

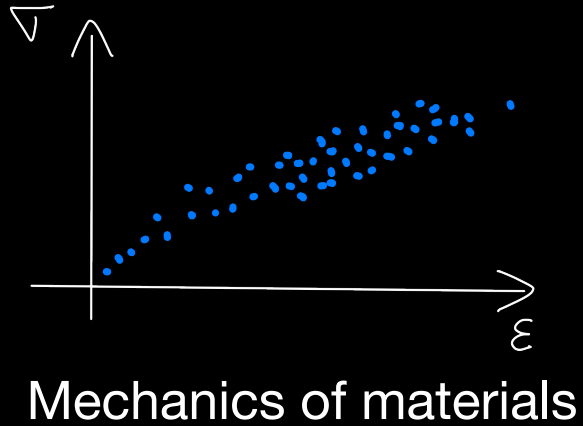
# Identifier des contraintes sans modèle pour identifier un modèle ensuite?

Adrien Leygue & Friends

GTs – Apprentissage – Mesures de champs et identification

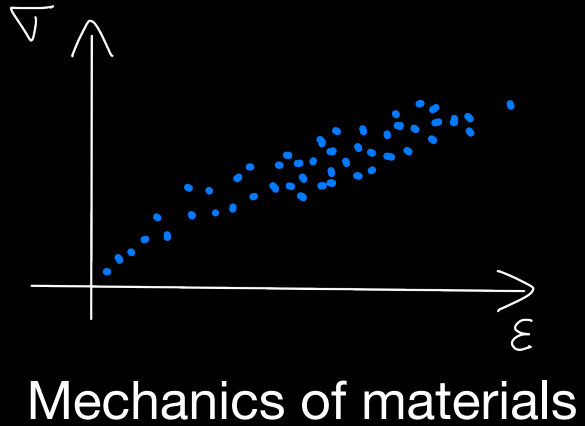


# Model-free Mechanics of Materials



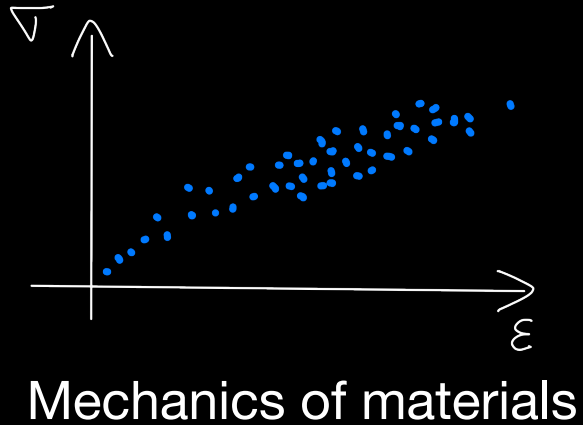
Simple experiments

# Model-free Mechanics of Materials



Rich experiments

# Model-free Mechanics of Materials



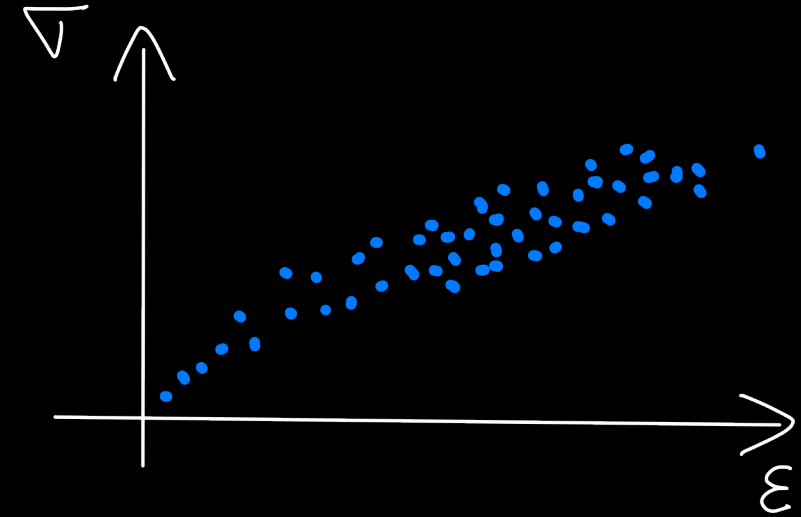
Rich experiments

$$\Psi(\lambda_1, \lambda_2, \lambda_3) = \sum_p \frac{\mu_p}{\alpha_p} (\lambda_1^{\alpha_p} + \lambda_2^{\alpha_p} + \lambda_3^{\alpha_p} - 3)$$

No constitutive models

# Outline

- Getting the data



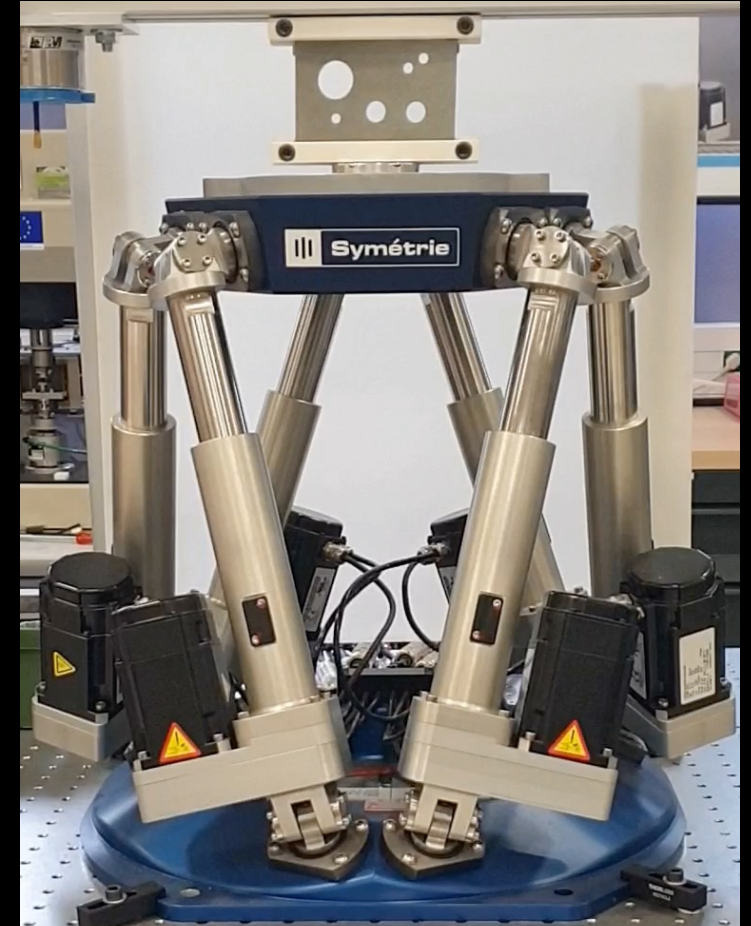
- Learning *from* the data

$$\Psi(\lambda_1, \lambda_2, \lambda_3) = \sum_p \frac{\mu_p}{\alpha_p} (\lambda_1^{\alpha_p} + \lambda_2^{\alpha_p} + \lambda_3^{\alpha_p} - 3)$$

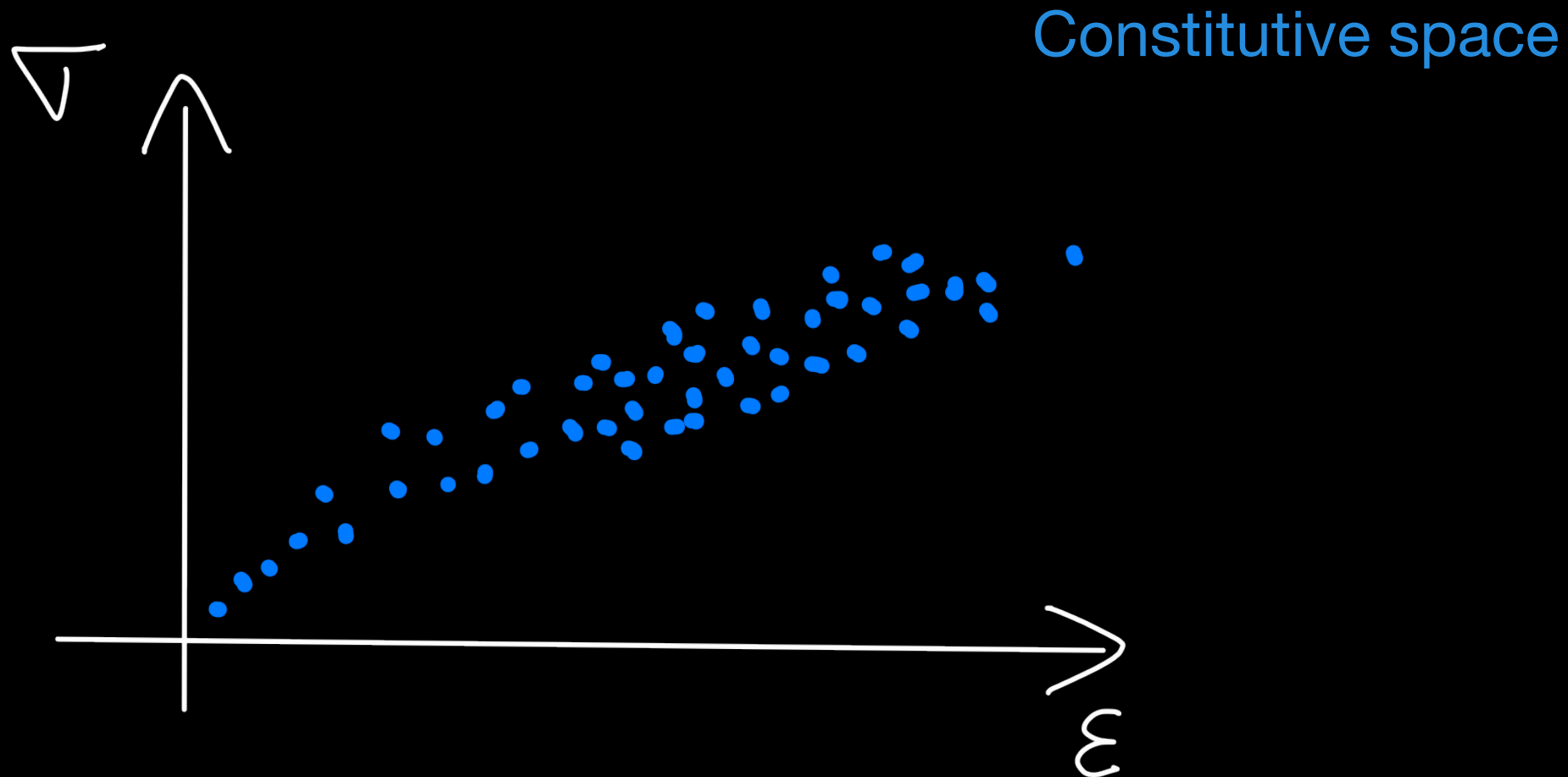
Getting the data

# Acquiring strain-stress data

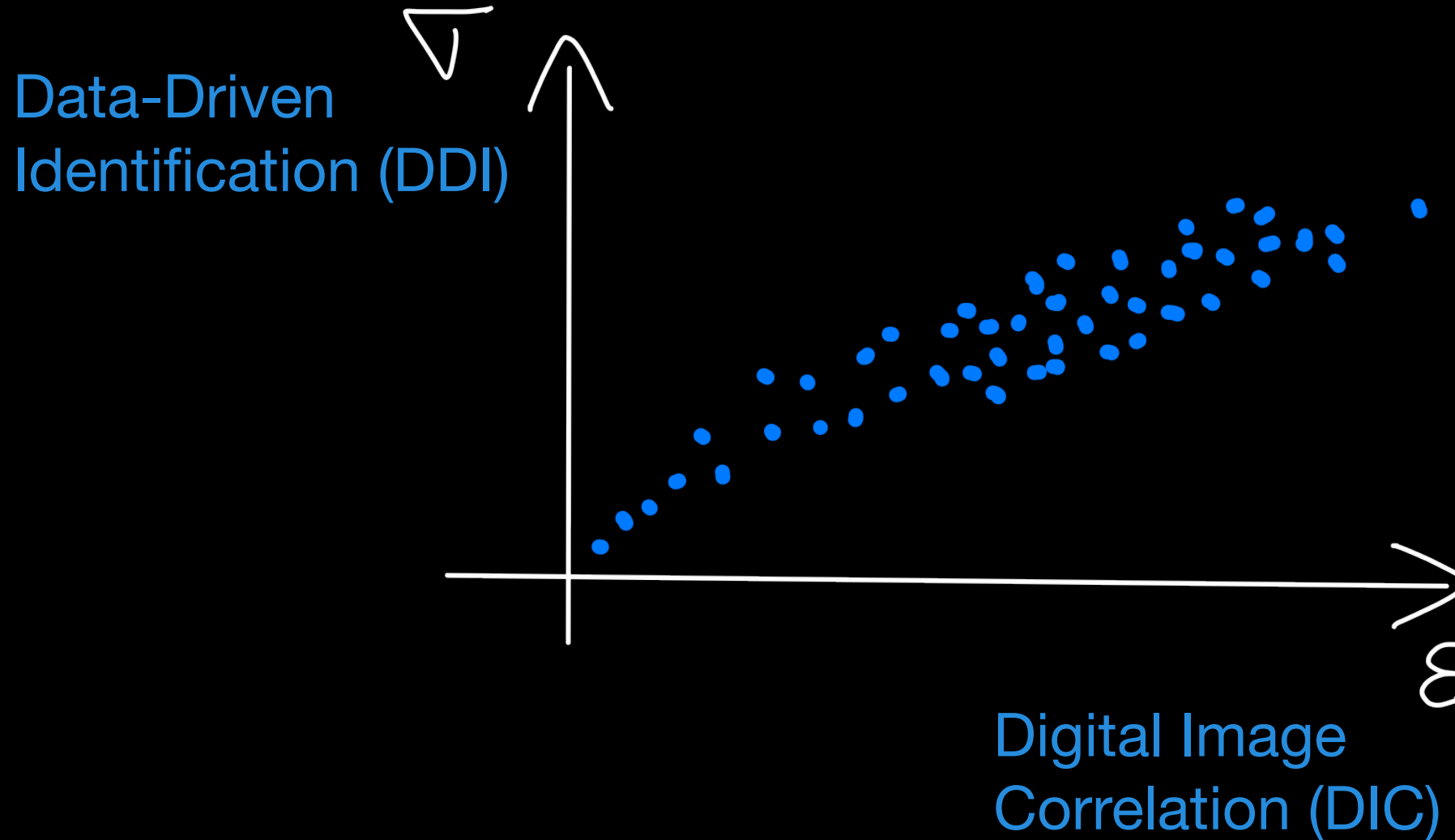
- Complex geometry
- Complex loading path
- Optical camera (not shown)
- 6-axis load cell measurements
- Multiple loading steps: snapshots



# Acquiring strain-stress data

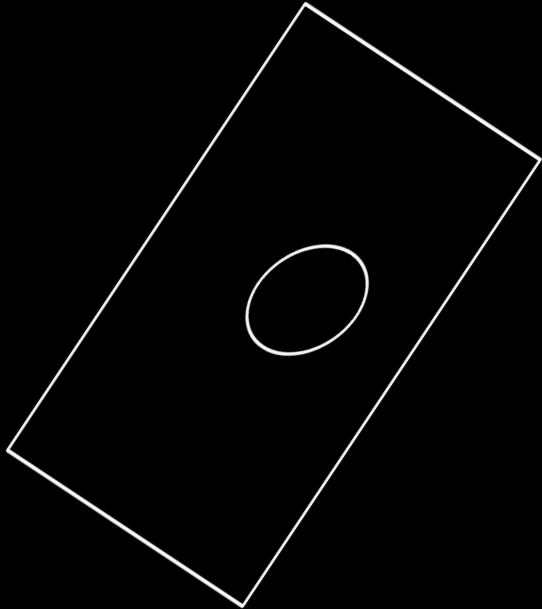
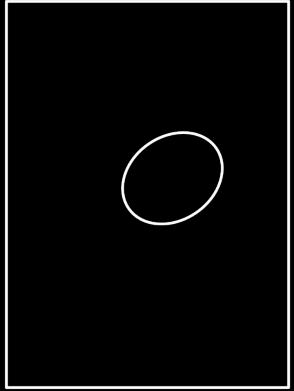


