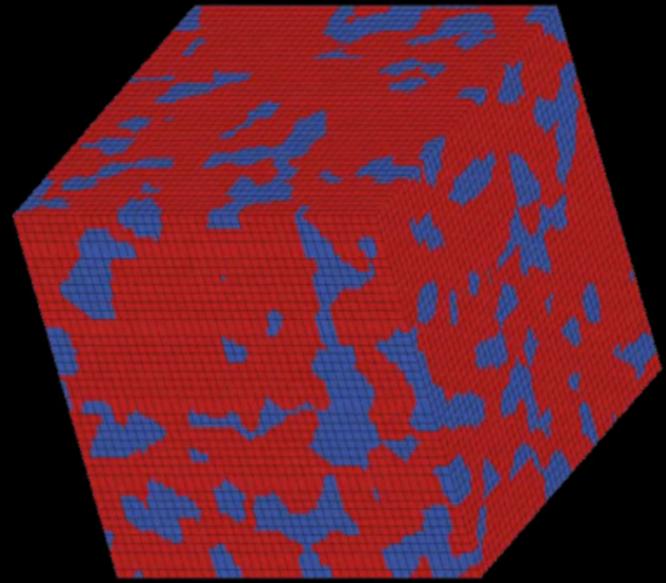


Neper (<https://neper.info>)

FEPX (<https://fepx.info>)

# Numerical Homogenization

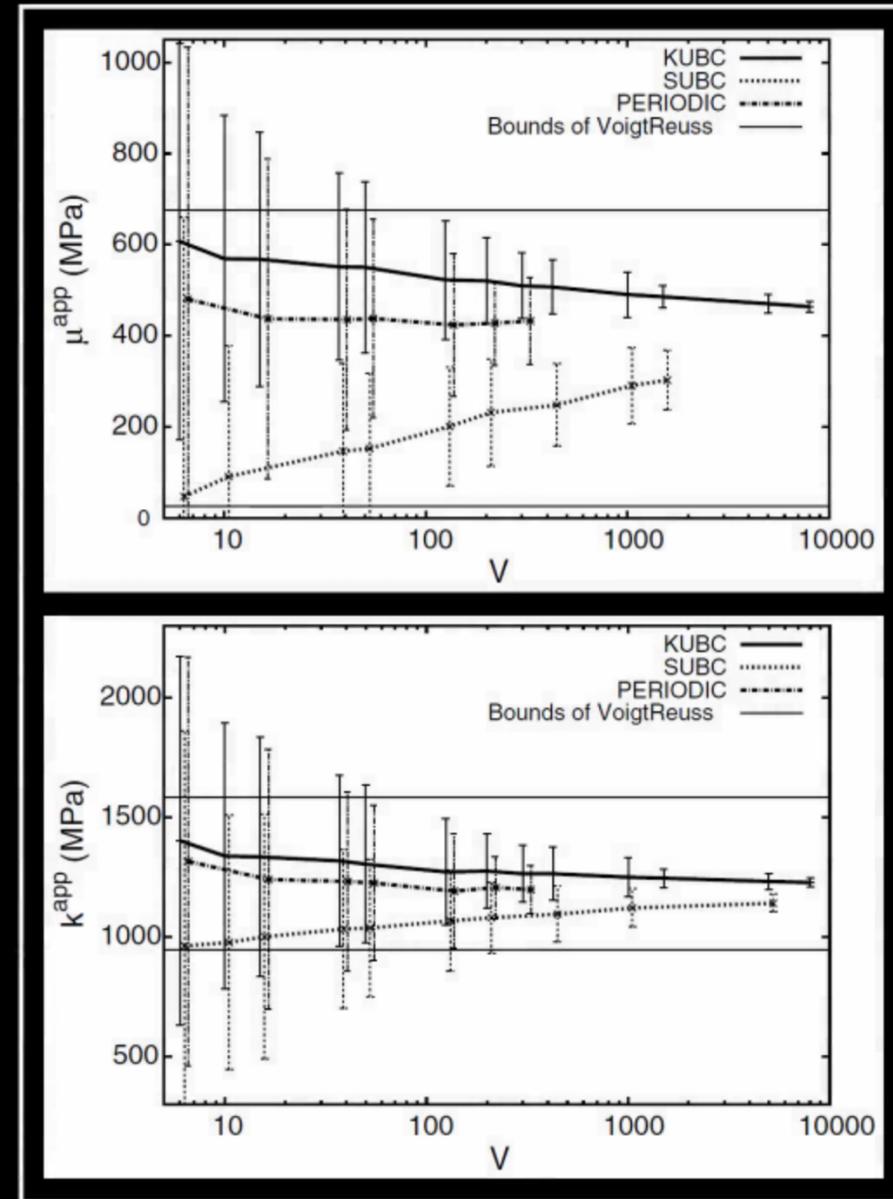
(Kanit et al, 2003)



2-phase microstructure



(AI-generated)



Periodic BCs are the best.

Relative error (95% confidence):

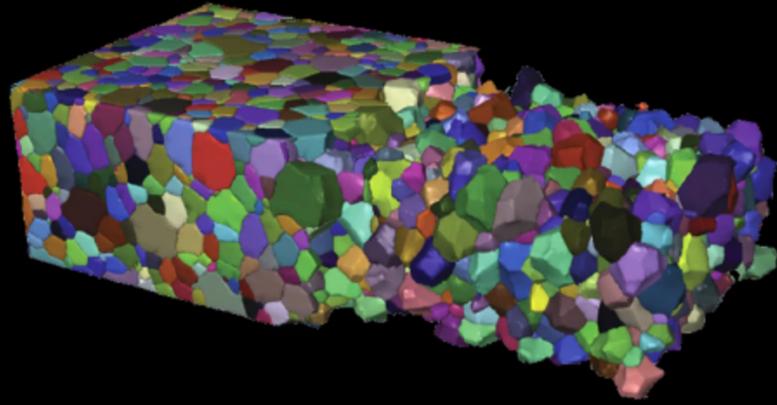
$$e(V) = \frac{2 \sigma_{\mu}(V)}{\bar{\mu}(V)}$$

Knowing  $e(V)$  and for a desired  $e$ ,  
 $V$  can be obtained.

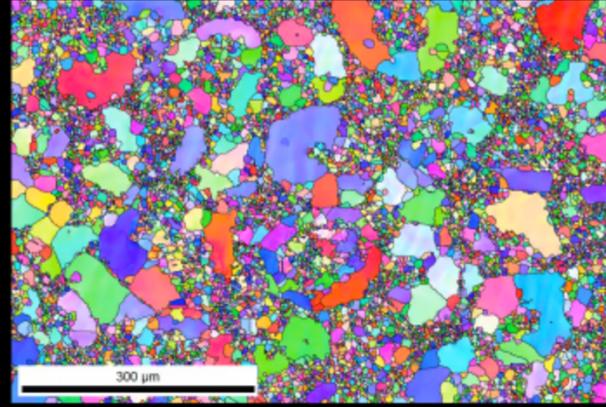
RVE = Domain for which a  
mean value can be estimated within  
a desired error (for a given property)

$e(V)$  can be related to  
microstructural properties (integral range).

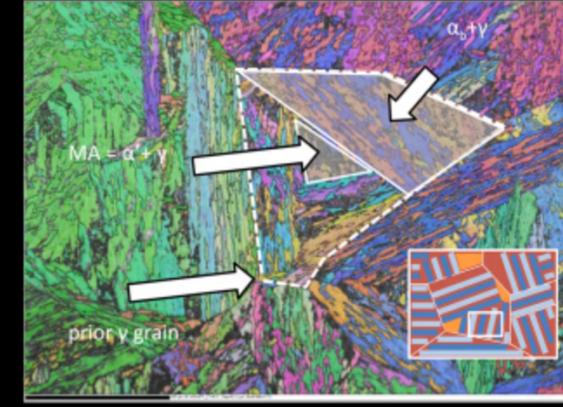
# Polycrystalline Microstructures



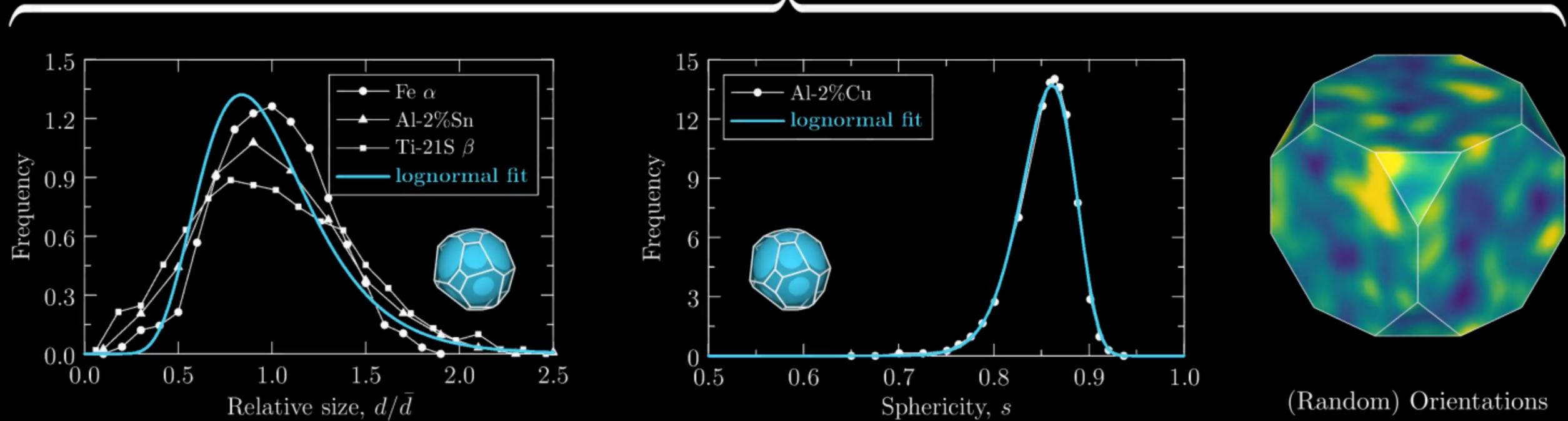
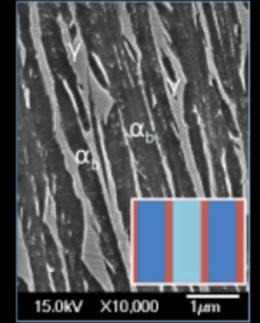
Ti-21S  $\beta$  (Rowenhorst et al, 2007)



Bimodal 316L (Flipon, 2020)

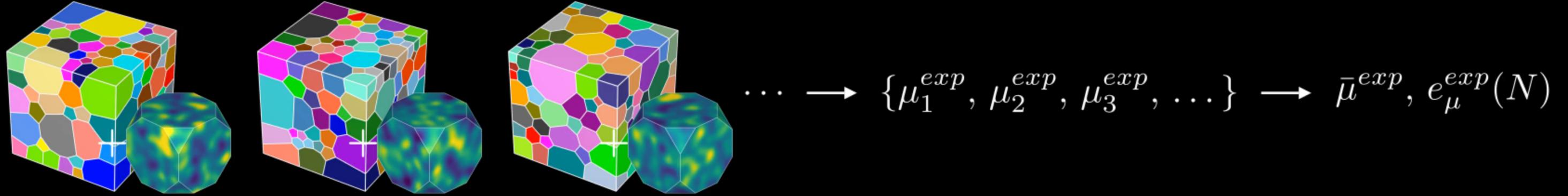


Martensite (Hell, 2011)

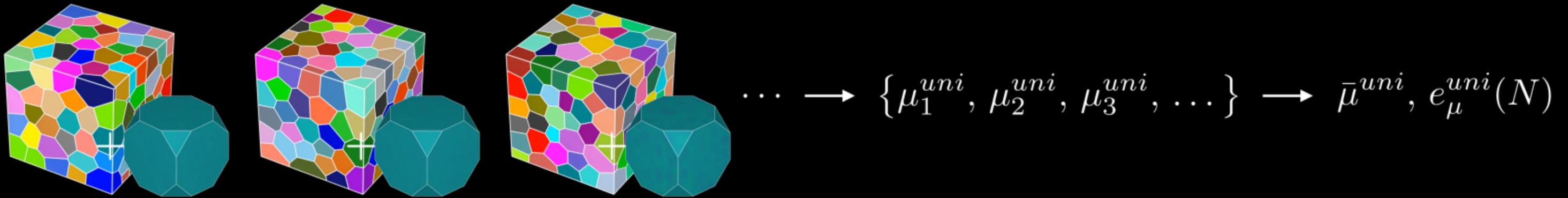


“Grain-growth statistics”: Variabilities  $\sigma_d$ ,  $\sigma_s$  and  $\sigma_f$  (standard deviation / average)

# Motivation



“Experimental”: Random orientation distribution ( $\sigma_f$ ) + grain size distribution ( $\sigma_d$ )



“Uniformized”: Uniform orientation distribution ( $\sigma_f \simeq 0$ ) + no grain size distribution ( $\sigma_d \simeq 0$ )

- Can we go from “experimental” to “uniformized”? ( $\bar{\mu}^{uni} = \bar{\mu}^{exp}$ ?)
  - Is there an interest? ( $e^{uni} < e^{exp}$  and so  $N^{uni} < N^{exp}$ ?)
  - How does  $e_{\mu}$  relate to  $\sigma_d$  and  $\sigma_f$ ?