# Acquiring strain-stress data



Sutton et al (2009)  
Leygue et al (2018)

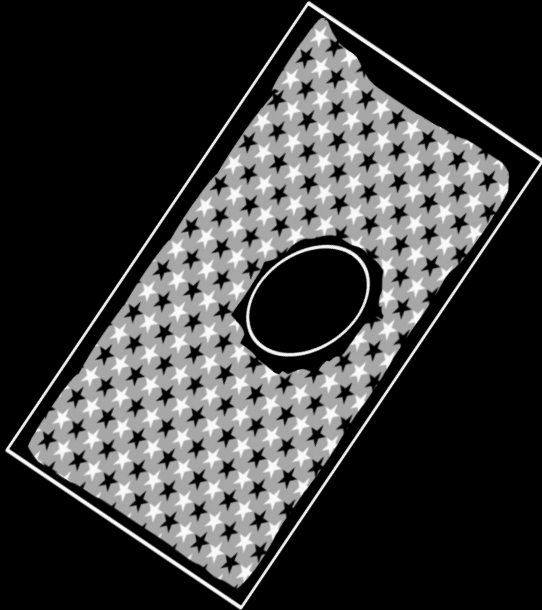
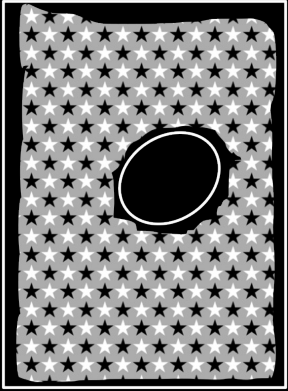
# Digital Image Correlation (DIC)



- Quantity of interest

$\vec{u}$

# Digital Image Correlation (DIC)

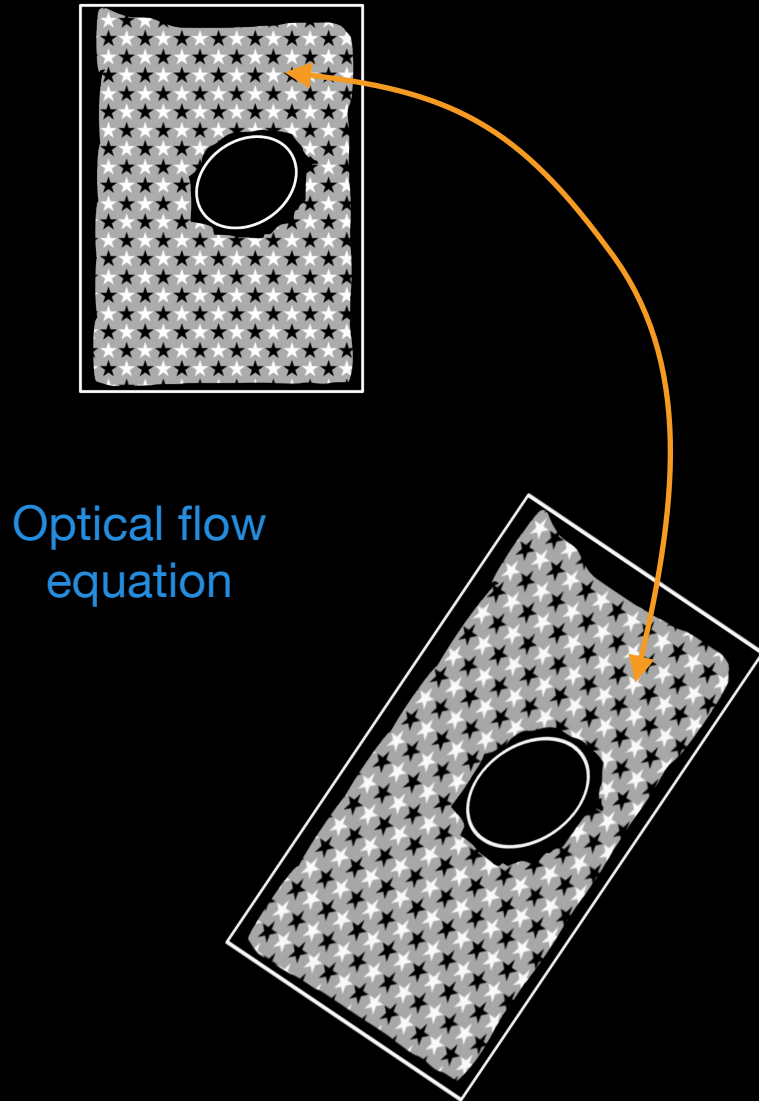


- Quantity of interest
- Auxiliary field

$$\vec{u}$$

$$I(x)$$

# Digital Image Correlation (DIC)



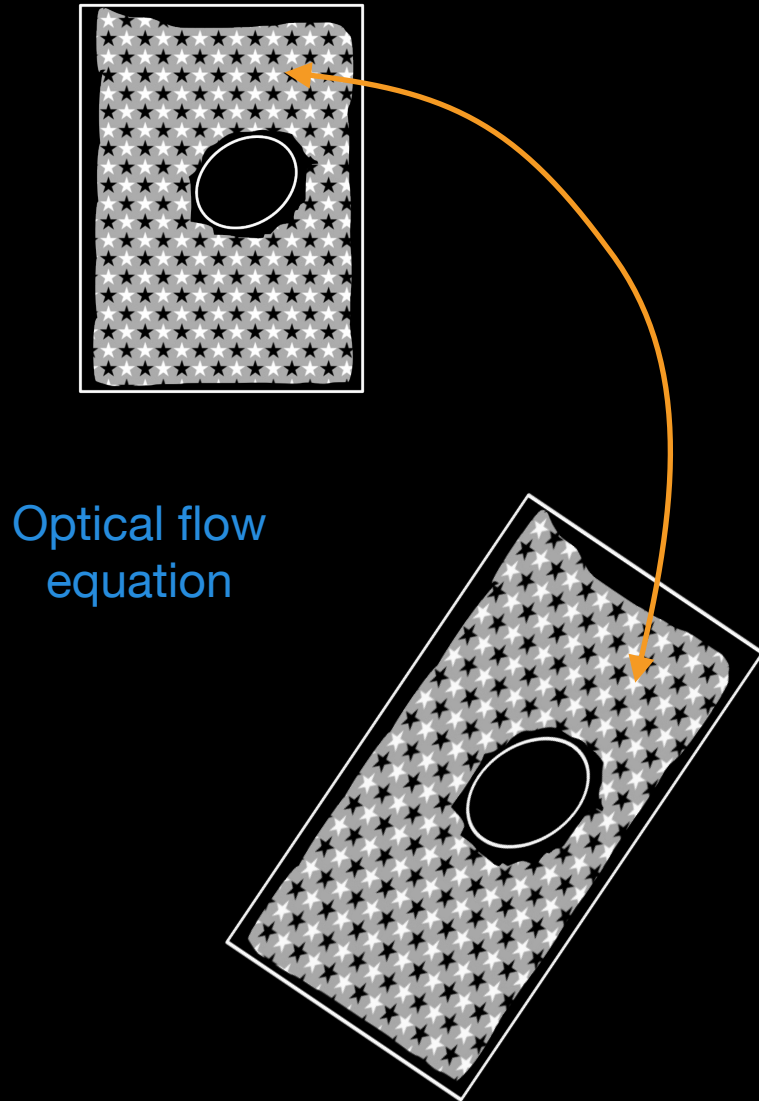
- Quantity of interest
- Auxiliary field
- Balance principle

$$\vec{u}$$

$$I(x)$$

$$I(\vec{x}, t) = I(\vec{x} + \vec{u}, t + \Delta t)$$

# Digital Image Correlation (DIC)



- Quantity of interest
- Auxiliary field
- Balance principle

$$\vec{u}$$

$$I(x)$$

$$\vec{\text{grad}}(I) \cdot \vec{u} + \Delta I = 0$$

# Digital Image Correlation (DIC)



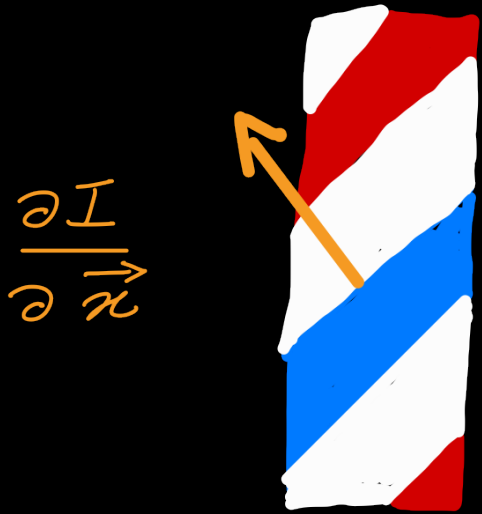
- Quantity of interest
- Auxiliary field
- Balance principle

$$\vec{u}$$

$$I(x)$$

$$\vec{\text{grad}}(I) \cdot \vec{u} + \Delta I = 0$$

# Digital Image Correlation (DIC)



- Quantity of interest

$\vec{u}$

- Auxiliary field

$I(x)$

- Balance principle

$$\vec{\text{grad}}(I) \cdot \vec{u} + \Delta I = 0$$

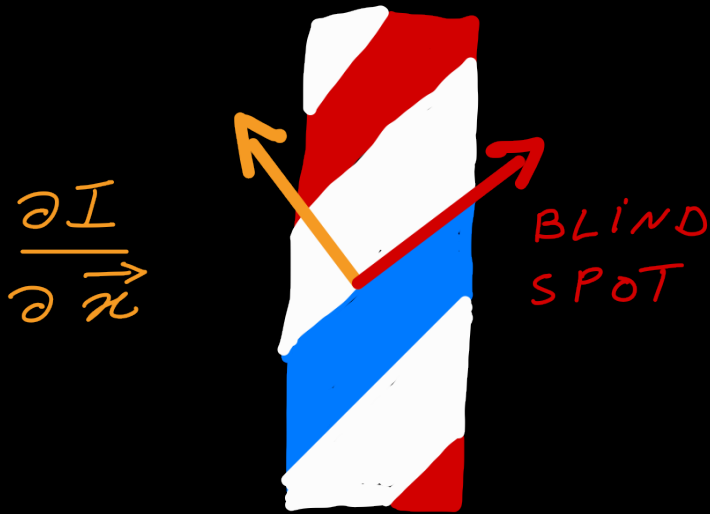
# Digital Image Correlation (DIC)

- Quantity of interest
- Auxiliary field
- Balance principle

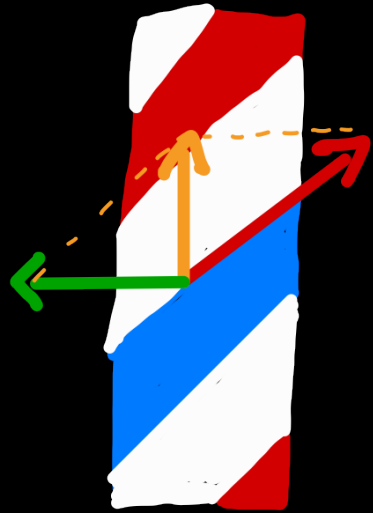
$$\vec{u}$$

$$I(x)$$

$$\vec{\text{grad}}(I) \cdot \vec{u} + \Delta I = 0$$



# Digital Image Correlation (DIC)



- Quantity of interest

$$\vec{u}$$

- Auxiliary field

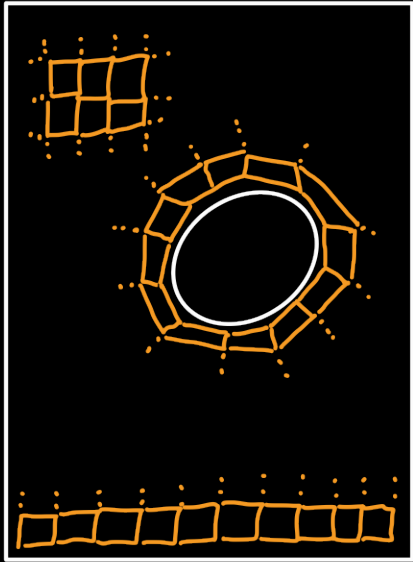
$$I(x)$$

- Balance principle

$$\vec{\text{grad}}(I) \cdot \vec{u} + \Delta I = 0$$

# Digital Image Correlation (DIC)

FE MESH



Close points in physical space  
Have similar displacement

- Quantity of interest

$$\vec{u}$$

- Auxiliary field

$$I(x)$$

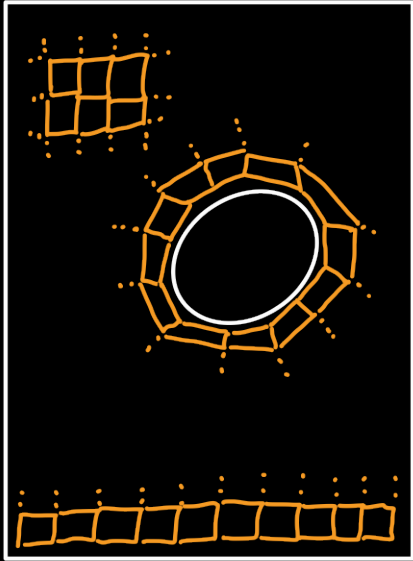
- Balance principle

$$\vec{\text{grad}}(I) \cdot \vec{u} + \Delta I = 0$$

- Regularization

$$\vec{u}(\vec{x}) \simeq \Phi_i(\vec{x}) \vec{U}_i$$

# Digital Image Correlation (DIC)



Best regularized displacement field?