# Contents

## 1. Microstructure Modelling

- a. Grain Morphology
- b. Grain Orientation Distribution

## 2. Application to Anisotropic Elasticity

- a. Reduction in RVE Size
- b. Relative Influence of Grain Morphology vs Grain Orientation Distribution

# Laguerre Tessellations

(aka “Weighted Voronoi”  
or “Radical” Tessellations)

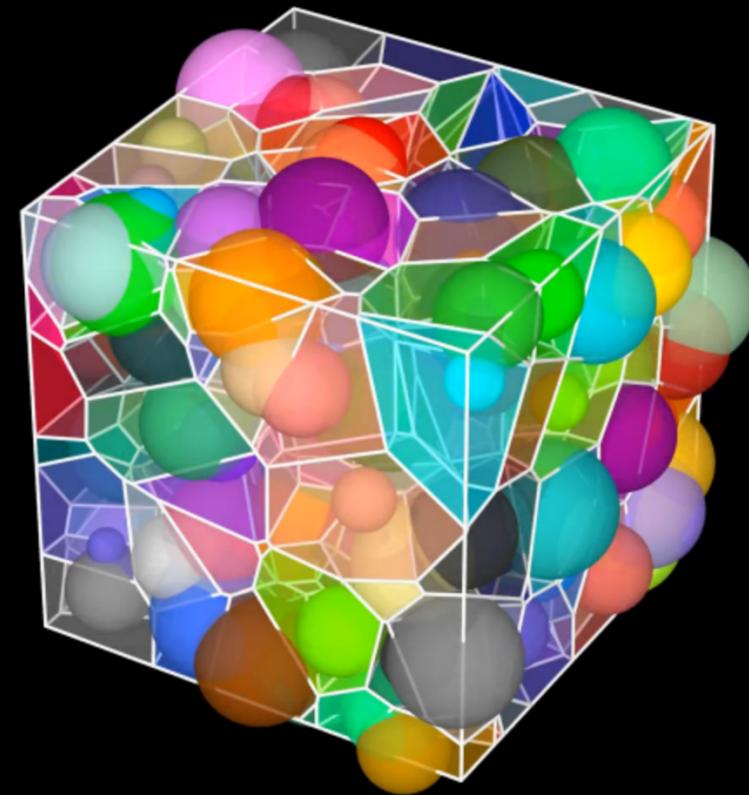
Domain of space,  $D$   
Seeds,  $S_i$  ( $i \in [1, N]$ ),  
of positions  $\mathbf{x}_i$   
and weights  $w_i$

→ Cells,  $C_i = \{P(\mathbf{x}) \in D \mid \|P, S_i\|^2 - w_i < \|P, S_j\|^2 - w_j \ \forall j \neq i\}$

In general, the larger the weight ( $w_i$ ),  
the bigger the cell ( $C_i$ ).

No direct relation between  $S_i(\mathbf{x}_i, w_i)$  and  $C_i$

Grains are convex → conventional meshing



Laguerre tessellations = general parameterization of normal tessellations  
(assuming independent parameters) (Lautensack, 2007).

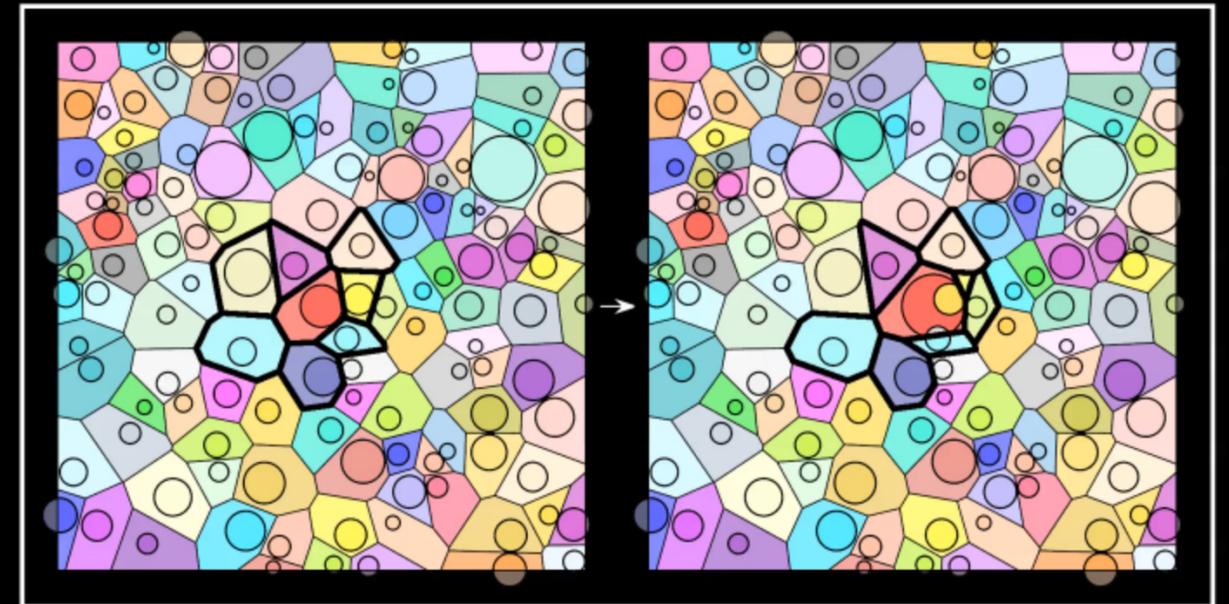
# Optimization of Laguerre Tessellations

(Quey and  
Renversade, 2018)

Variables = Seed weights and coordinates  
Objective Function = “actual vs target properties”  
(grain statistics or individual grain properties)

→ non-linear, unknown gradient,  
large-scale, local optimization problem

Resolution using  
NLopt’s *Subplex* algorithm  
(one variable changed at each iteration)  
+  
a tessellation update algorithm

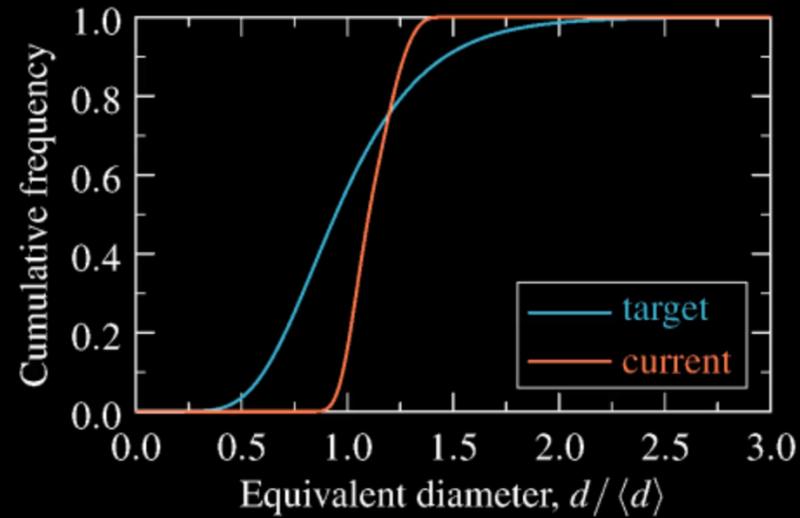
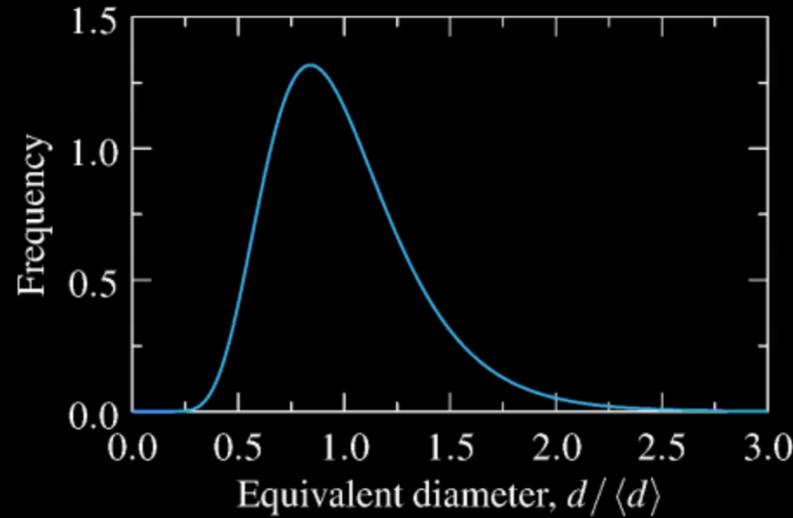


Tessellation update (red seed modified).

Any (convex-grain) polycrystal can be generated given a proper definition of  
the objective function.

# Optimization of Laguerre Tessellations

(Quey and  
Renversade, 2018)



Modified Anderson-Darling test (1952):

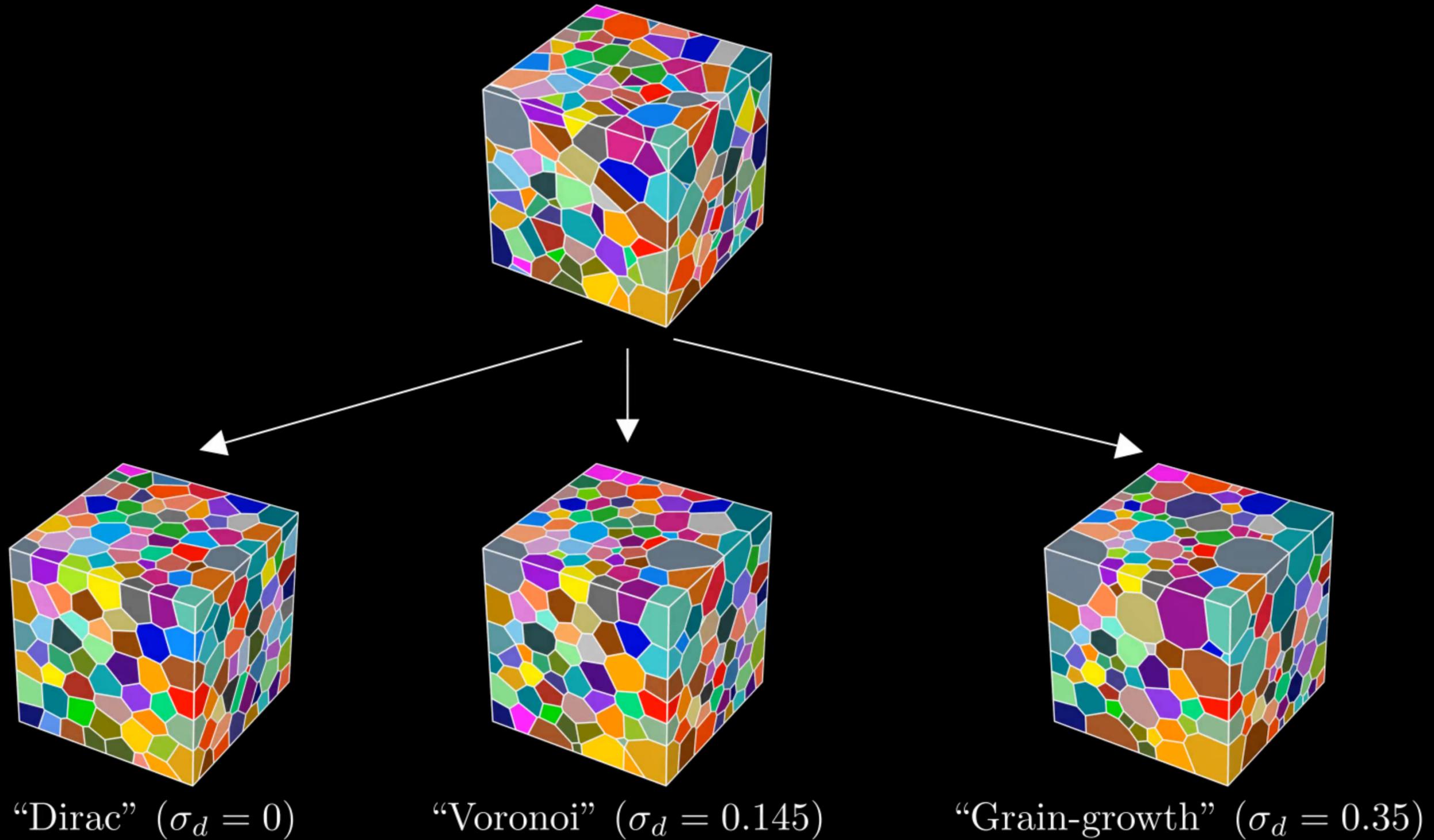
$$O_d = \int_{-\infty}^{+\infty} \frac{(F^* \circ s(x) - F \circ s(x))^2}{F \circ s(x) (1 - F \circ s(x))} dx$$

Same for other distributions (sphericity)...

$$O = \sqrt{O_d^2 + O_s^2}$$

(Aggregated optimization)

# Example Microstructures



# Contents

## 1. Microstructure Modelling

a. Grain Morphology

b. Grain Orientation Distribution

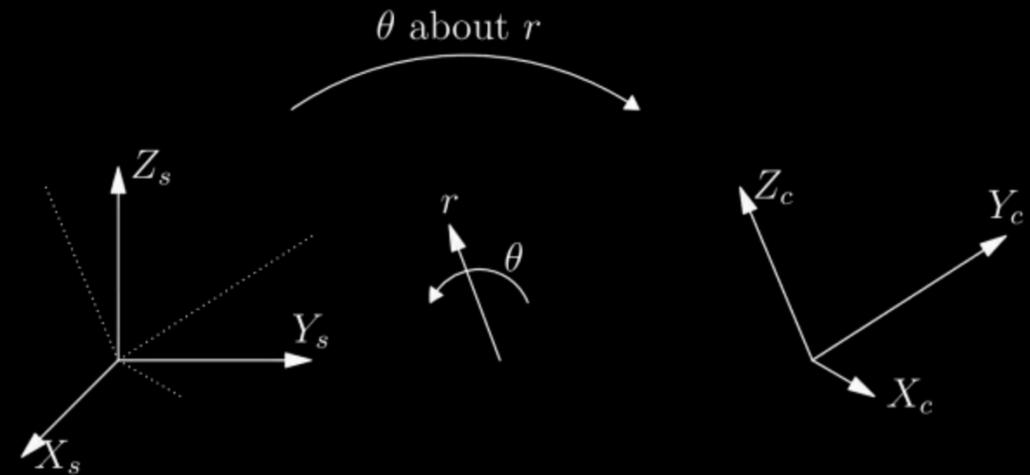
## 2. Application to Anisotropic Elasticity

a. Reduction in RVE Size

b. Relative Influence of Grain Morphology vs Grain Orientation Distribution

# Orientations Represented by Unit Quaternions (Hamilton, 1843)

*Any orientation can be described by a rotation of angle  $\theta \in [0, \pi]$  around a unique axis,  $\mathbf{r}$  (Euler, 1775).*



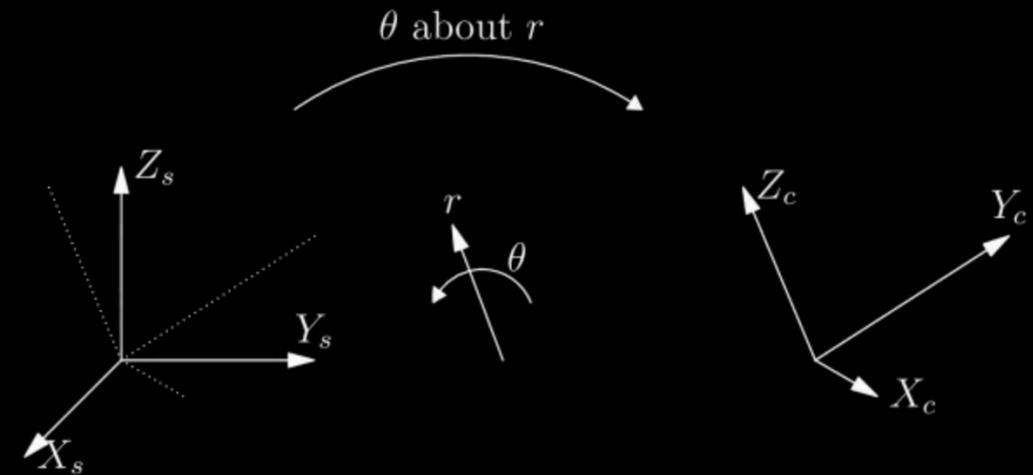
$$\boxed{\mathbf{q} = \cos\left(\frac{\theta}{2}\right) + \mathbf{r} \sin\left(\frac{\theta}{2}\right)} \longrightarrow \begin{cases} 4\text{D vectors, } \|\mathbf{q}\| = 1, \mathbf{q} \in \mathbb{S}^3 \\ 1 \text{ orientation} = 2 \text{ quaternions } (\mathbf{q} \text{ and } -\mathbf{q}) \end{cases}$$

Easy computation:  $\mathbf{q}_3 = \mathbf{q}_1 \mathbf{q}_2$ ,  $\mathbf{q}_m = \mathbf{q}_2 \mathbf{q}_1^{-1}$ ,  $\mathbf{q}^k = \mathbf{q} \mathbf{u}^k, \dots$

Misorientation angle =  $2 \times$  distance between quaternions (no distortion)

# Visualization of Orientations using Rodrigues Vectors (Rodrigues, 1840)

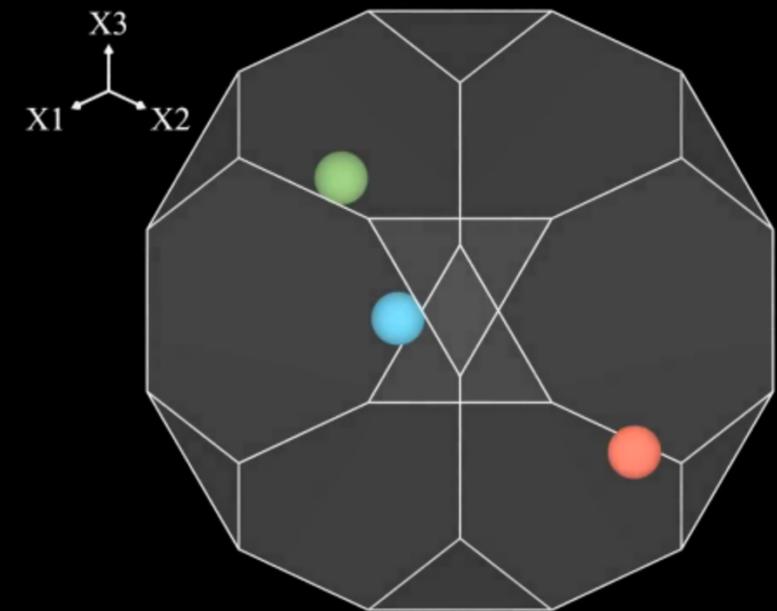
*Any orientation can be described by a rotation of angle  $\theta \in [0, \pi]$  around a unique axis,  $\mathbf{r}$  (Euler, 1775).*



$$\mathbf{v} = \mathbf{r} \tan\left(\frac{\theta}{2}\right)$$

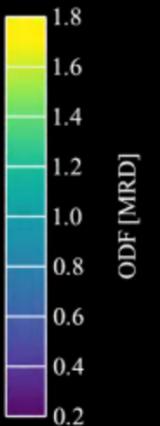
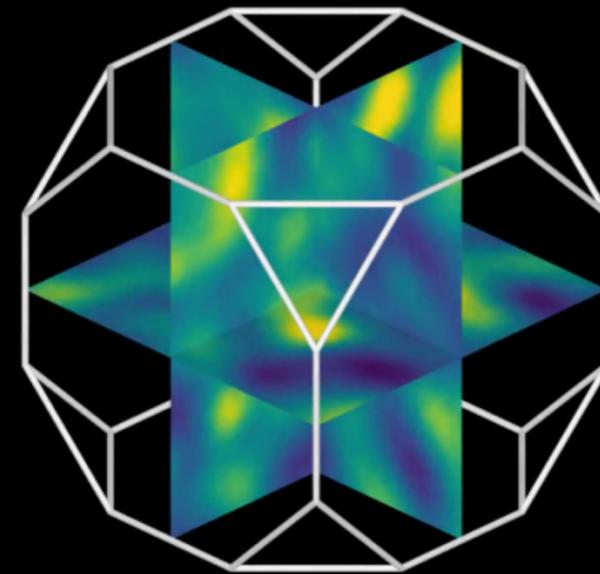
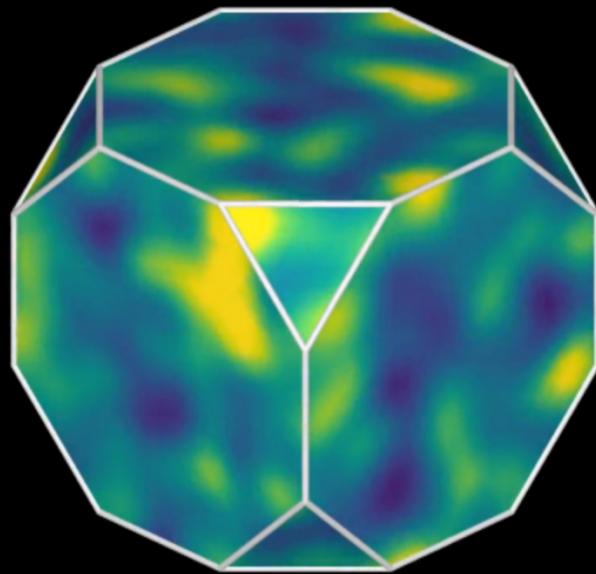
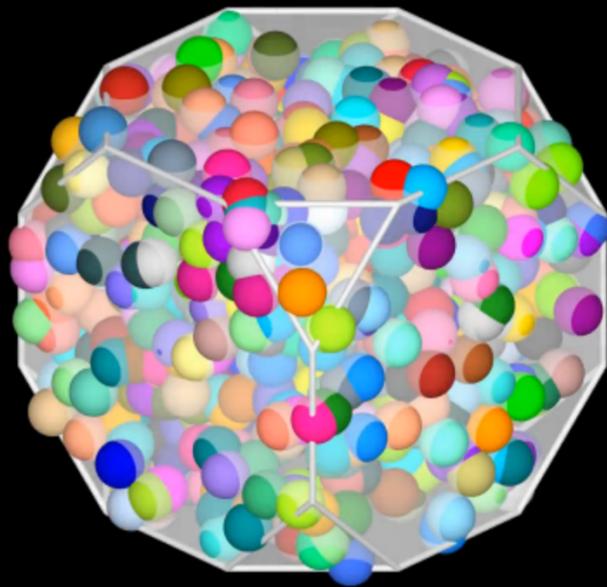
→ { 3D vectors,  $v \in \mathbb{R}^3$  (infinite space)  
1 orientation = 1 Rodrigues vector

Cubic symmetry  $\Rightarrow$  “fundamental region” = truncated cube



# Random Distributions of Orientations

Rejection Sampling Algorithm:  $\left\{ \begin{array}{l} 1. \text{ Draw random numbers, } n_1, n_2, n_3 \text{ and } n_4, \text{ in } [-1, 1] \\ 2. \text{ If } n_1^2 + n_2^2 + n_3^2 + n_4^2 \leq 1, \text{ accept orientation:} \\ \mathbf{q} = \frac{(n_1, n_2, n_3, n_4)}{\sqrt{n_1^2 + n_2^2 + n_3^2 + n_4^2}} \end{array} \right.$