- Quantity of interest

$$\vec{u}$$

- Auxiliary field

$$I(x)$$

- Balance principle

$$\vec{\text{grad}}(I) \cdot \vec{u} + \Delta I = 0$$

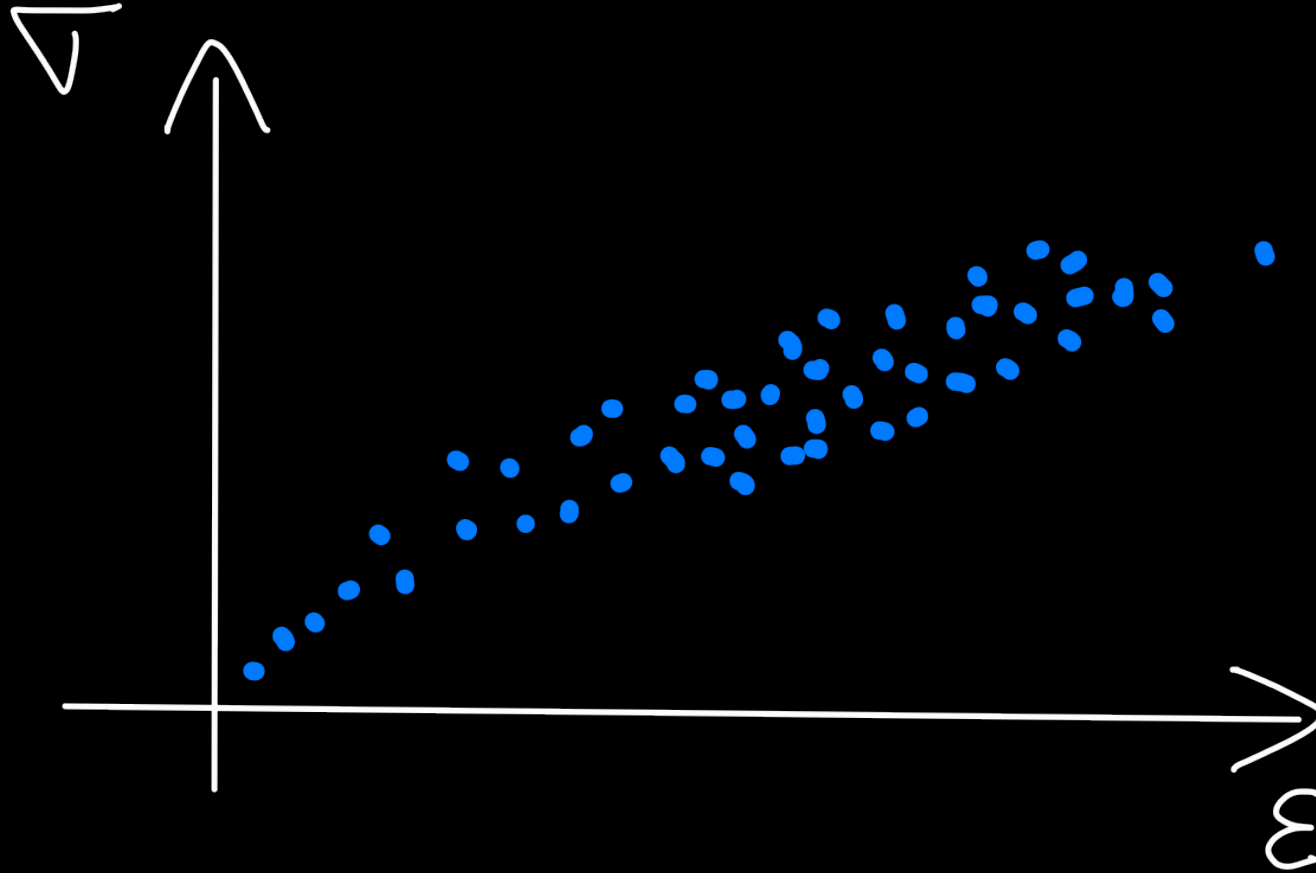
- Regularization

$$\vec{u}(\vec{x}) \simeq \Phi_i(\vec{x}) \vec{U}_i$$

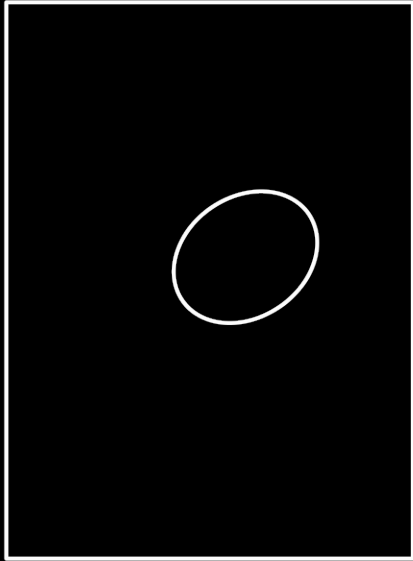
- Minimization

$$\min_{\vec{U}_i} \left\| \vec{\text{grad}}(I) \cdot \left( \Phi_k \vec{U}_k \right) + \Delta I \right\|_2^2$$

# Acquiring strain-stress data



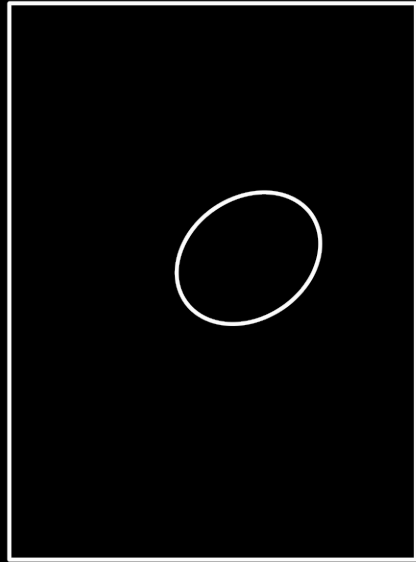
# Data Driven Identification (DDI)



- Quantity of interest

Q11

# Data Driven Identification (DDI)

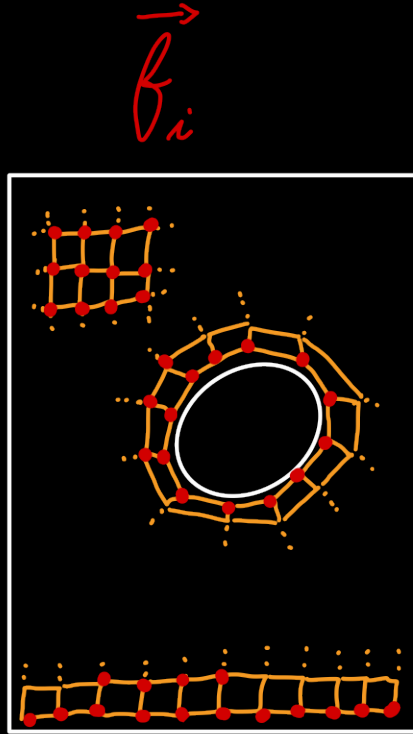


The stress field is identified simultaneously for all loading steps

- Quantity of interest

$Q_{II}$

# Data Driven Identification (DDI)



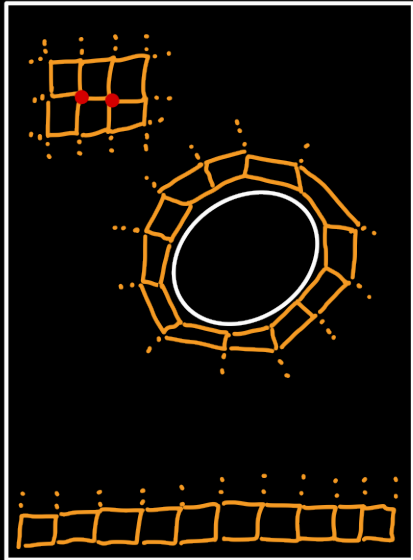
- Quantity of interest
- Auxiliary field

$$\vec{\sigma}$$

$$\vec{f}(\vec{x})$$

# Data Driven Identification (DDI)

$$\vec{f}_i = \vec{0}$$



- Quantity of interest
- Auxiliary field
- Balance principle

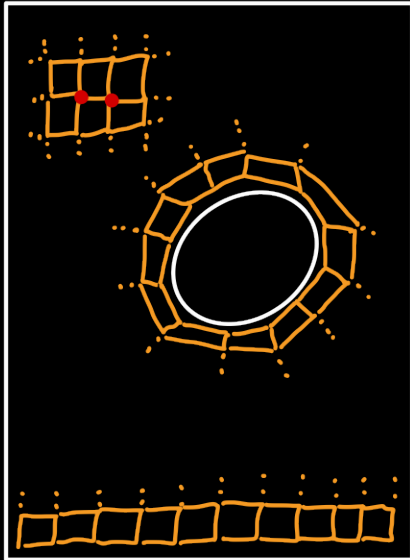
$$\vec{\sigma}$$

$$\vec{f}(\vec{x})$$

$$\text{div}(\vec{\sigma}) + \vec{f} = \vec{0}$$

# Data Driven Identification (DDI)

$$\vec{f}_i = \vec{0}$$



- Quantity of interest
- Auxiliary field
- Balance principle

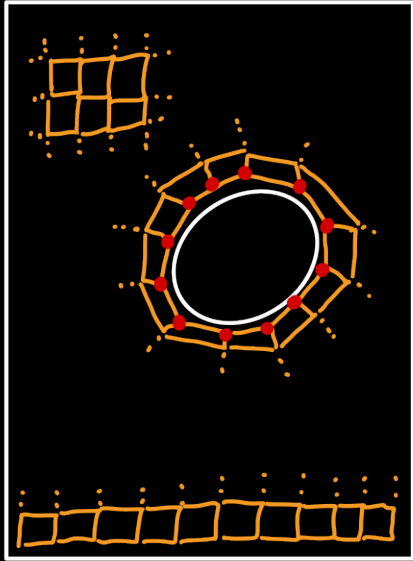
$$\vec{\sigma}$$

$$\vec{f}(\vec{x})$$

$$\vec{D}(\vec{\sigma}) + \vec{f} = \vec{0}$$

# Data Driven Identification (DDI)

$$\sum \vec{f}_i = \vec{0}$$



- Quantity of interest
- Auxiliary field
- Balance principle

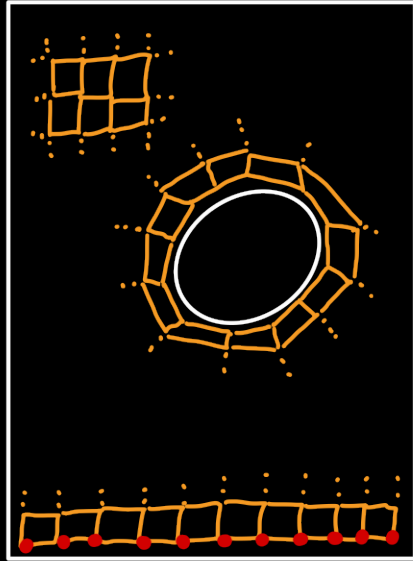
$$\vec{\sigma}$$

$$\vec{f}(\vec{x})$$

$$\vec{D}(\vec{\sigma}) + \vec{f} = \vec{0}$$

# Data Driven Identification (DDI)

$$\sum \vec{f}_i = \vec{F}_{xp}$$



$$\vec{F}_{xp}$$

- Quantity of interest
- Auxiliary field
- Balance principle

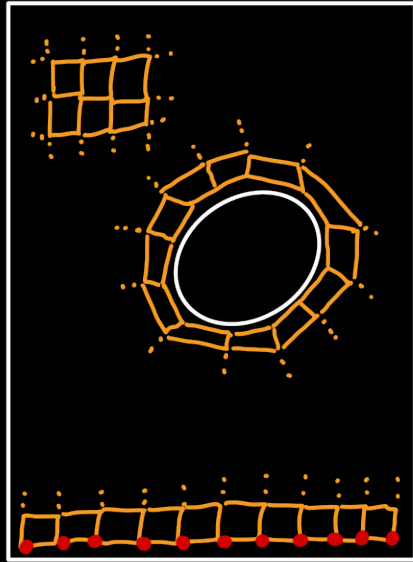
$$\vec{\sigma}$$

$$\vec{f}(\vec{x})$$

$$\vec{D}(\vec{\sigma}) + \vec{f} = \vec{0}$$

# Data Driven Identification (DDI)

$$\sum \vec{f}_i = \vec{F}_{xp}$$



$$\vec{F}_{xp}$$

Blind spot = Ker(D)

- Quantity of interest
- Auxiliary field
- Balance principle

$$\vec{\sigma}$$

$$\vec{f}(\vec{x})$$

$$\vec{D}(\vec{\sigma}) + \vec{f} = \vec{0}$$

# Data Driven Identification (DDI)

- Quantity of interest

$$\bar{\sigma}$$

- Auxiliary field

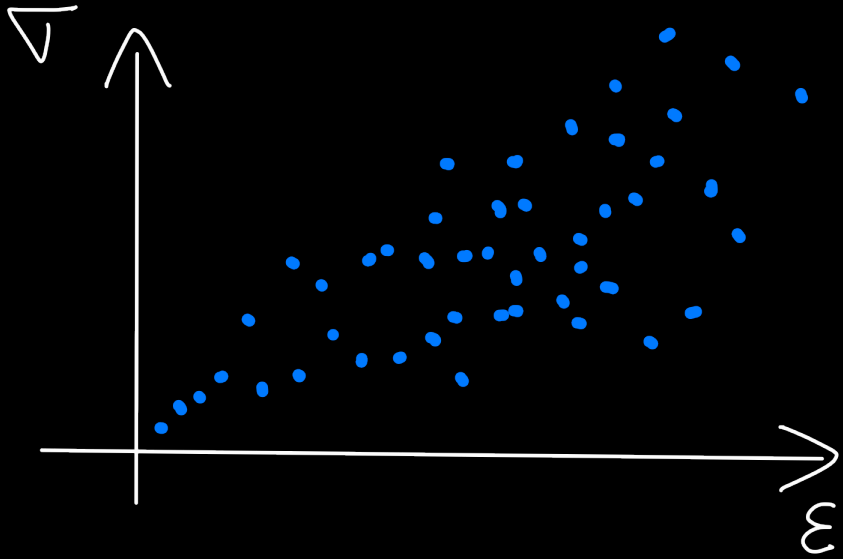
$$\vec{f}(\vec{x})$$

- Balance principle

$$\vec{D}(\bar{\sigma}) + \vec{f} = \vec{0}$$

- Regularization

# Data Driven Identification (DDI)



- Quantity of interest
- Auxiliary field
- Balance principle
- Regularization

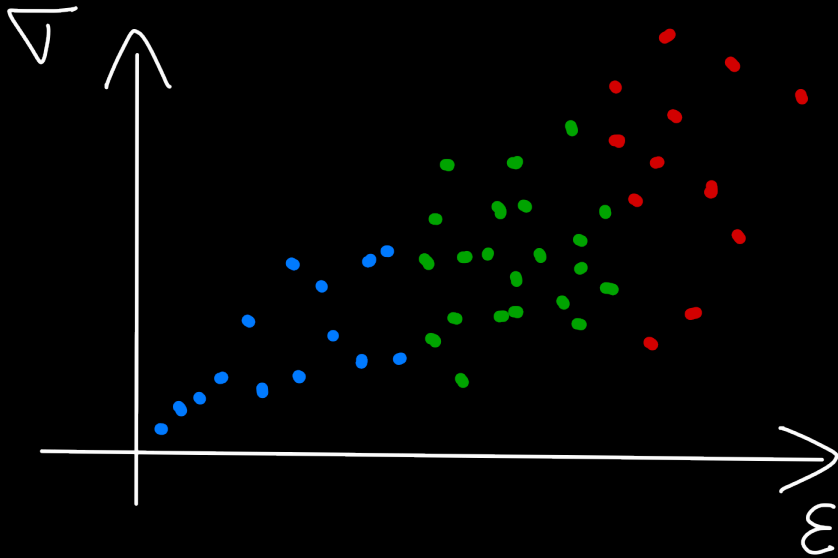
$$\bar{\bar{\sigma}}$$

$$\vec{f}(\vec{x})$$

$$\vec{D}(\bar{\bar{\sigma}}) + \vec{f} = \vec{0}$$

$$\bar{\bar{\sigma}}(\bar{\bar{\epsilon}}) \simeq \Phi_k(\bar{\bar{\epsilon}}) \bar{\bar{\mathcal{S}}}_k$$