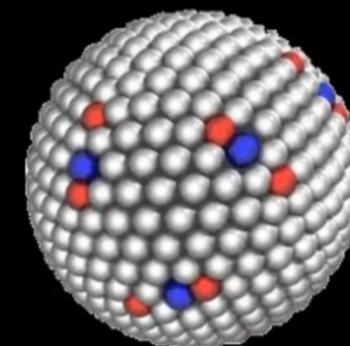


1000 orientations, cubic symmetry

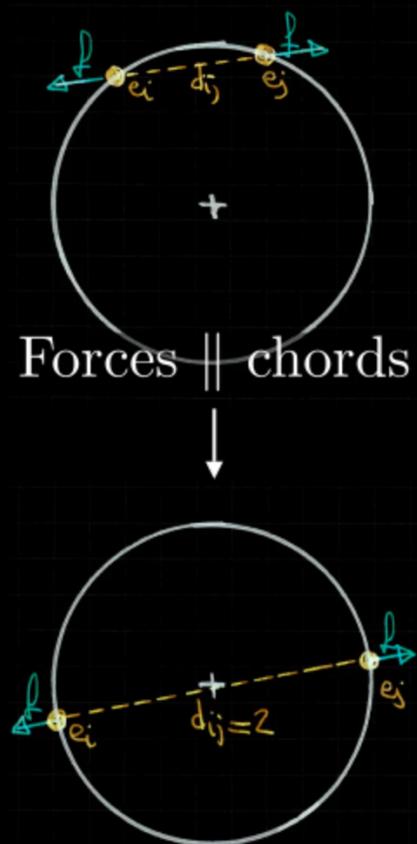
$$\sigma_f \simeq 0.3 \forall N$$

# Nearly-Uniform Distributions of Orientations (Quey et al, 2018)

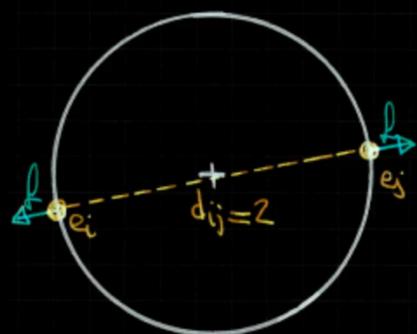
Applied to Orientations: “Determine the minimum energy configuration of  $N$  unit quaternions on the surface of  $\mathbb{S}^3$ .”



Electrons

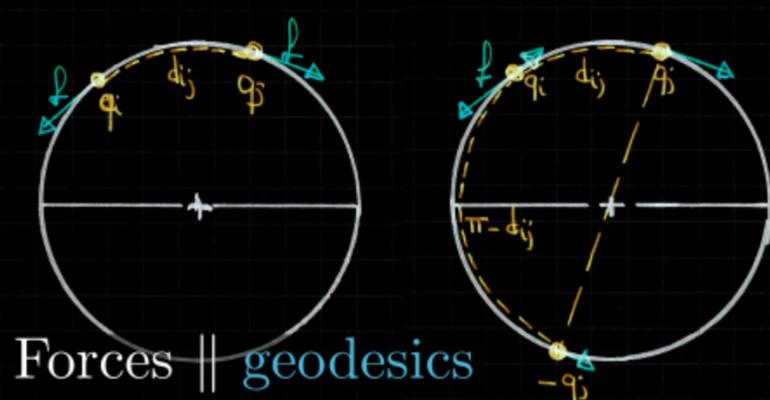


Forces  $\parallel$  chords

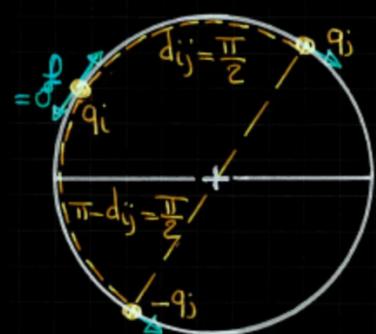


$f \neq 0$

Orientations



Forces  $\parallel$  geodesics



$f = 0$

Formulation in tangent space:

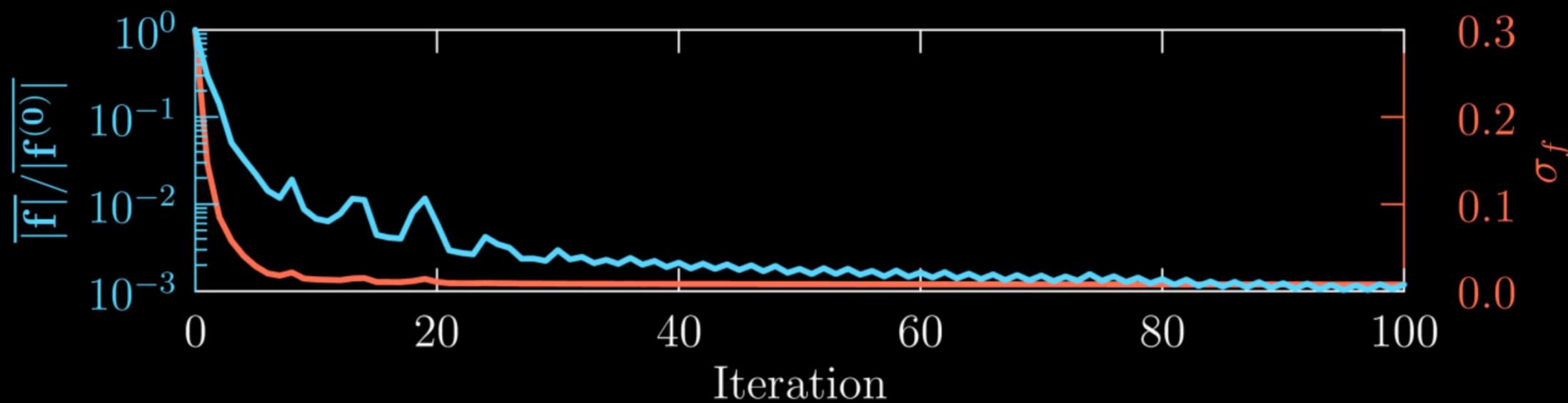
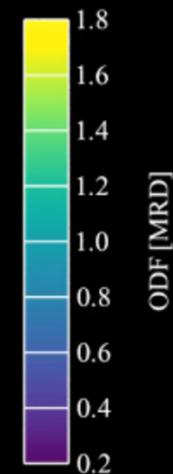
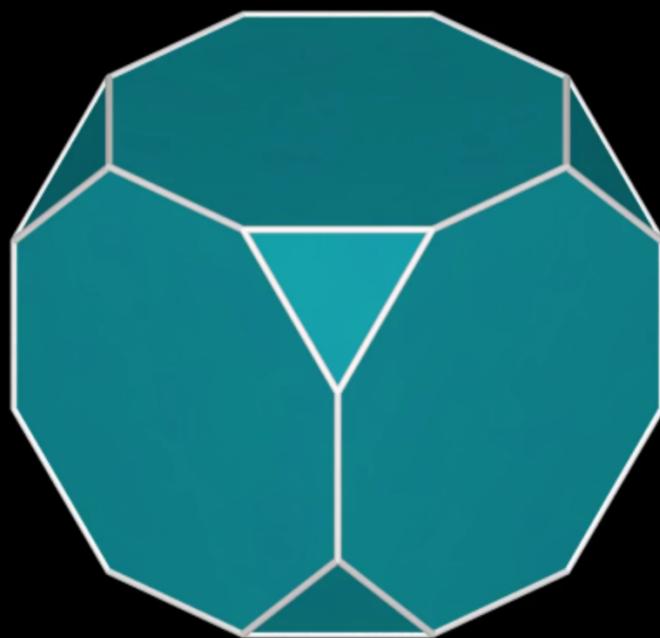
$$\mathbf{f}_i = - \sum_{j=1, j \neq i}^N \sum_{k=1}^{n_c} \left( \frac{1}{d_{ij}^k{}^2} + \frac{1}{(\pi - d_{ij}^k)^2} \right) \mathbf{r}_{ij}$$

$N$  orientations  
(cut-off for large  $N n_c$ )

Crystal symmetry

$$\Delta \mathbf{q}_i^{(l)} = \alpha^{(l)} \mathbf{f}_i^{(l)}$$

(Gradient descent, Barzilai-Borwein step size) 12



1000 orientations, cubic symmetry

$$\sigma_f \simeq 0.007$$

$$\sigma_f^{bcc} \simeq 0.002_{13}$$

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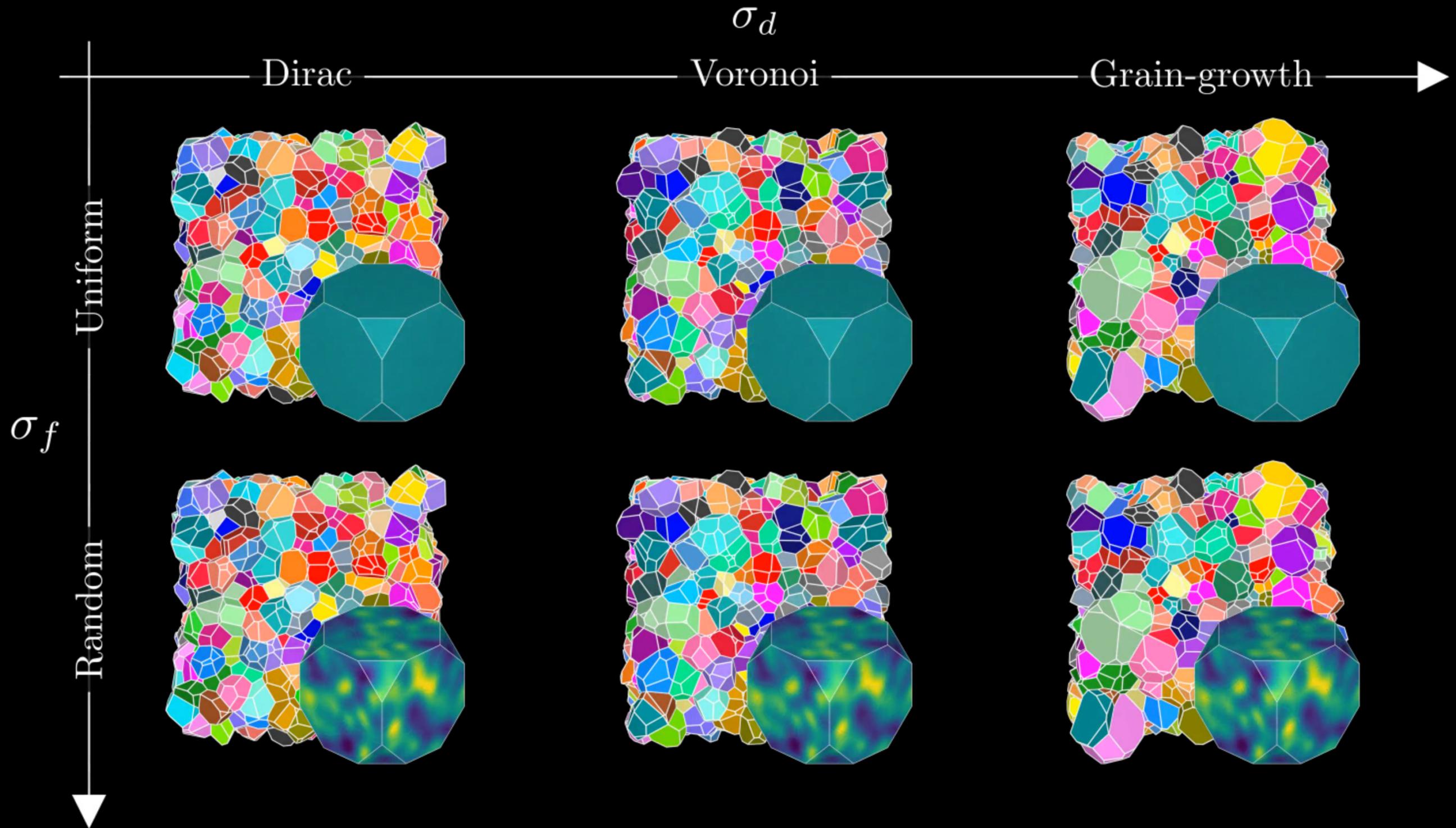
b. Grain Orientation Distribution

## 2. Application to Anisotropic Elasticity

a. Reduction in RVE Size

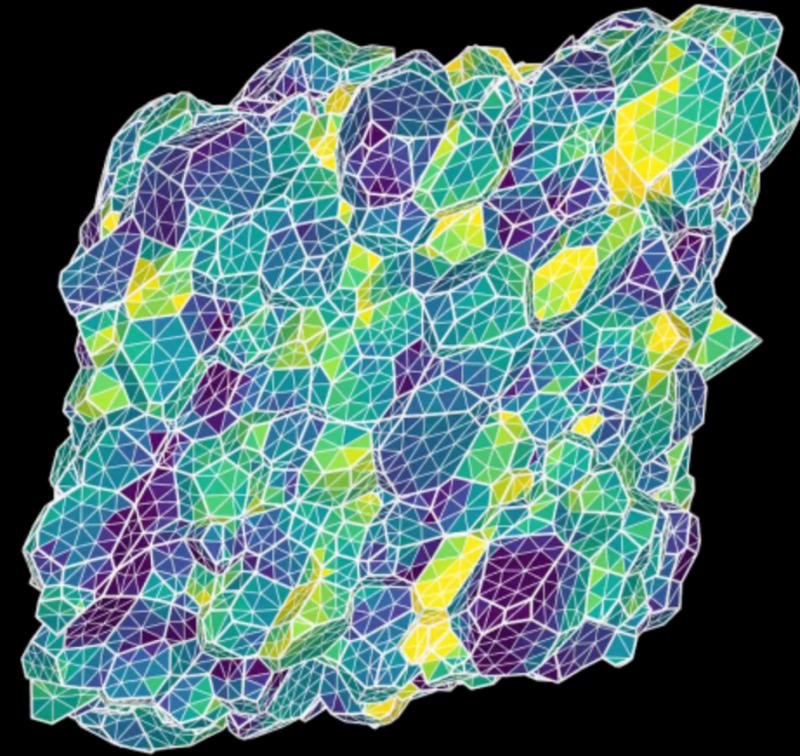
b. Relative Influence of Grain Morphology vs Grain Orientation Distribution

# Microstructural Configurations



# Simulations

- Copper in Elasticity  
( $C_{11} = 159$  GPa,  $C_{12} = 122$  GPa,  $C_{44} = 81$  GPa)
- Periodic polycrystals
- Shear deformation in FE  $\rightarrow \mu$   
( $\kappa$  isotropic)

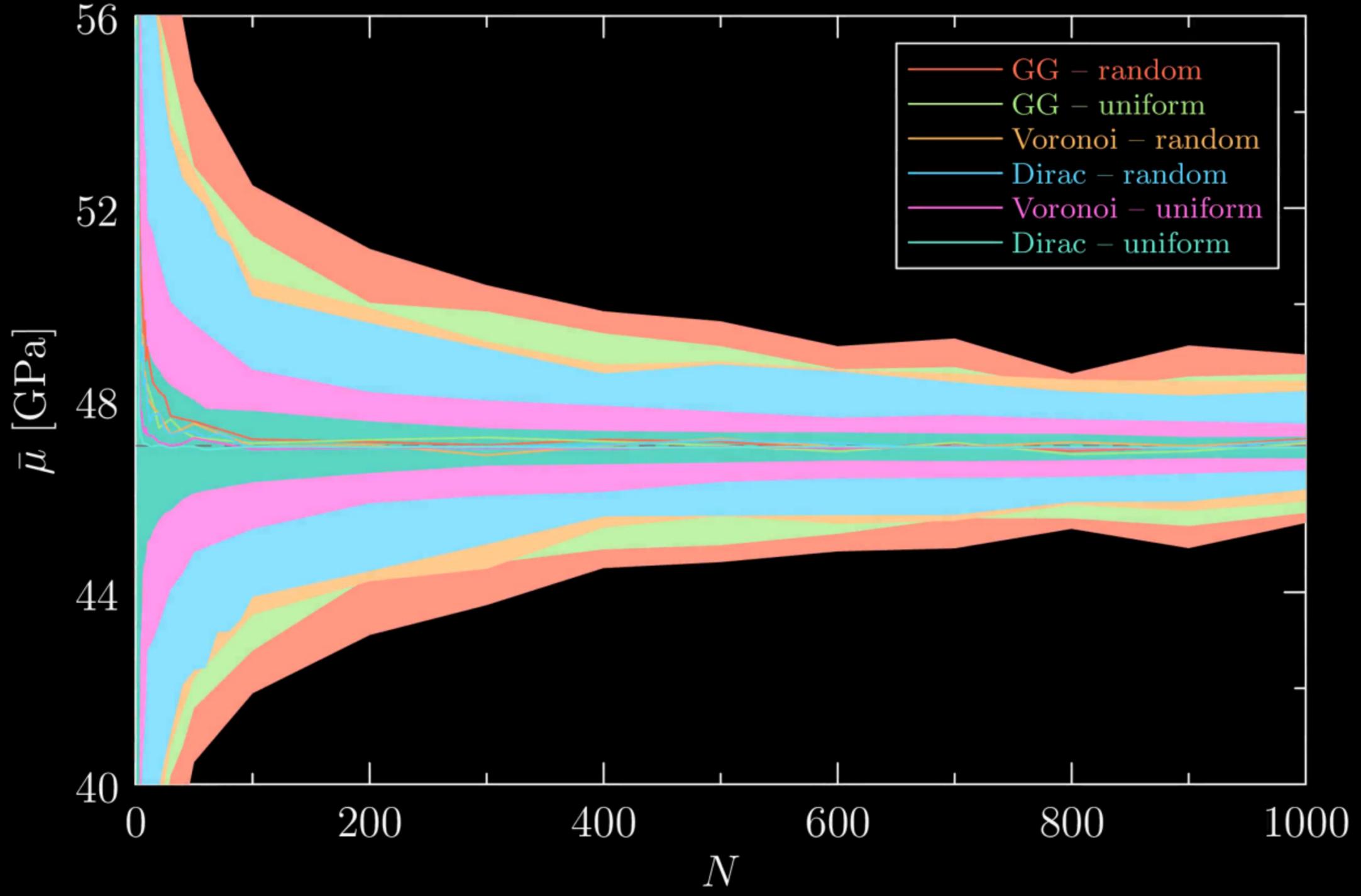


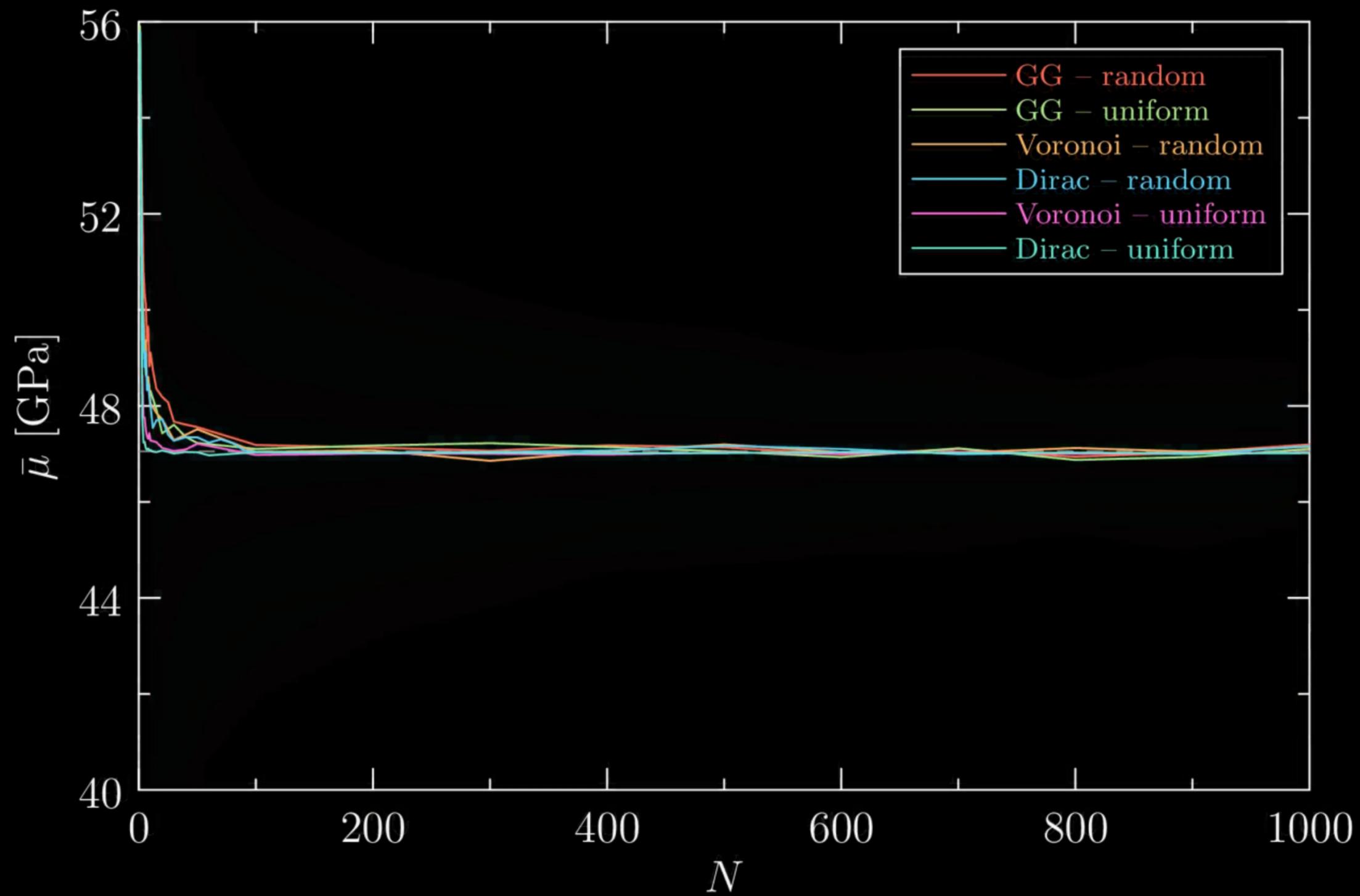
For each microstructural configuration

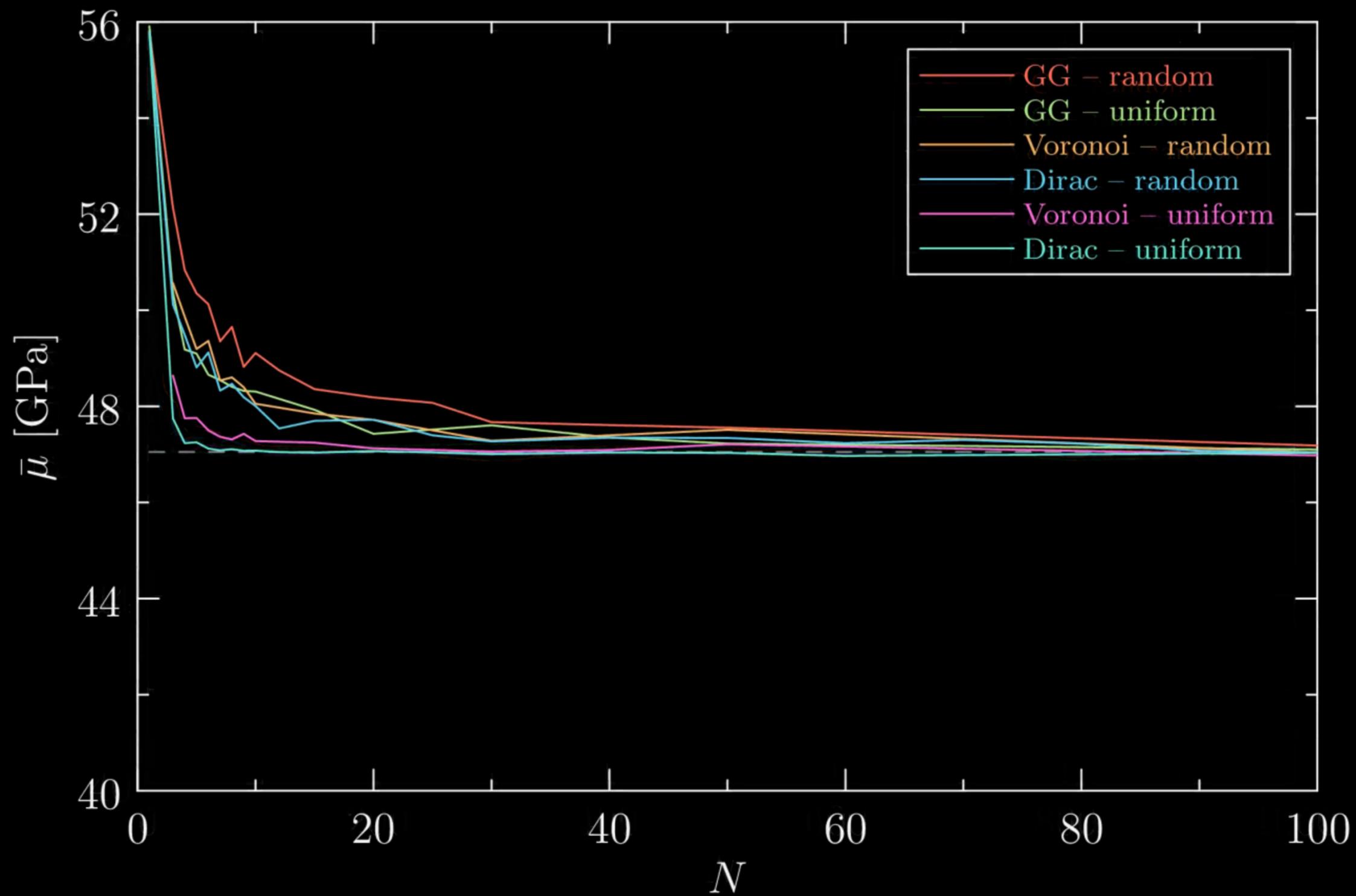
For  $N = 3, 4, 5, \dots, 10, 20, 30, 40, 50, \dots, 100, 200, 300, 400, 500, \dots, 1000$