# Data Driven Identification (DDI)



Introduce a clustering in  
constitutive space

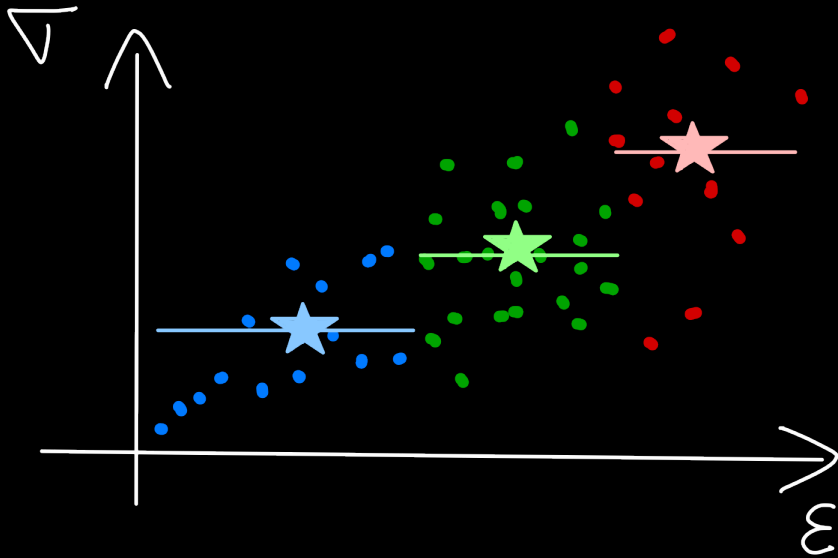
- Quantity of interest
- Auxiliary field
- Balance principle
- Regularization

$$\bar{\sigma}$$

$$\vec{f}(\vec{x})$$

$$\vec{D}(\bar{\sigma}) + \vec{f} = \vec{0}$$

# Data Driven Identification (DDI)



Piecewise constant regularization  
in constitutive space

- Quantity of interest
- Auxiliary field
- Balance principle
- Regularization

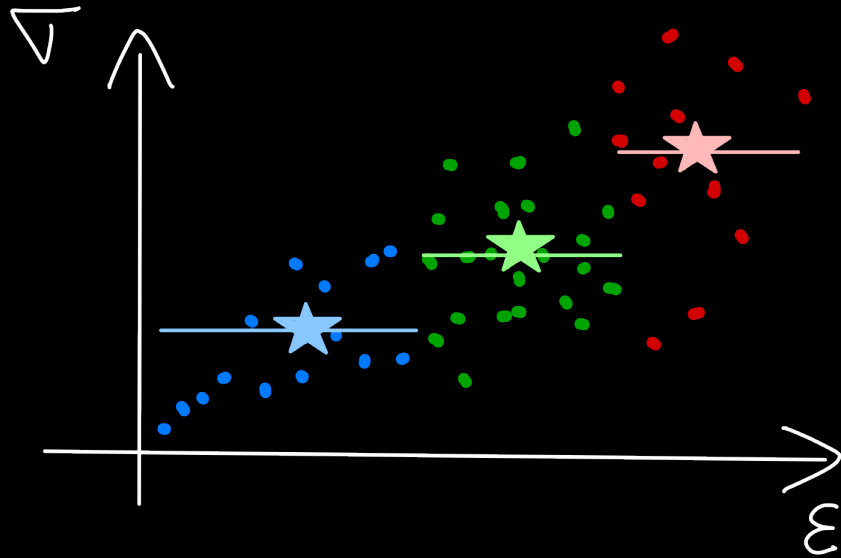
$$\bar{\bar{\sigma}}$$

$$\vec{f}(\vec{x})$$

$$\vec{D}(\bar{\bar{\sigma}}) + \vec{f} = \vec{0}$$

$$\bar{\bar{\sigma}}(\bar{\bar{\epsilon}}) \simeq \Phi_k(\bar{\bar{\epsilon}}) \bar{\bar{S}}_k$$

# Data Driven Identification (DDI)



Piecewise constant regularization  
in constitutive space

- Quantity of interest
- Auxiliary field
- Balance principle
- Regularization

$$\bar{\sigma}$$

$$\vec{f}(\vec{x})$$

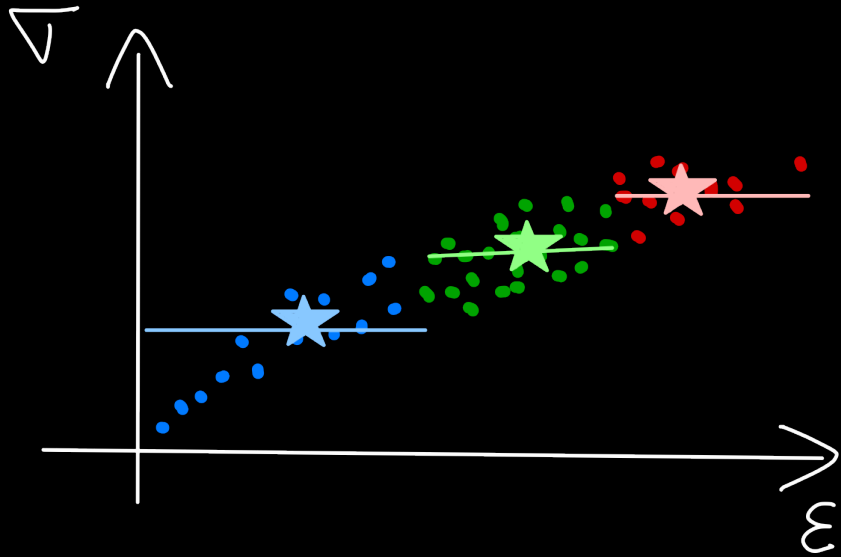
$$\vec{D}(\bar{\sigma}) + \vec{f} = \vec{0}$$

$$\bar{\sigma}(\bar{\epsilon}) \simeq \Phi_k(\bar{\epsilon}) \bar{\mathcal{S}}_k$$

● mechanical states

★ material states  
database

# Data Driven Identification (DDI)



Minimize the distance between  
a stress field at equilibrium  
and a regularized field

- Quantity of interest

$$\bar{\bar{\sigma}}$$

- Auxiliary field

$$\vec{f}(\vec{x})$$

- Balance principle

$$\vec{D}(\bar{\bar{\sigma}}) + \vec{f} = \vec{0}$$

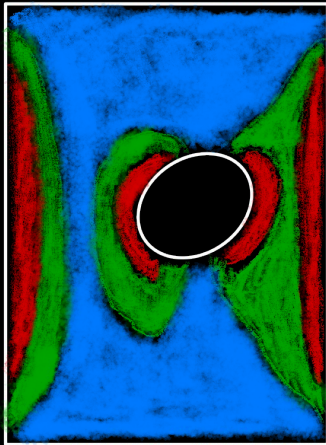
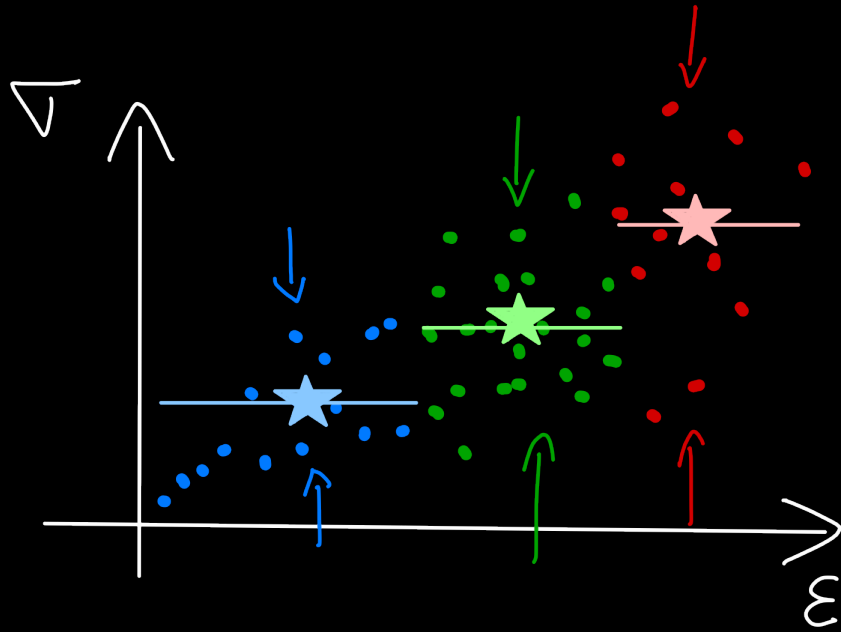
- Regularization

$$\bar{\bar{\sigma}}(\bar{\bar{\epsilon}}) \simeq \Phi_k(\bar{\bar{\epsilon}}) \bar{\bar{\mathcal{S}}}_k$$

- Minimization

$$\min_{\bar{\bar{\mathcal{S}}}_i, \bar{\bar{\sigma}}} \left\| \bar{\bar{\sigma}} - \Phi_k \bar{\bar{\mathcal{S}}}_k \right\|_{\mathbb{C}}^2 \quad \& \quad \vec{D}(\bar{\bar{\sigma}}) + \vec{f} = \vec{0}$$

# DDI Blind Spot?



- Minimization problem

$$\min_{\bar{\bar{\mathcal{S}}}_i, \bar{\bar{\sigma}}} \left\| \bar{\bar{\sigma}} - \Phi_k \bar{\bar{\mathcal{S}}}_k \right\|_{\mathbb{C}}^2 \quad \& \quad \vec{D}(\bar{\bar{\sigma}}) + \vec{f} = \vec{0}$$

- Equivalent formulation

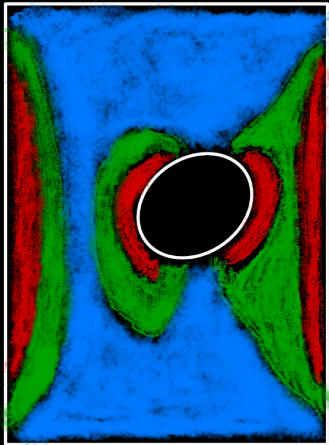
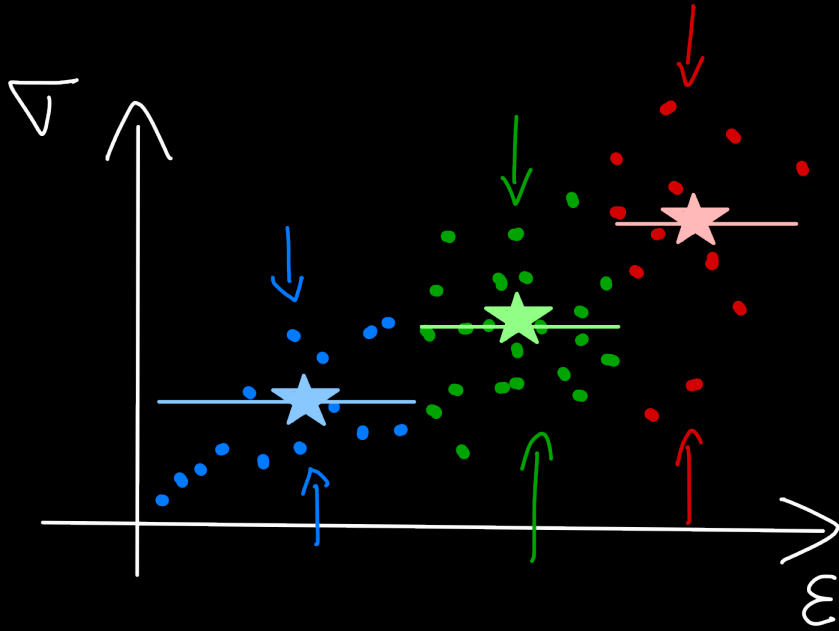
$$\sigma = \arg \min_{\sigma} \frac{1}{2} \sigma^T H \sigma$$

$$\& \quad D\sigma = f$$

- Solution is unique if

$$\text{Ker } H \cap \text{Ker } D = \{0\}$$

# Some results



- Equivalent formulation

$$\sigma = \arg \min_{\sigma} \frac{1}{2} \sigma^T H \sigma$$
$$\& \quad D\sigma = f$$

- Loss of uniqueness

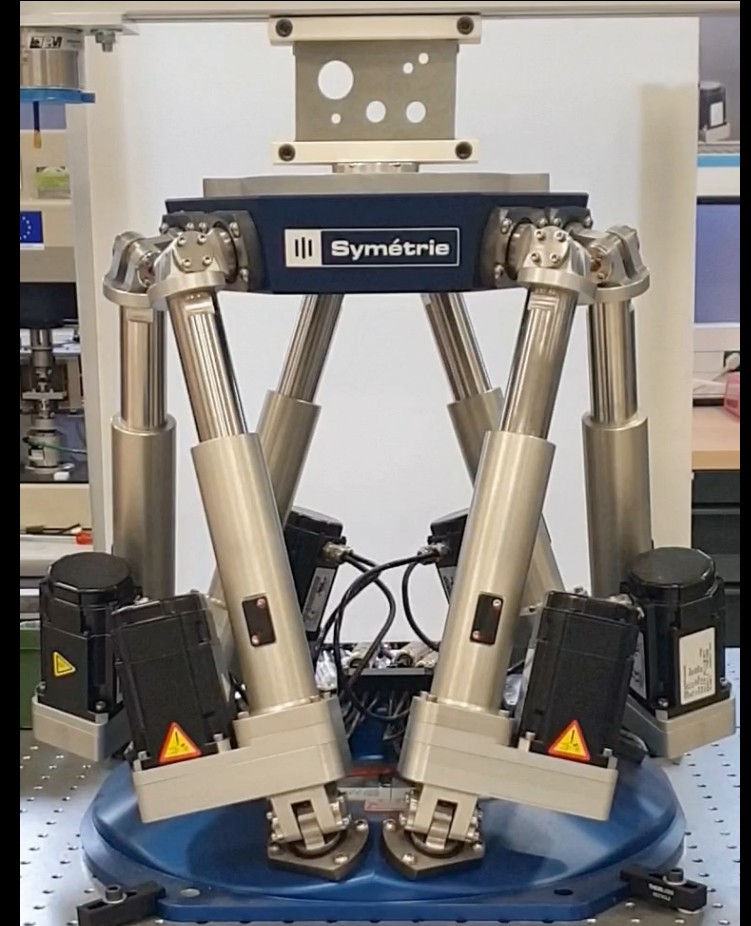
$$\text{Ker } H \cap \text{Ker } D \neq \{0\}$$

- The geometry is too simple
- The clustering is too fine
- The strain data is not rich enough
- Efficient alternated projection algorithms

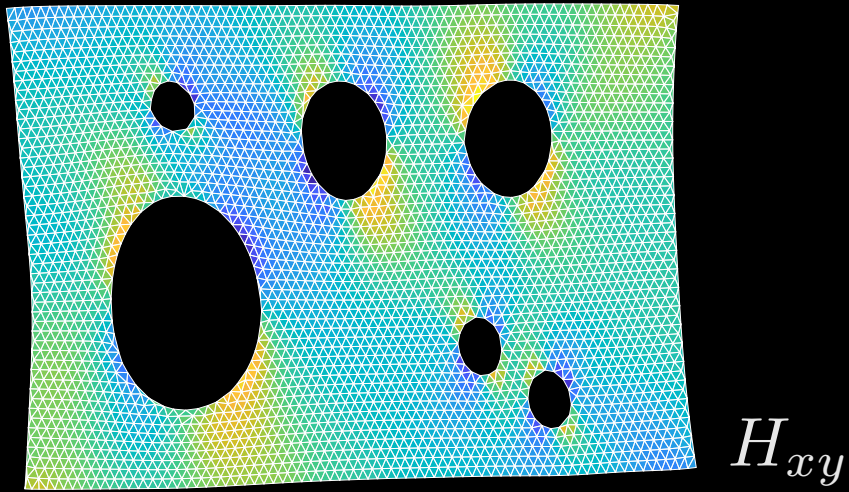
Learning *from* the data

# Experimental setup

- Membrane with holes
- Carbon black-filled polychloroprene (Joreau elastomers)
- New vs. aged 21 days at 100°C
- Symétrie hexapod
- Quasi-static “monotonous” in-plane loading
- Incompressibility & plane stress assumed
- DIC with Ufreckles (J. Réthoré)
- 622 snapshots
- ~6000 elements mesh → over 3.5 million points

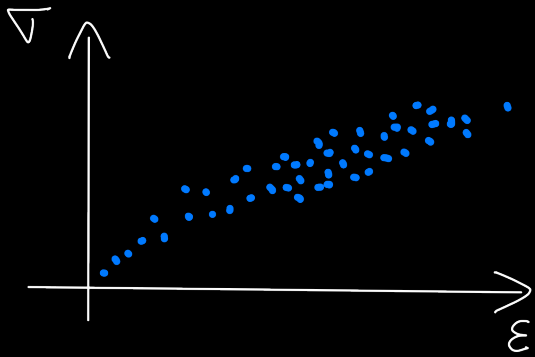


# Kinematics



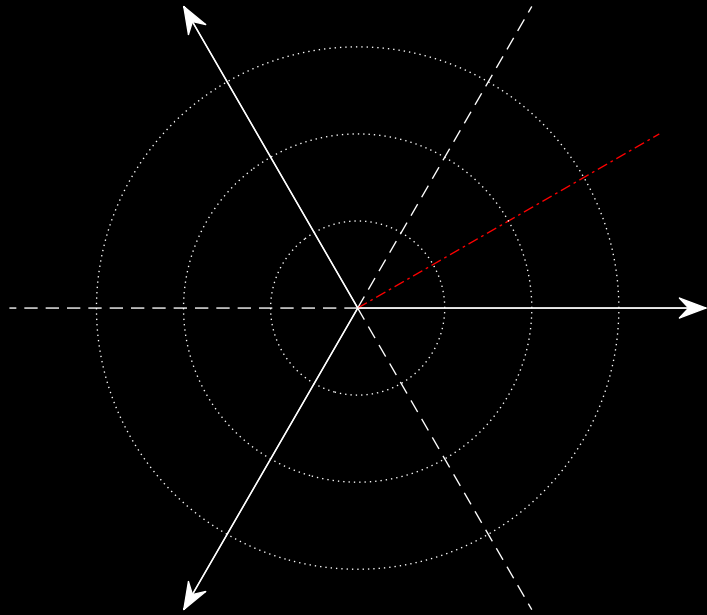
- Strain tensor

$$\bar{\bar{H}} = \frac{1}{2} \ln \left( \bar{\bar{F}} \cdot \bar{\bar{F}}^T \right)$$



Representation in 3D(strain) x 3D (stress) ?