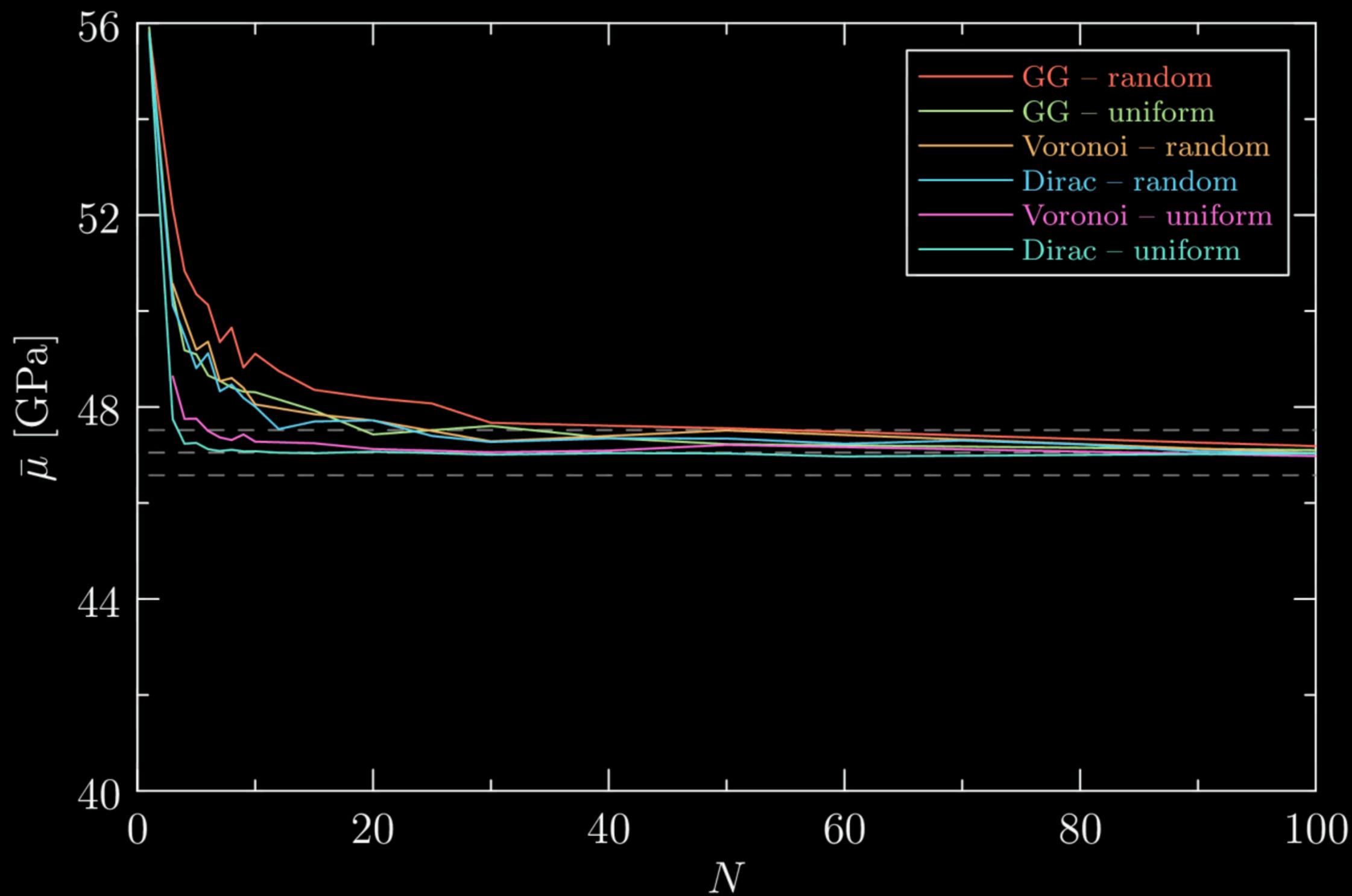
Consider 100s different microstructures to get  $\{\mu_1, \mu_2, \mu_3, \dots\}$

Compute  $\bar{\mu}(N)$  and  $e_\mu(N)$

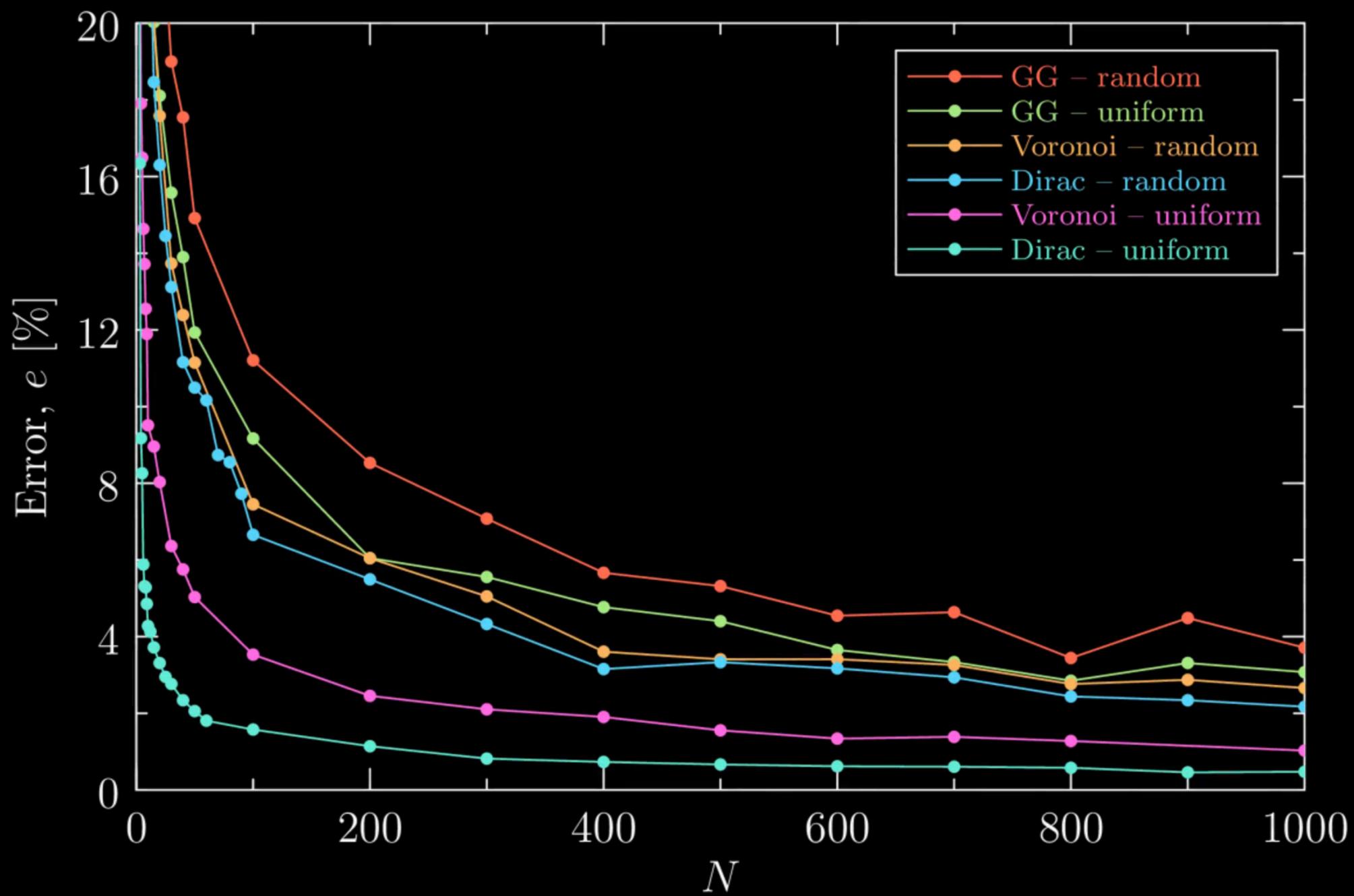


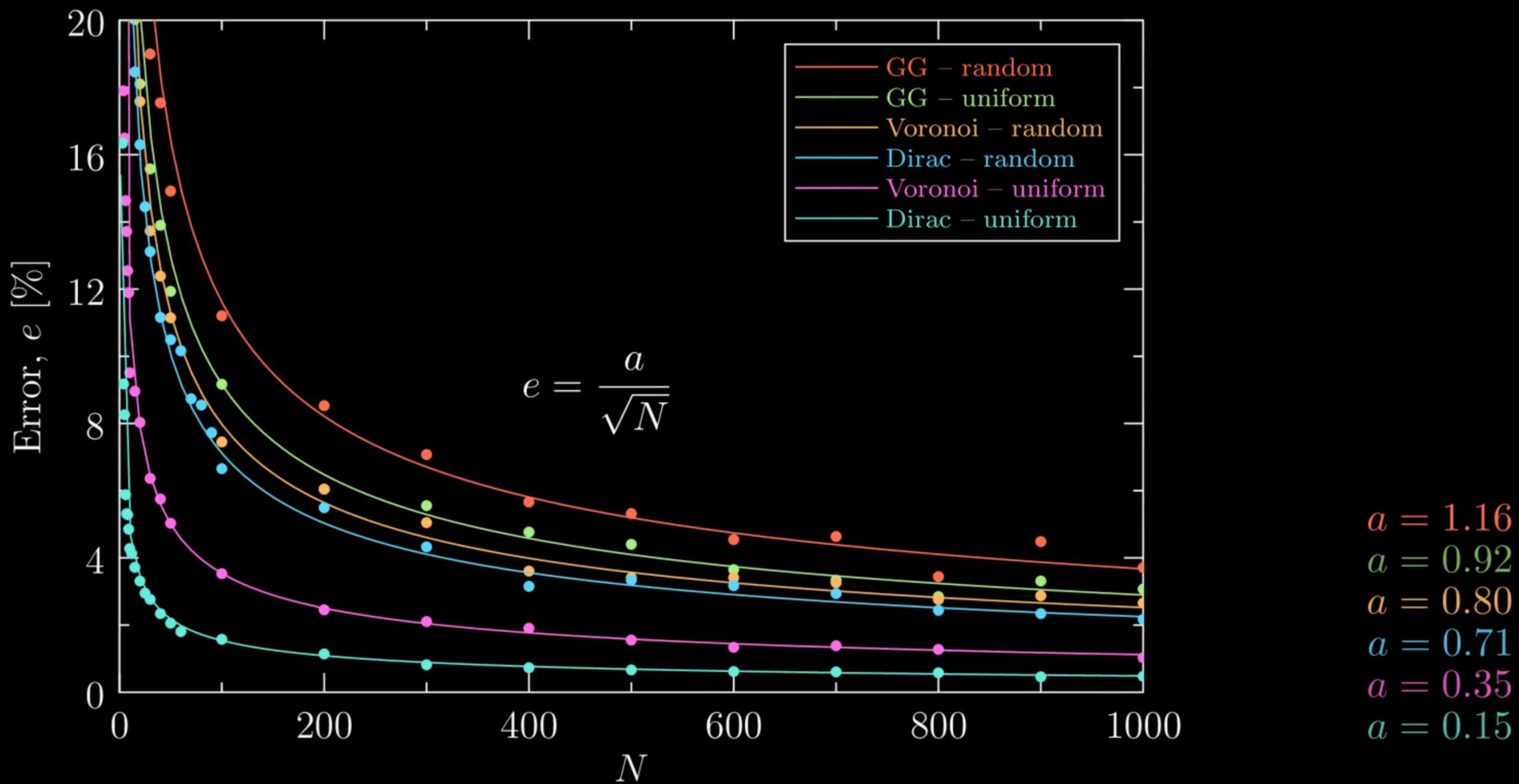






“Gray area” (1%): “Grain-growth – random”:  $N \leq 50$ , “Dirac – uniform”:  $N \leq 4(!)$