# Kinematics



- Strain tensor

$$\bar{\bar{H}} = \frac{1}{2} \ln \left( \bar{\bar{F}} \cdot \bar{\bar{F}}^T \right)$$

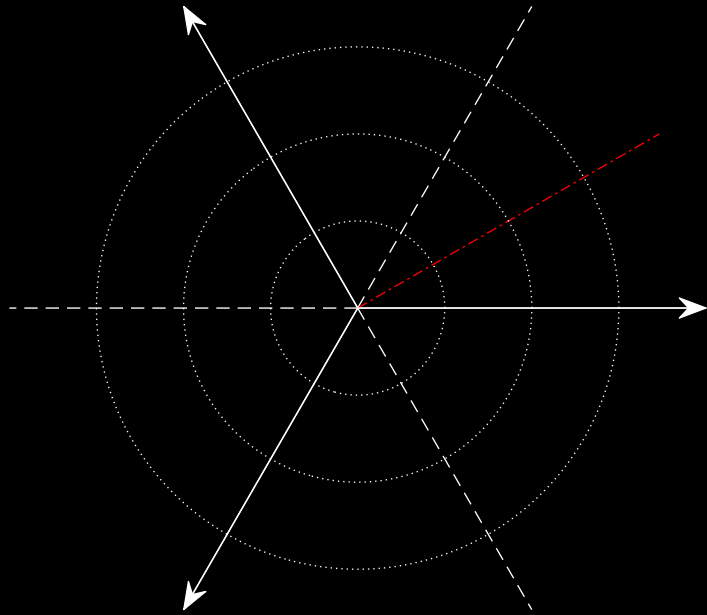
- Haigh-Westergaard representation

$$z = \text{tr} \bar{\bar{H}}$$

$$r = \sqrt{\text{dev} \bar{\bar{H}} : \text{dev} \bar{\bar{H}}}$$

$$\cos(3\theta) = \frac{3\sqrt{6}}{r^3} \det \left( \text{dev} \bar{\bar{H}} \right)$$

# Kinematics



- Strain tensor

$$\bar{\bar{H}} = \frac{1}{2} \ln \left( \bar{\bar{F}} \cdot \bar{\bar{F}}^T \right)$$

- Haigh-Westergaard representation

$$z = \text{tr} \bar{\bar{H}}$$

$$r = \sqrt{\text{dev} \bar{\bar{H}} : \text{dev} \bar{\bar{H}}}$$

$$\cos(3\theta) = \frac{3\sqrt{6}}{r^3} \det \left( \text{dev} \bar{\bar{H}} \right)$$

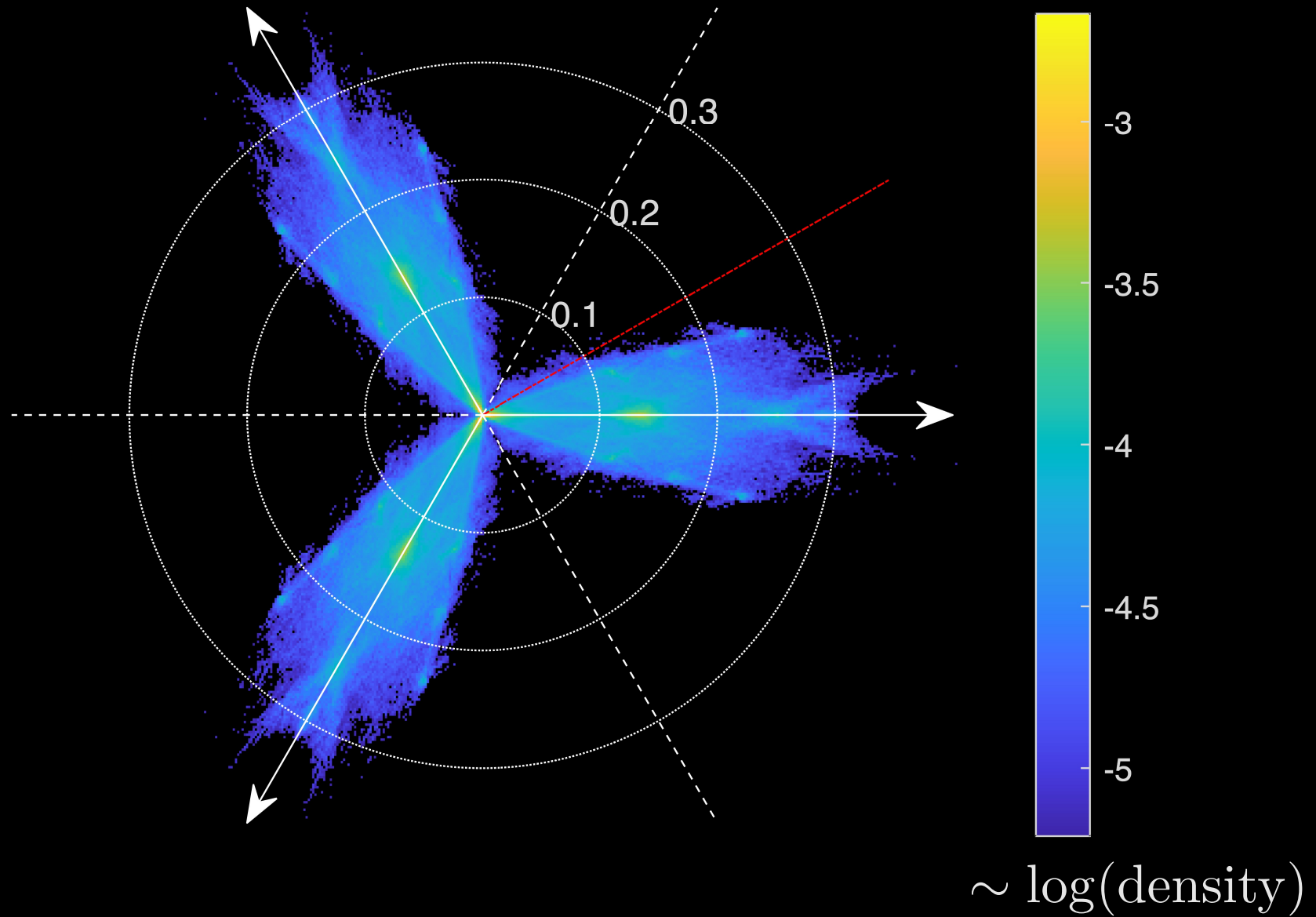
- Interpretation

$$\theta = 0 \quad \text{uniaxial tension}$$

$$\theta = \pi/6 \quad \text{pure shear}$$

$$\theta = \pi/3 \quad \text{equibiaxial tension}$$

# Kinematics



# DDI details

- Minimization problem:

$$\min_{\bar{\bar{\mathcal{S}}}_i, \bar{\bar{\sigma}}} \left\| \bar{\bar{\sigma}} - \Phi_k \bar{\bar{\mathcal{S}}}_k \right\|_{\mathbb{C}}^2 \quad \& \quad \vec{D}(\bar{\bar{\sigma}}) + \vec{f} = \vec{0}$$

- 2-norm:

$$\mathbb{C} = \mathbb{I}$$

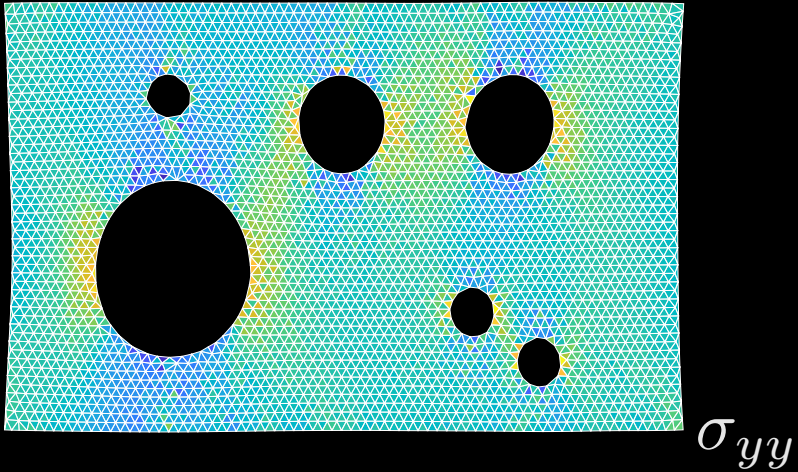
- Clustering

k-means

$\bar{\bar{H}}$ -based

3.5k clusters (ratio=1000)

# Stress field



- Stress tensor

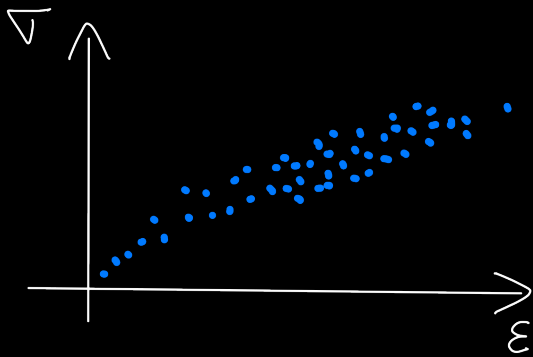
$$\bar{\bar{\sigma}}$$

- Orientation

Misorientation w.r.t. strain

- Strain energy density (hyperelastic hypothesis)

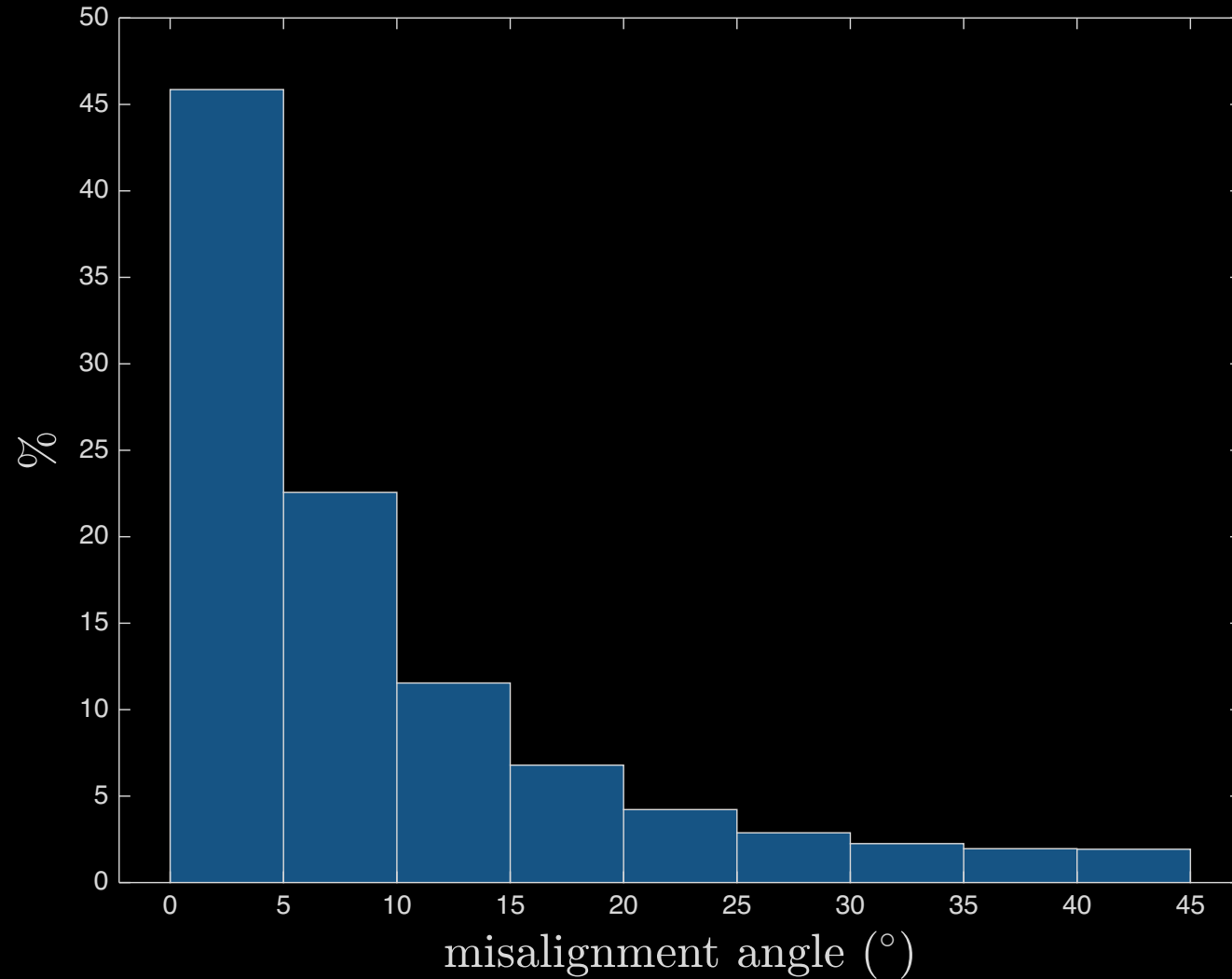
$$W(\bar{\bar{H}}) = \int_0^t \bar{\bar{\sigma}} : \bar{\bar{D}} dt'$$