From “Grain-growth – random” to “Dirac – uniform”:  $e$  divided by 7.7,  $N$  divided by  $7.7^2 = 60$  17

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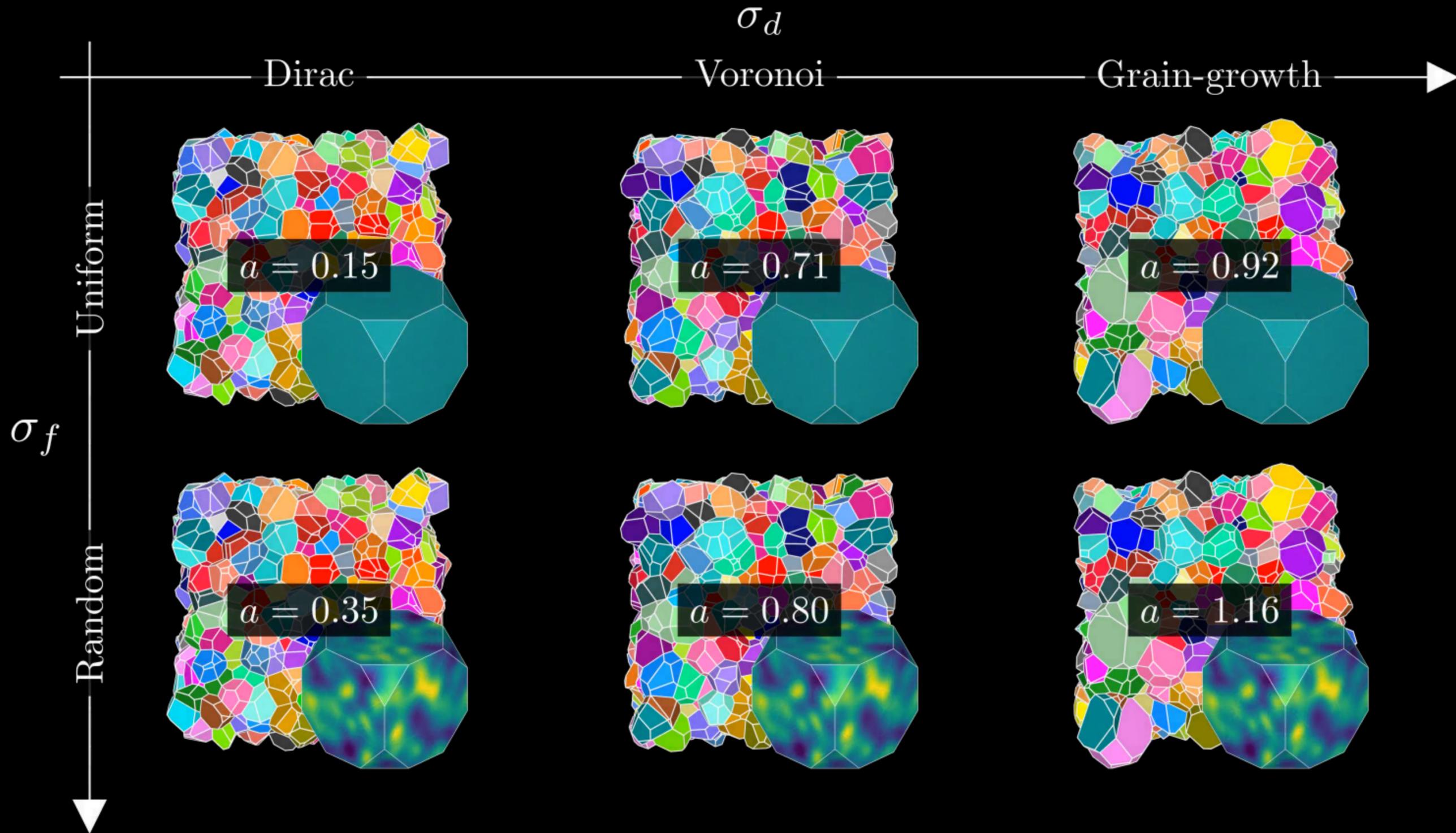
b. Grain Orientation Distribution