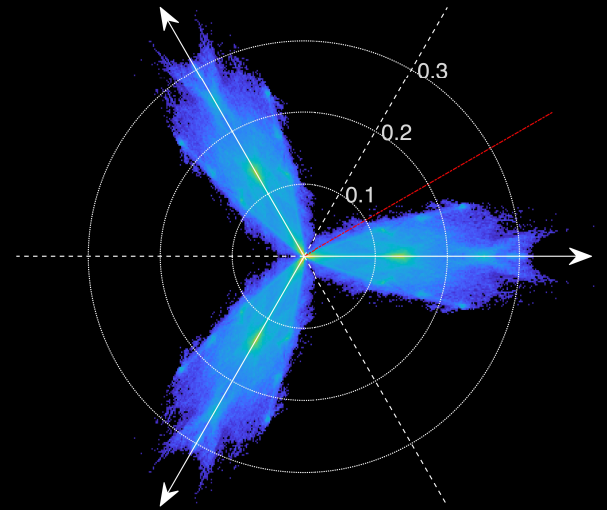
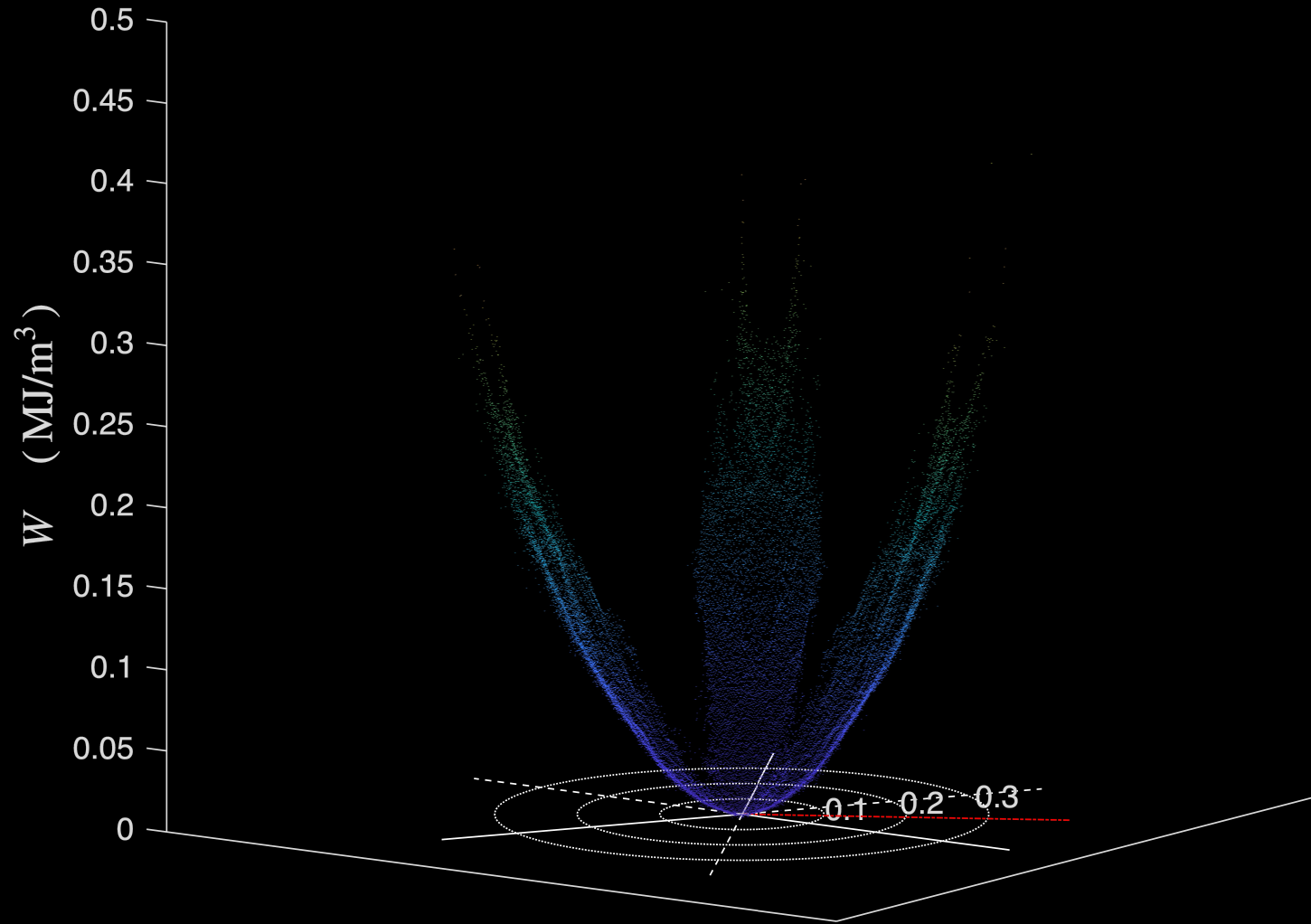
Representation in 3D(strain) x 3D (stress) ?

# Isotropy

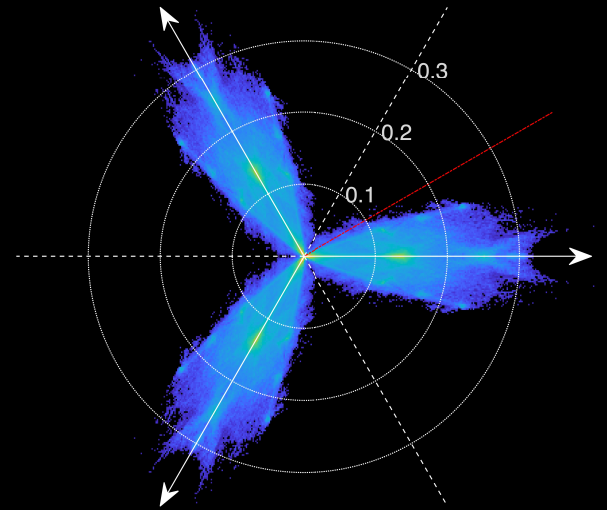
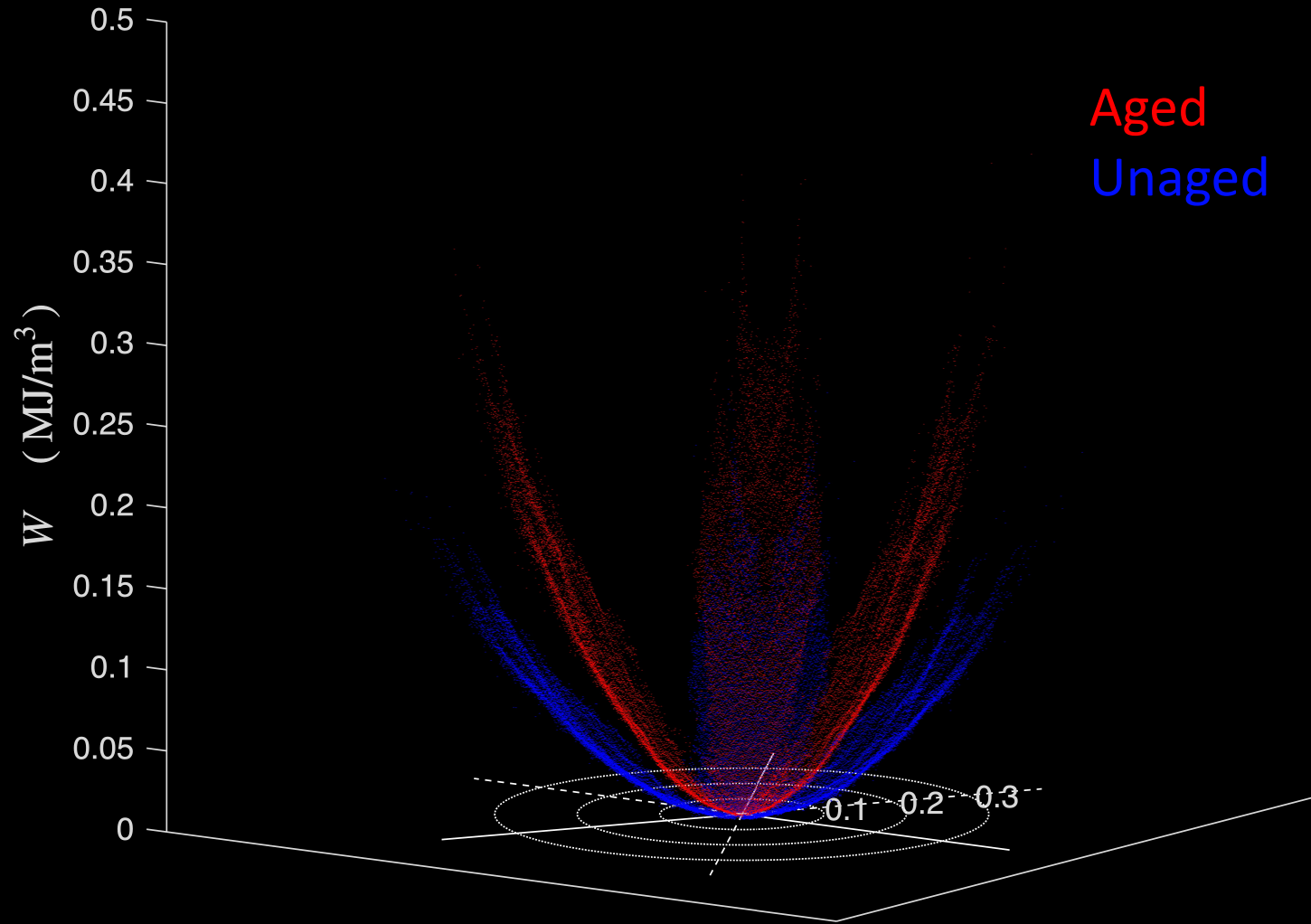
Strain-stress alignment?



# Strain energy density

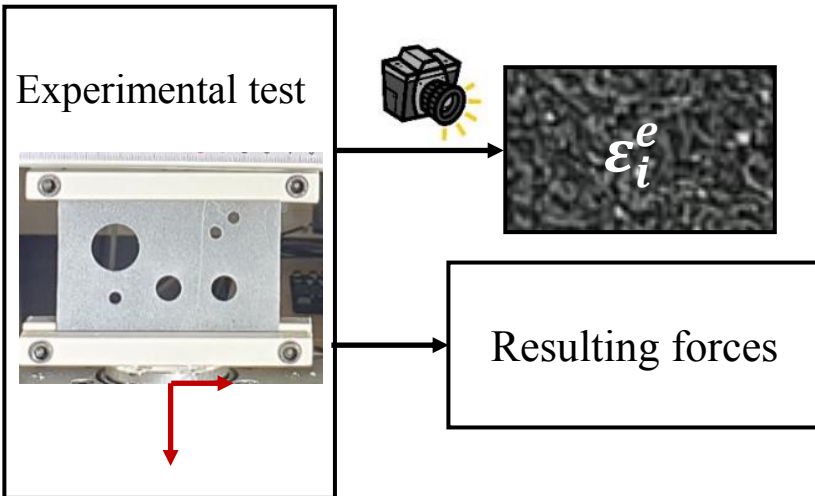


# Aged vs. unaged

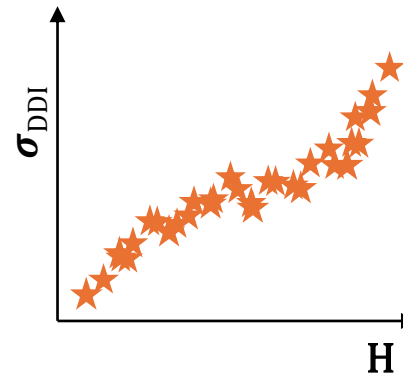


# Data-Driven (Model) Identification

## Step 1: Inhomogeneous experiment



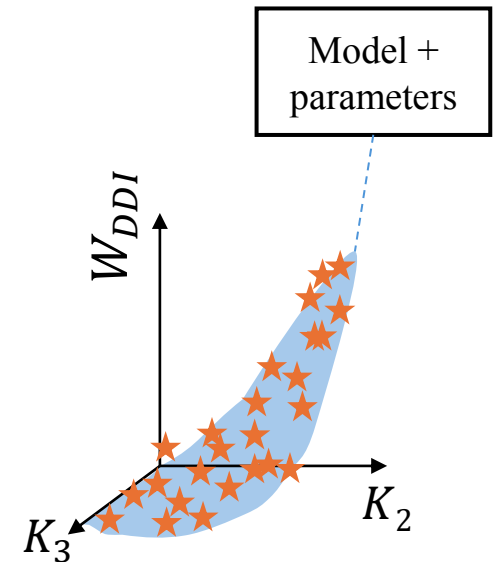
## Step 2: Model-free stress and strain energy estimation



+

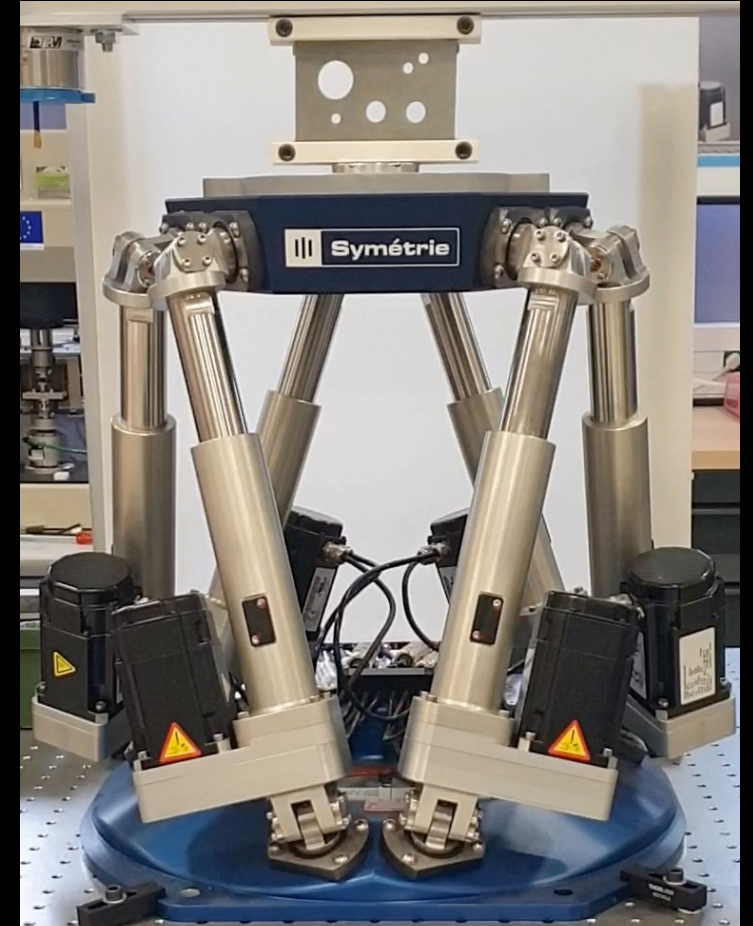
$$W_{DDI}^t = \int_0^t \sigma_{DDI} : \mathbf{D} dt$$

## Step 3: Model choice and parameters fit

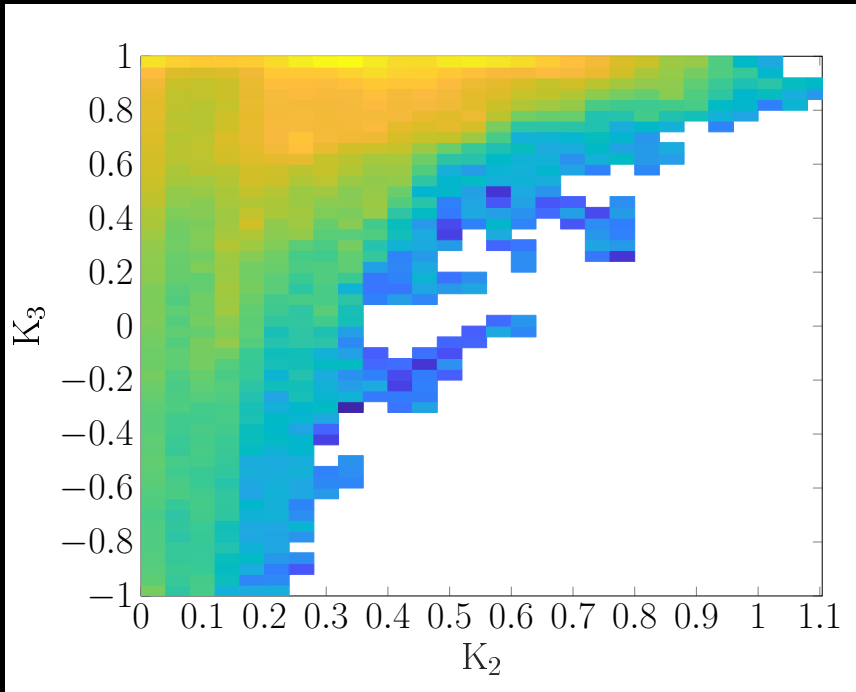


# Experimental setup

- Membrane with holes (65 x 100 x 1.6 mm)
- Carbon black-filled SBR (Michelin)
- Symétrie hexapod
- Quasi-static “monotonous” in-plane loading
- Incompressibility & plane stress assumed
- DIC with Ufreckles (J. Réthoré)
- 1000 snapshots
- ~3400 elements mesh → over 3.4 million points