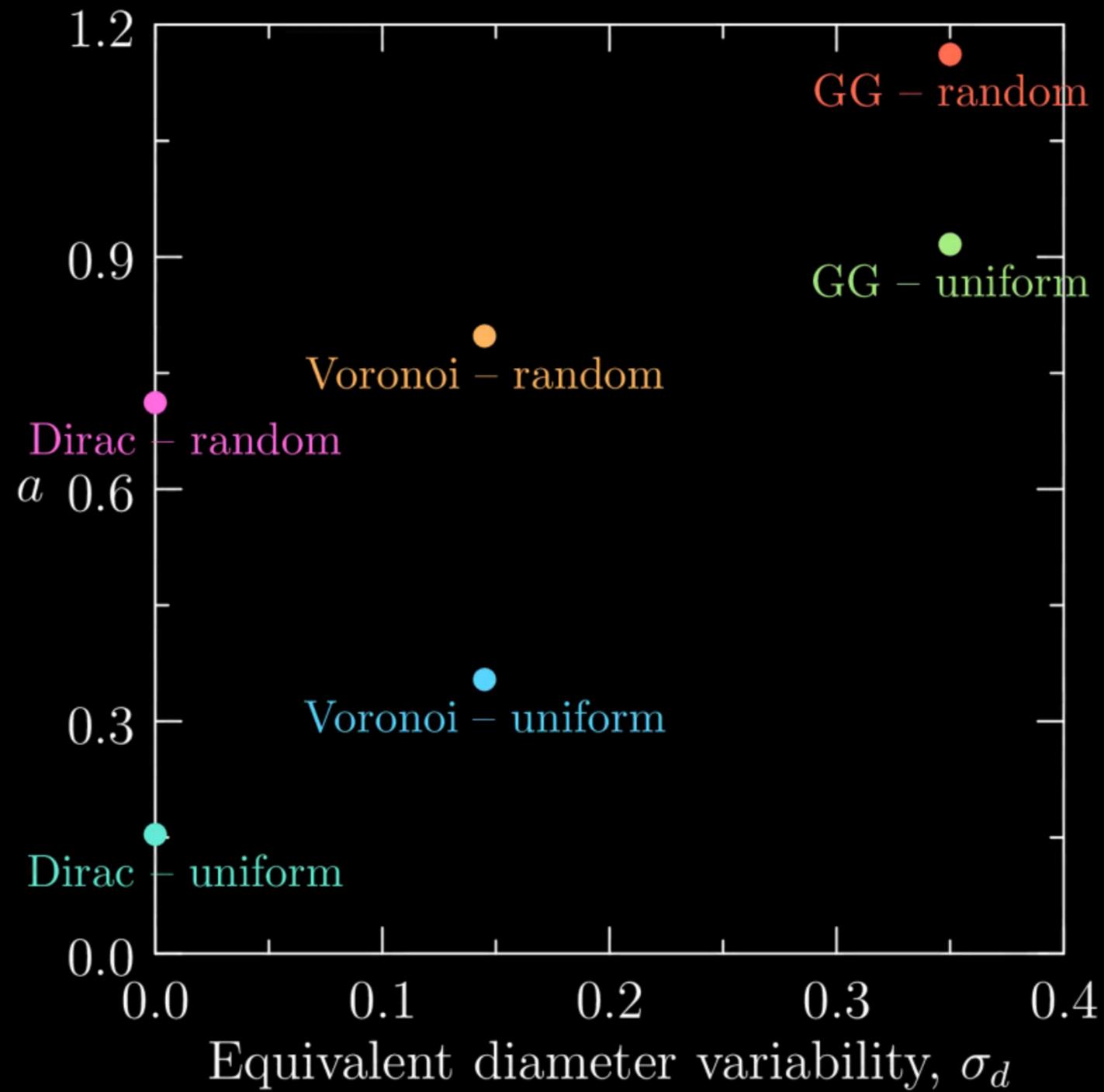
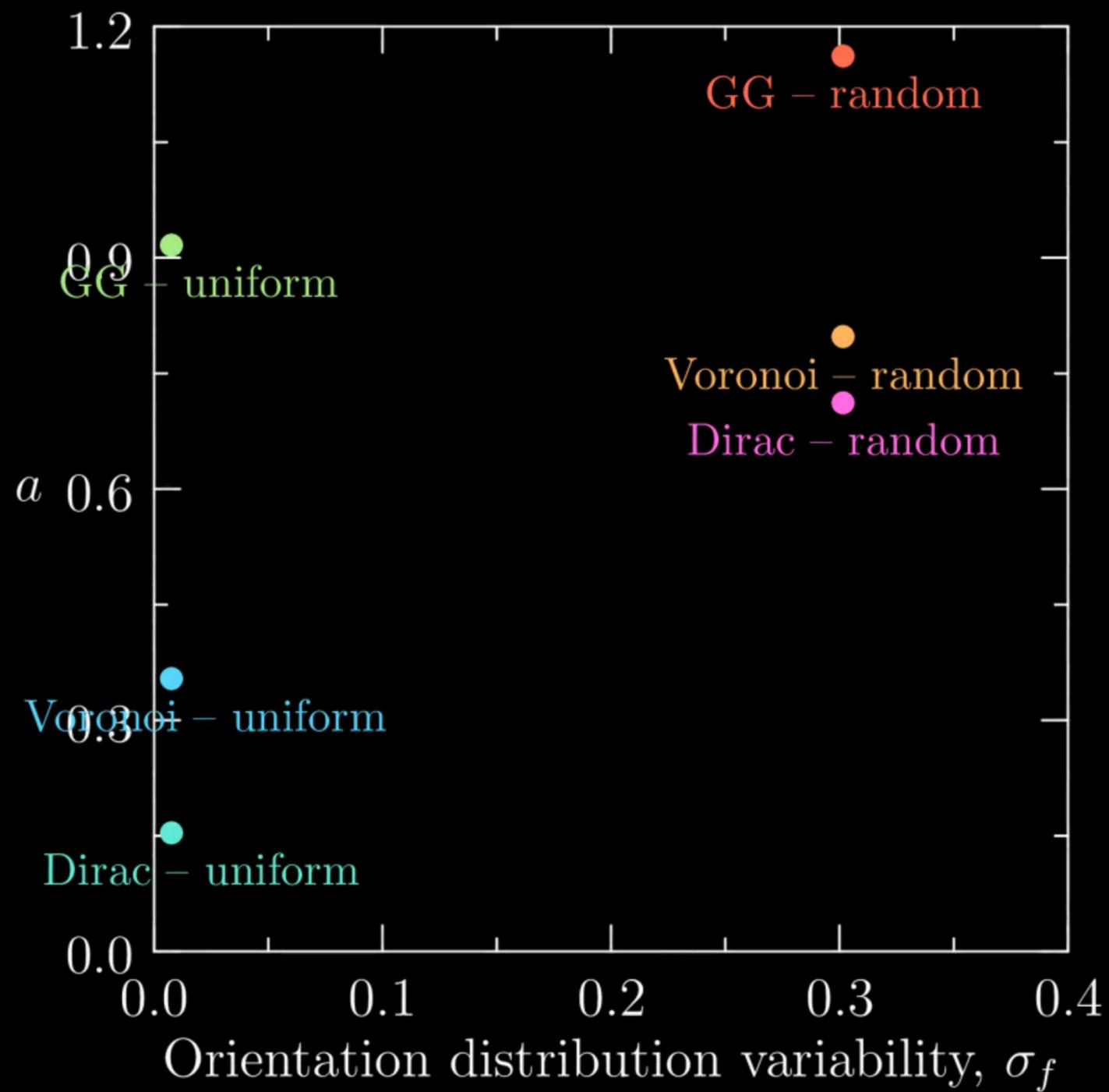
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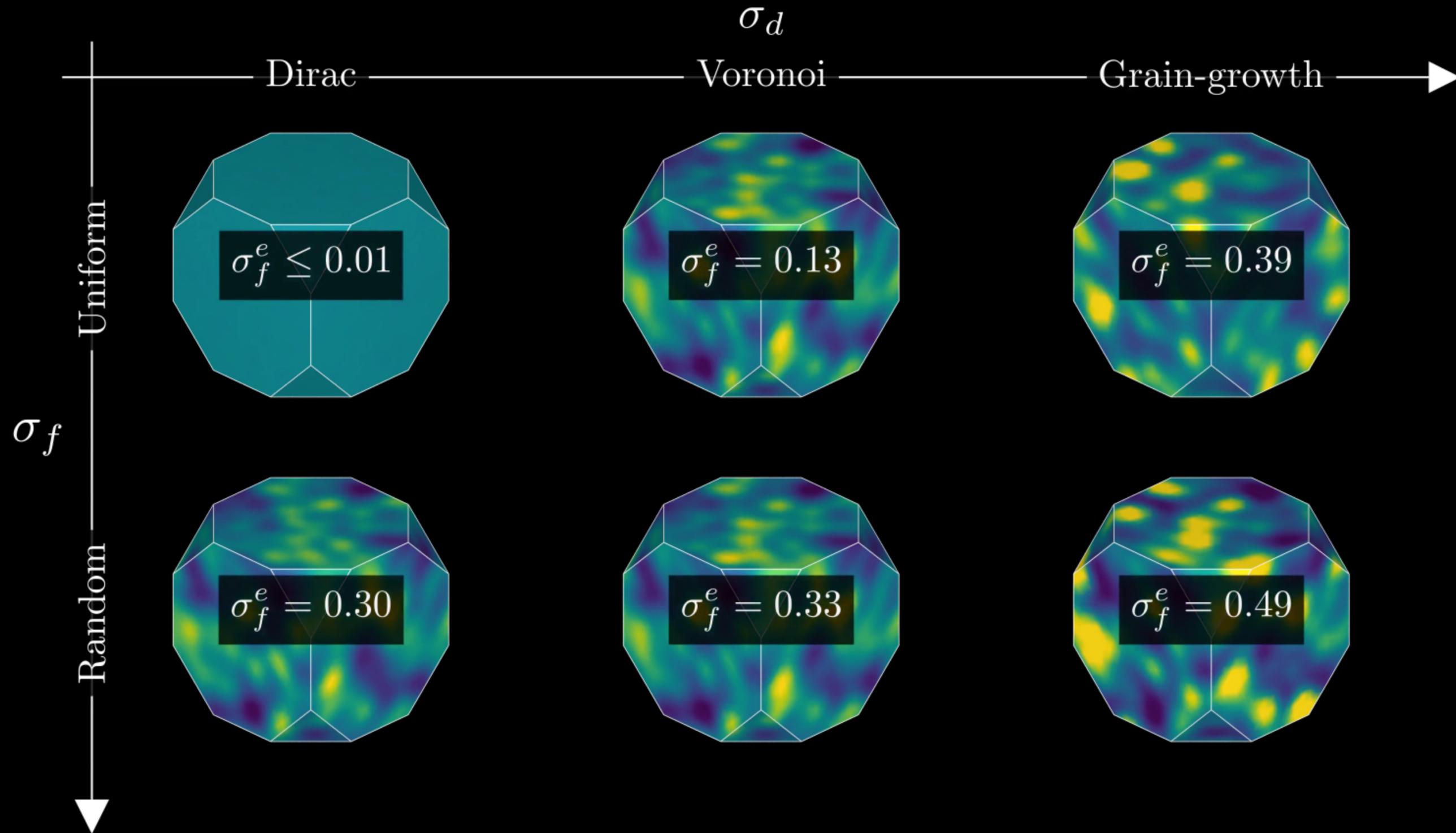
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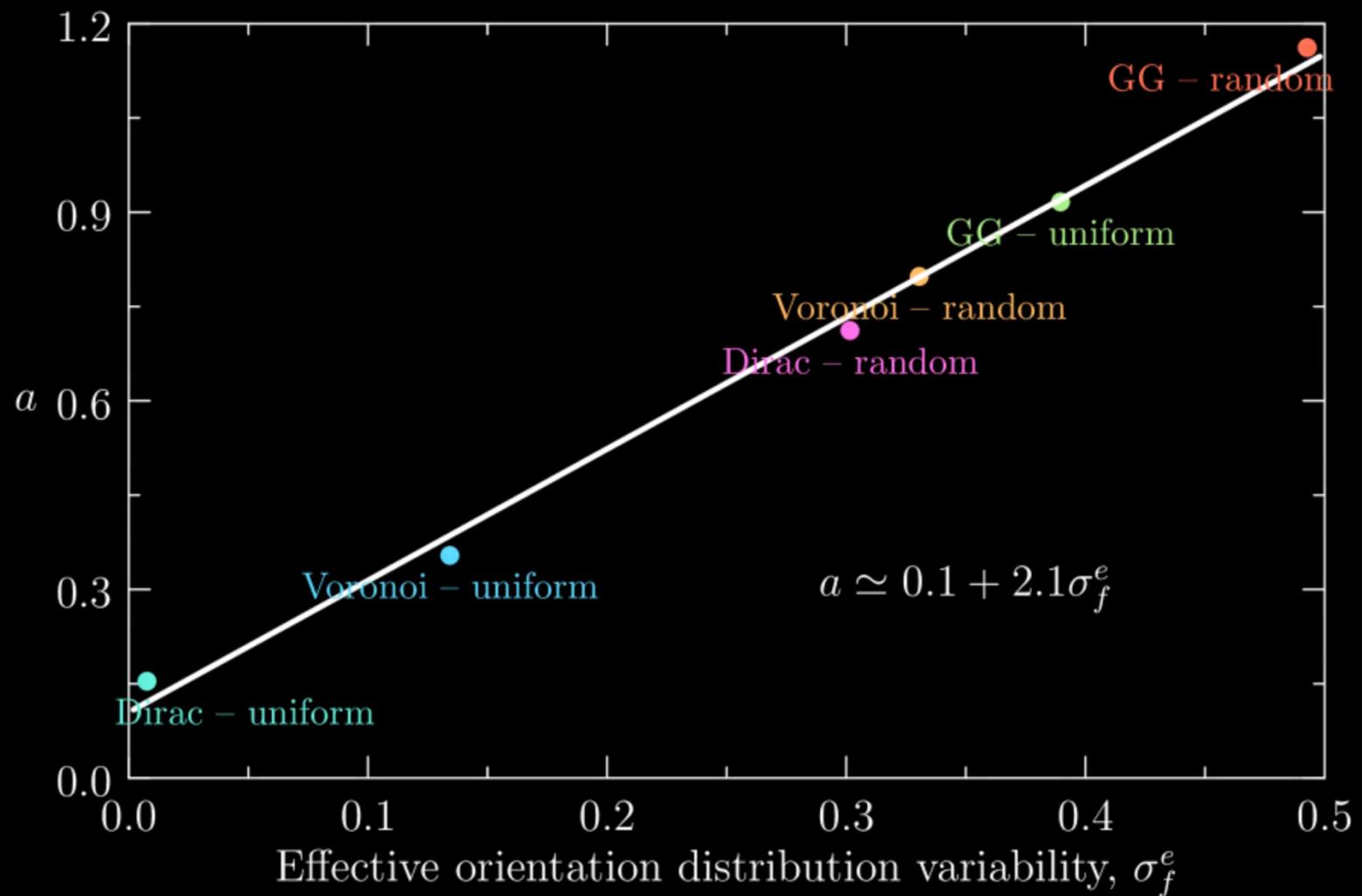
# Microstructural Configurations





# Microstructural Configurations





$$e = \frac{0.1 + 2.1 \sigma_f^e}{\sqrt{N}}$$

$$\sigma_f^e = \sqrt{\sigma_f^2 + f(\sigma_d)^2}$$

$\sigma_f$ : orientation distribution effect

$f(\sigma_d)$ : size distribution effect

	Dirac	Voronoi	Grain-growth
$a$	0.73	0.79	1.13
$f(\sigma_d)$	0.00 ( 0%)	0.13 (13%)	0.39 (57%)
$\sigma_f$	0.30 (86%)	0.30 (74%)	0.30 (33%)
constant	0.10 (14%)	0.10 (13%)	0.10 (10%)

# Conclusions (for Copper / Grain-growth)

- “Uniformized” polycrystals can be used ( $\bar{\mu}^{uni} \simeq \bar{\mu}^{exp}$ )

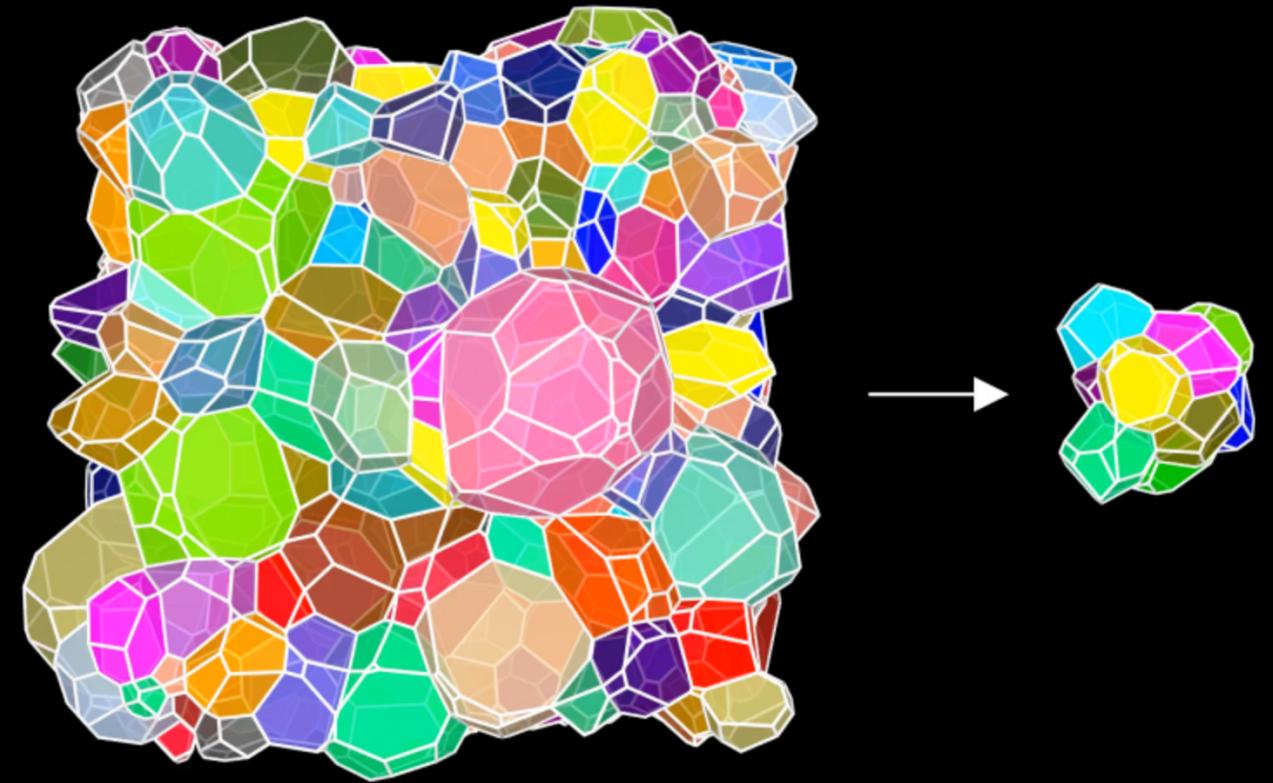
1% deviation on  $\mu$  for  $N \leq 50$  for “experimental” vs  $N \leq 4$  for “uniformized”

(for PBCs, deviation related to the uniformity rather than the size)

- Error ( $e_\mu$ ) divided by 7.7, RVE size divided by 60

- Error ( $e_\mu$ ) related to  $N$ ,  $\sigma_d$  and  $\sigma_f$  by

$$e_\mu = \frac{0.1 + 2.1 \sigma_f^e}{\sqrt{N}} \rightarrow e_\mu = \frac{f_1(C_{ij}) + f_2(C_{ij}) \sigma_f^e}{\sqrt{N}}$$



$e_\mu = 2\%$