# Kinematics



- Strain tensor

$$\bar{\bar{H}} = \frac{1}{2} \ln \left( \bar{\bar{F}} \cdot \bar{\bar{F}}^T \right)$$

- Invariants by Criscione (2000)

$$K_1 = \text{tr} \bar{\bar{H}}$$

$$K_2 = \sqrt{\text{dev} \bar{\bar{H}} : \text{dev} \bar{\bar{H}}}$$

$$K_3 = \frac{3\sqrt{6}}{K_2^3} \det \left( \text{dev} \bar{\bar{H}} \right)$$

- Interpretation

$$K_3 = 1 \quad \text{uniaxial tension}$$

$$K_3 = 0 \quad \text{pure shear}$$

$$K_3 = -1 \quad \text{equibiaxial tension}$$

# DDI details

- Minimization problem:

$$\min_{\bar{\bar{\mathcal{S}}}_i, \bar{\bar{\sigma}}} \left\| \bar{\bar{\sigma}} - \Phi_k \bar{\bar{\mathcal{S}}}_k \right\|_{\mathbb{C}}^2 \quad \& \quad \vec{D}(\bar{\bar{\sigma}}) + \vec{f} = \vec{0}$$

- 2-norm

$\mathbb{C}$  pseudo elasticity tensor with  $\nu = 0.5$

- Clustering

k-means

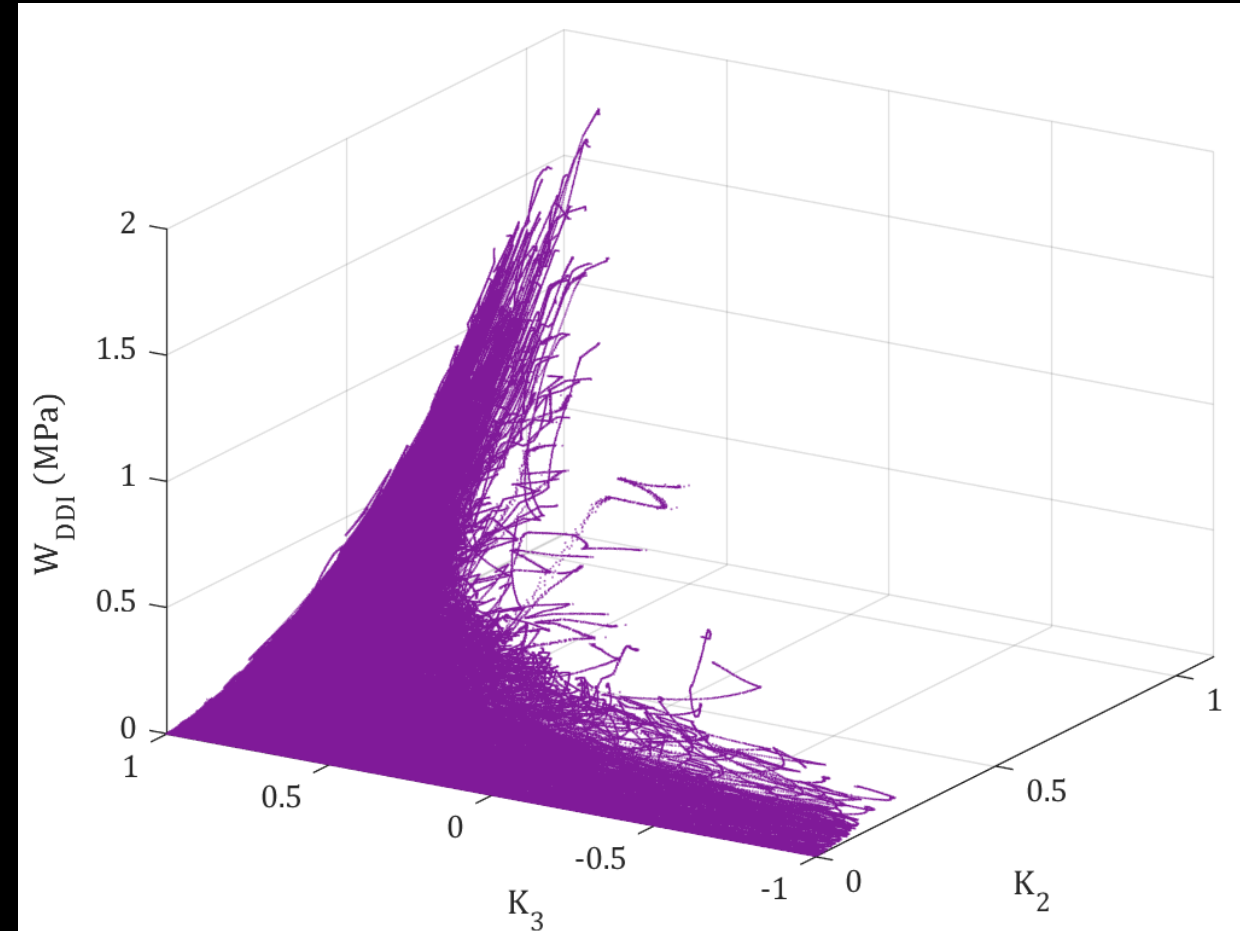
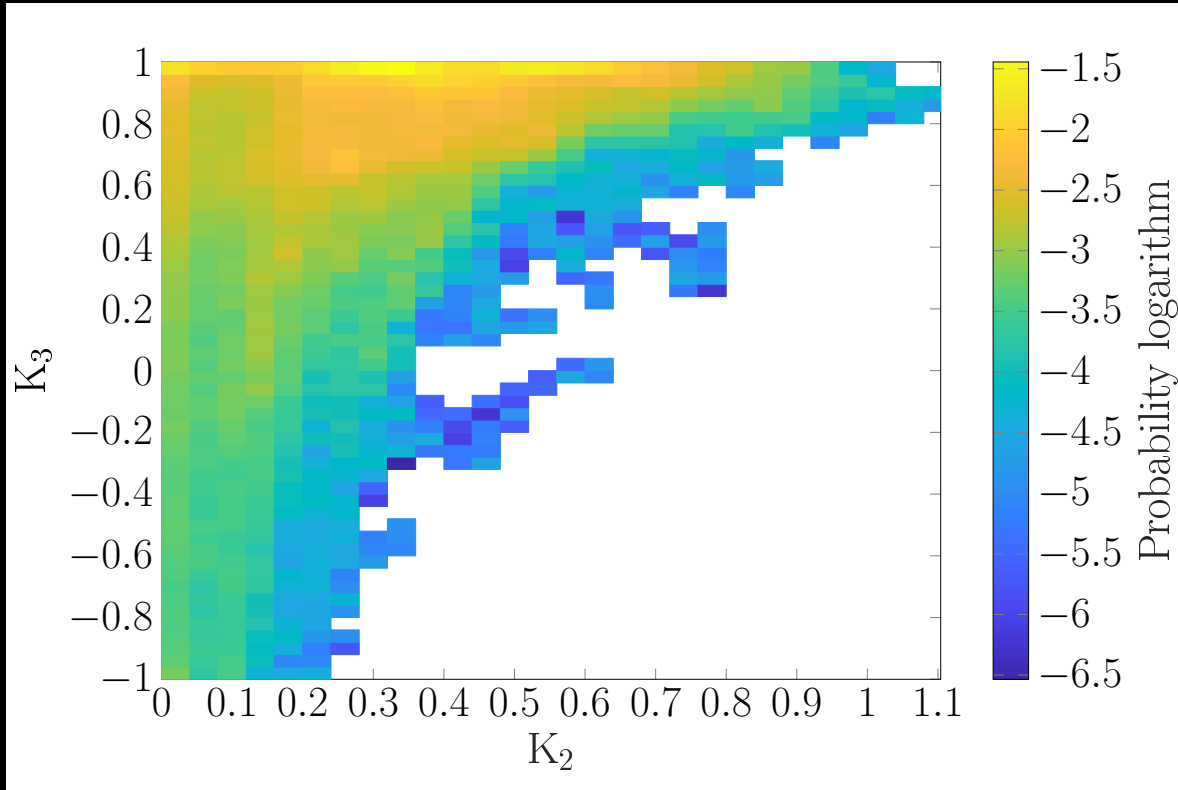
$\bar{\bar{H}}$ -based

~3.5k clusters (ratio=1000)

- Ogden model

$$\Psi(\lambda_1, \lambda_2, \lambda_3) = \sum_p \frac{\mu_p}{\alpha_p} (\lambda_1^{\alpha_p} + \lambda_2^{\alpha_p} + \lambda_3^{\alpha_p} - 3)$$

# Kinematics & Identified energy



# Fitting a model

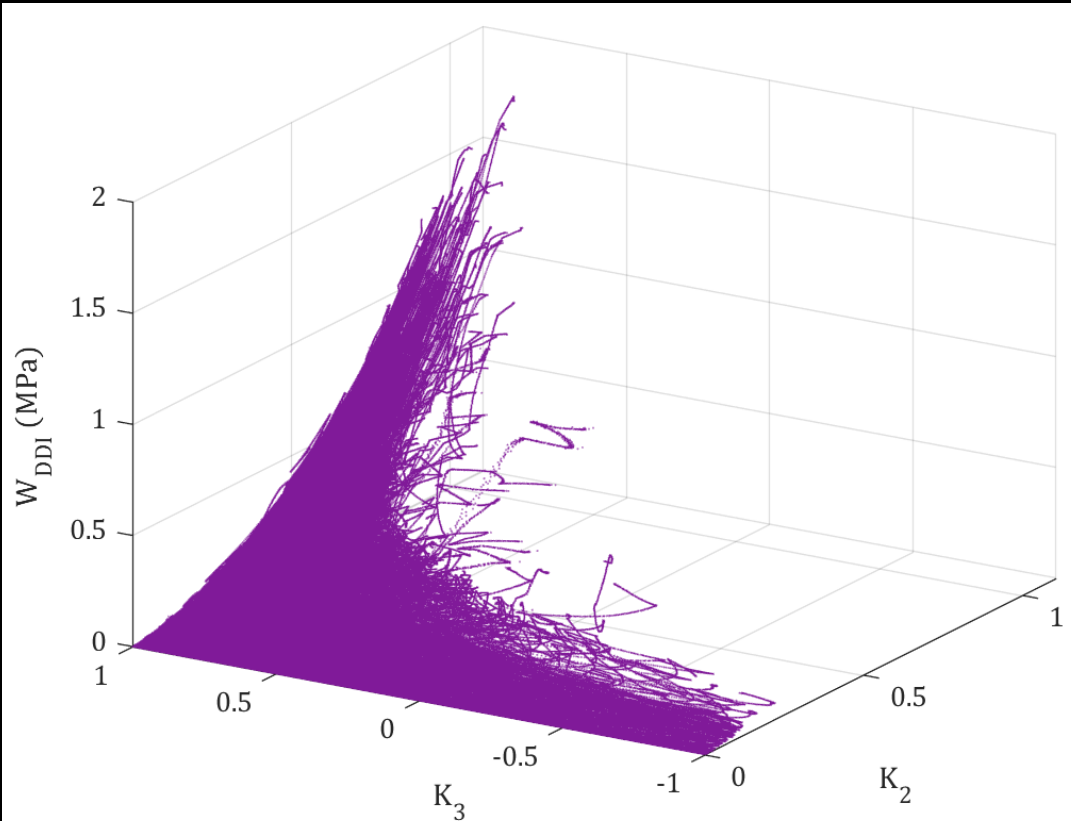
Model: Ogden Model (3 terms)

$$\Psi(\lambda_1, \lambda_2, \lambda_3) = \sum_p \frac{\mu_p}{\alpha_p} (\lambda_1^{\alpha_p} + \lambda_2^{\alpha_p} + \lambda_3^{\alpha_p} - 3)$$

Fitting procedure:

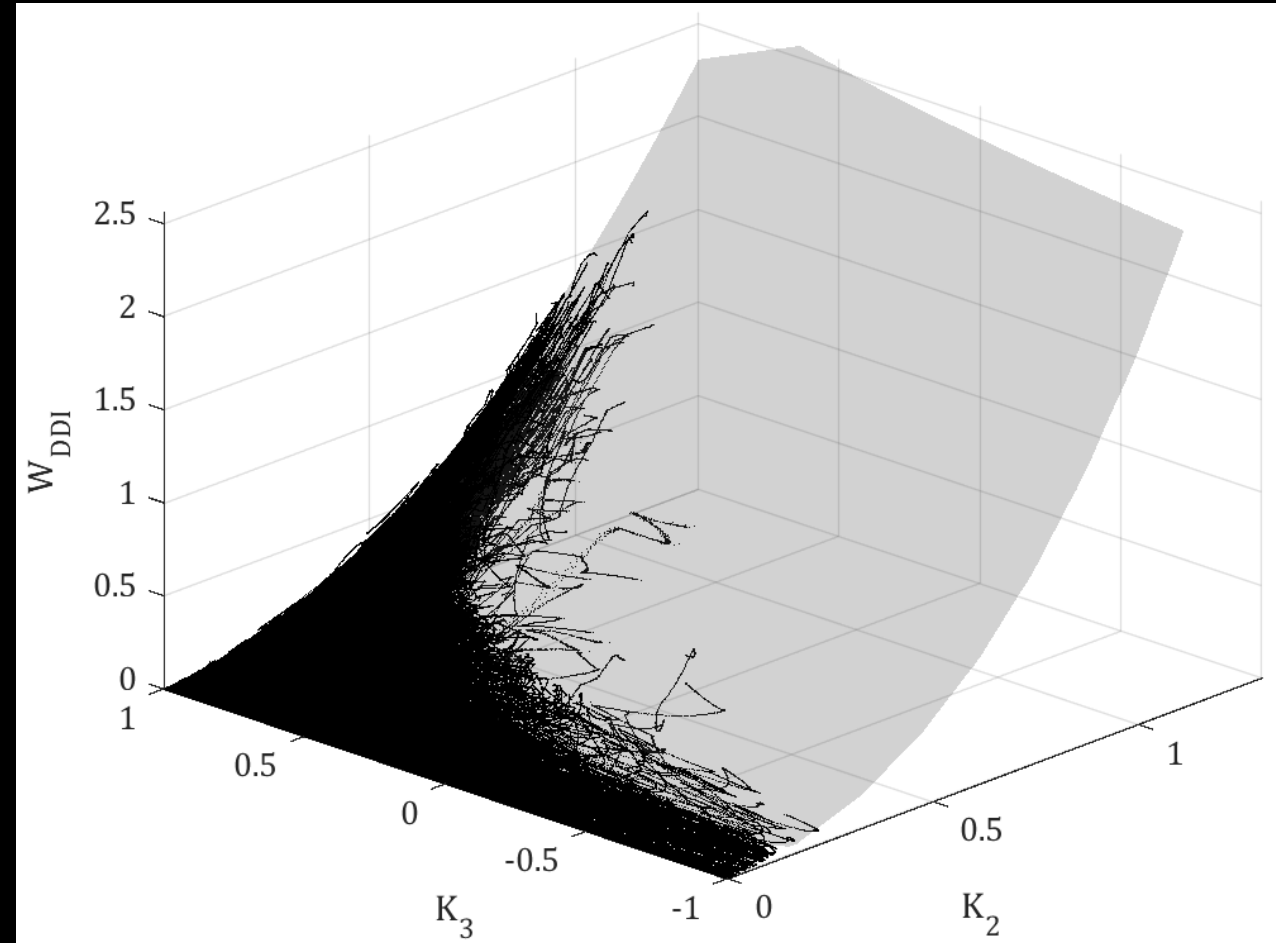
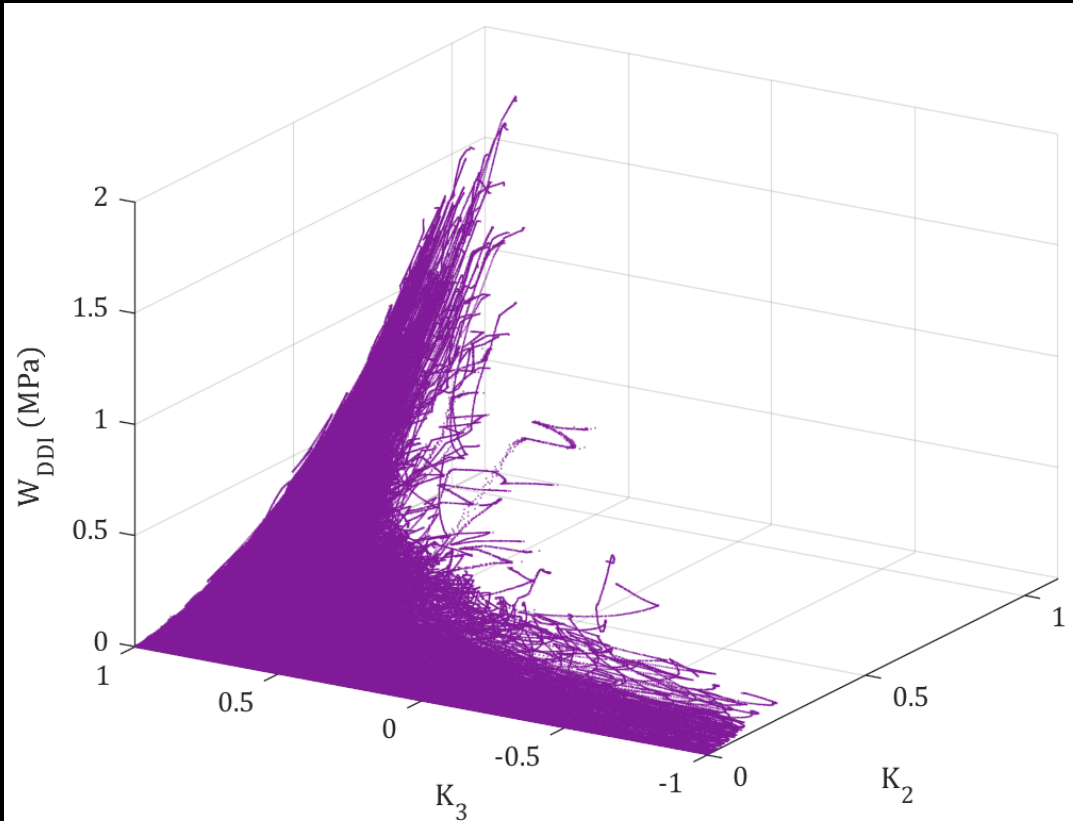
least square on all mechanical points

$$\alpha = \arg \min_{\alpha'} \int_{\Omega} \int_t (W_{DDI} - \Psi(\alpha'))^2$$

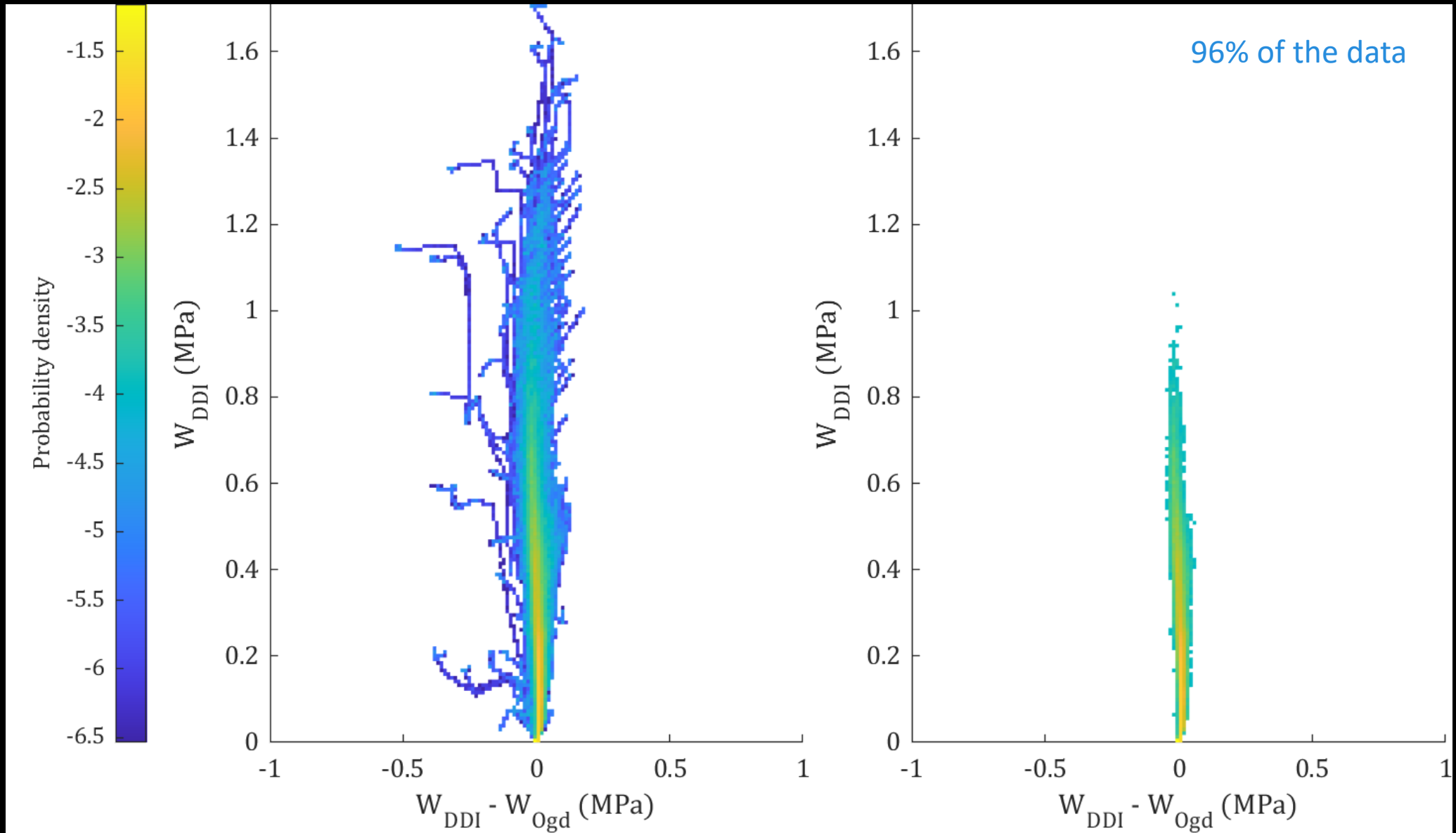


# Fitting a model

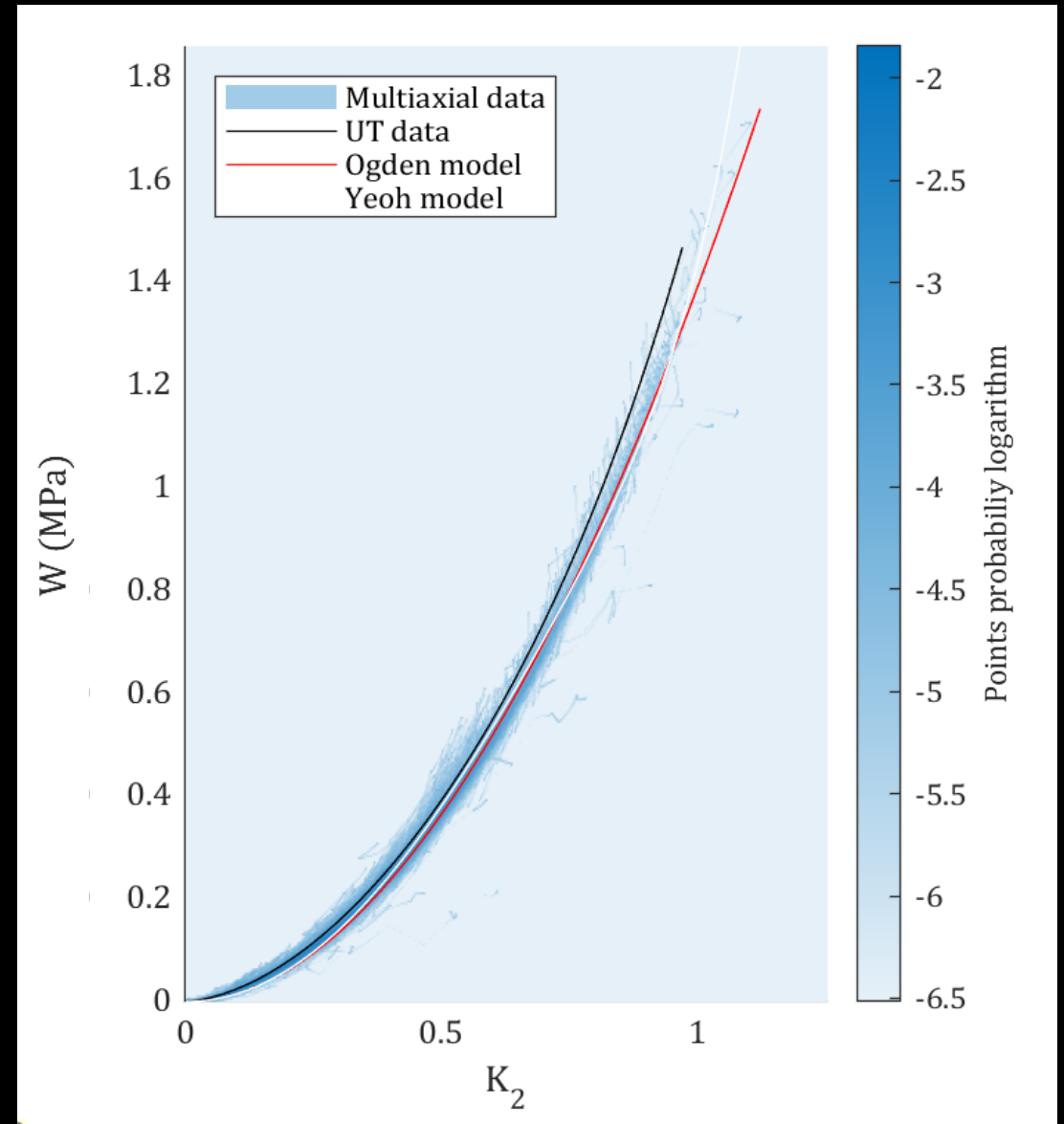
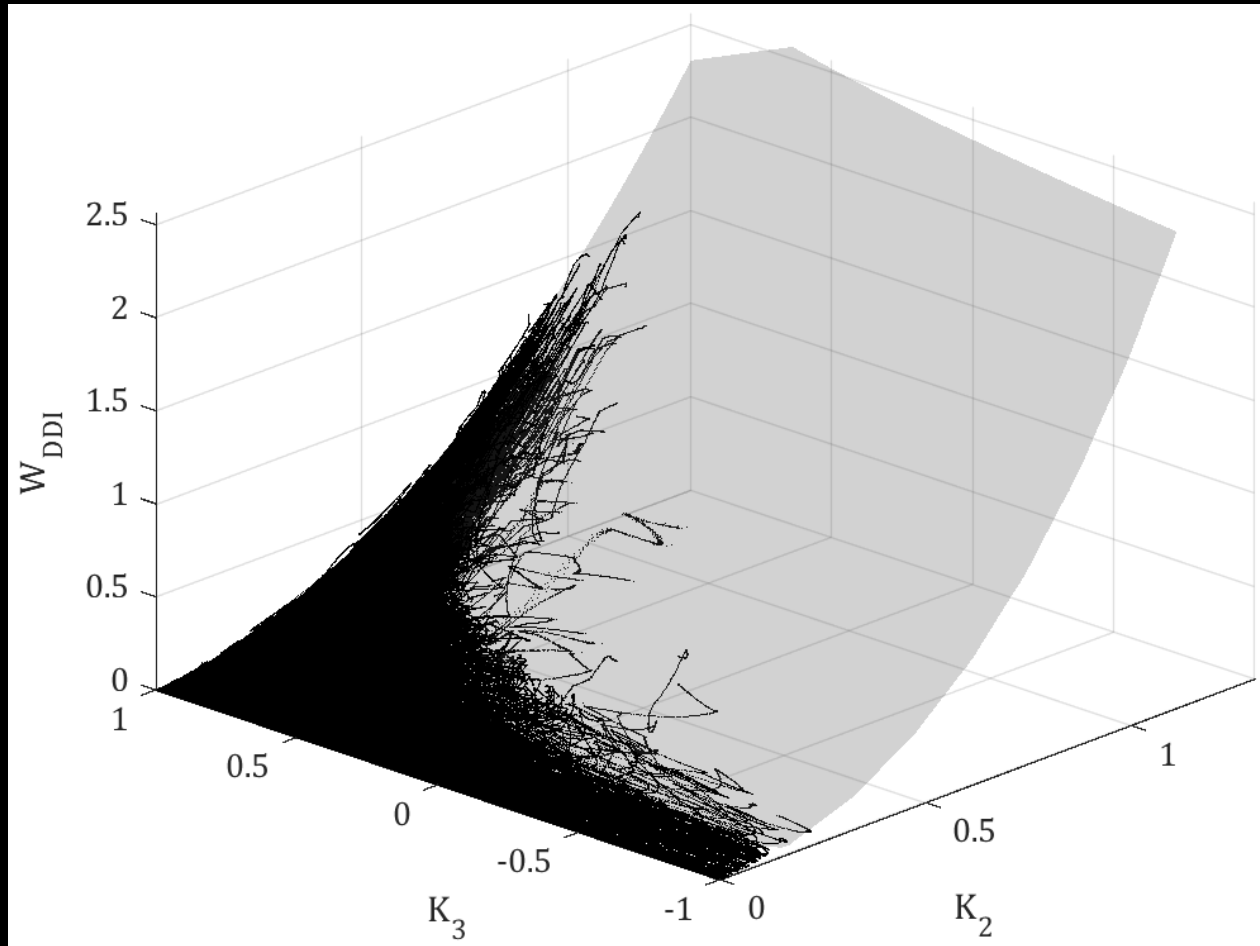
$$\Psi(\lambda_1, \lambda_2, \lambda_3) = \sum_p \frac{\mu_p}{\alpha_p} (\lambda_1^{\alpha_p} + \lambda_2^{\alpha_p} + \lambda_3^{\alpha_p} - 3)$$



# Fitting a model



# Data-Driven (Model) Identification



# Conclusions & perspectives

- Methods for estimating strain & stress in data-rich experiments:
  - Digital Image Correlation
  - Data-Driven Identification
- Preliminary theoretical results on model-free stress estimation
  - Efficient algorithms
  - Guidelines for optimal (hyper)parameters & experiment design
- Classical material models can easily be adjusted a posteriori
  - Cost !
  - Capitalizing on data

# Collaborators

- Christophe Binetruy
- Michel Coret
- Léna Costecalde
- Marie Dalémat
- Héloïse Dandin
- Elie Eid
- Nour Hachem
- Raphaël Langlois
- Pierre-Yves Le Gac
- Maelenn Le Gall
- Hugo Madeira
- Annie Morch
- Auriane Platzer
- Julien Réthoré
- Rian Séghir
- Laurent Stainier
- Gabriel Valdes-Alonzo
- Erwan Verron
- Adrien Vinel